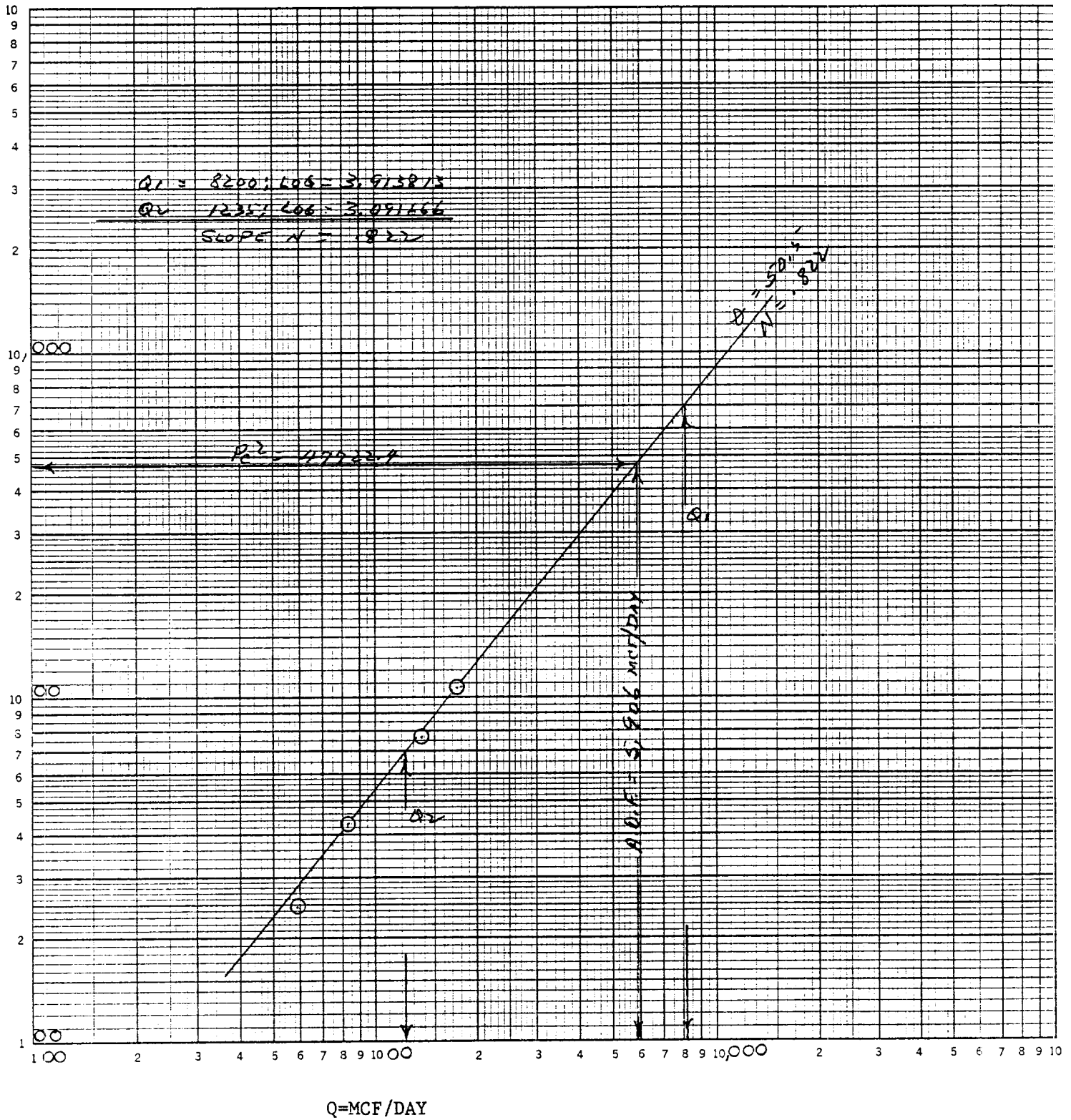


MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 03-11-93	
Company BRIGHT & COMPANY				Connection VENTED			
Pool WILD CAT				Formation ATOKA			
Completion Date 3-3-93		Total Depth 12233		Plug Back TD 12605		Elevation 4321 KB	
Casing Size 5 1/2"		WT. 17		Set At 4.892		Perforations From 10998 To 11034	
Tubg. Size 2 7/8"		WT. 6.5		Set At 10906		Perforations From To	
Type Well - Single - Drawdown - G.C. or G.O. Multiple SINGLE						Packer Set At 10893	
Producing Thru TBG		Reservoir Temp. °F 60°		Mean Annual Temp. °F 60°		Baro. Press. - P _a 13.2	
L 11016		H 11016		C _d .763		% CO ₂ 4.476	
						% N ₂ 3.041	
						% H ₂ S	
						Prover	
						Meter Run 4.026	
						Taps FLG	
FLOW DATA				TUBING DATA		CASING DATA	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. in. H ₂ O	Temp. °F	Press. p.s.i.g.
SI							2013
1.	4	X	2.000	150	4.00	64	1915
2.	4	X	2.000	150	8.00	56	1862
3.	4	X	2.000	150	22.00	61	1803
4.	4	X	2.000	150	35.00	58	1743
5.							
RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{R/P_a}$	Pressure P _a	Flow Temp. Factor FL	Gravity Factor F _g	Super. Compens. Factor. F _{sp}	Rate of Flow O. Mbd
1.	19.81	25.55	163.2	.9962	1.145	1.020	589
2.	19.81	36.13	163.2	1.004	1.145	1.020	839
3.	19.81	59.92	163.2	.9990	1.145	1.020	1,385
4.	19.81	75.58	163.2	1.002	1.145	1.020	1,752
5.							
NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio 95.1 Mcf/bbl.		
1.	.24	524	1.32	.962	A.P.I. Gravity of Liquid Hydrocarbons 54.0 @ 60 Deg.		
2.	.24	516	1.30	.962	Specific Gravity Separator Gas .763		
3.	.24	521	1.31	.962	Specific Gravity Flowing Fluid X X X X X		
4.	.24	518	1.30	.962	Critical Pressure *679 P.S.I.A.		
5.					Critical Temperature *395 °R		
*** P _r 2173.1 P _r ² 4722.4					(1) $\frac{P_c^2}{P_r^2 - P_c^2} = 4.386$		
NO.	P _r ²	P _w	P _r ²	P _r ² - P _w ²	(2) $\left[\frac{P_c^2}{P_r^2 - P_c^2} \right]^n = 3.371$		
1	2116.0	4477.5	244.9		AOF = Q $\left[\frac{P_r^2}{P_r^2 - P_c^2} \right]^n = 5.906$		
2	2071.8	4292.4	430.0				
3	1989.5	3958.1	764.3				
4	1909.4	3645.8	1076.6				
5							
Absolute Open Flow 5,906 Mcf @ 13.025				Angle of Slope 50.5		Slope, n .822	
Remarks: **=CORRECTED TO 4.476% CO ₂ & 3.041 % N ₂ . ***=BHP INSTRUMENT @ THIS DEPTH.							
***=CALCULATED FROM KNOWN BHP'S. WELL MADE 2.00 BBLS 54.0 API GR FLUID DURING TEST.							
Approved By Division		Conducted By JOHN WEST ENGINEERING		Calculated By BM		Checked By BM	



LOGARITHMIC 3 X 3 CYCLES
KEUFFEL & ESSER CO. MADE IN U.S.A.



WORK SHEET FOR CALCULATION OF WELLHEAD PRESSURE (Pc or Pw)
FROM KNOWN BOTTOM HOLE PRESSURE (Pf or Ps)

FORM C-122F

COMPANY BRIGHT & CO. LEASE : APACHE WELL NO. : 1 DATE 3 11 93
UNIT E SECTION : 5 TWSHP : 9 RANGE : 34
L 11016 H : 11016 L/H : 1 G/GMIX : 0.7630
CO2 : 4.476 N2 : 3.041 H2S :
GH : 8405.2 PCR : 679 TCR : 395

LINE		1	2	3	4	5	6	7	8
1	TW(W.H. R)	534	534	534	534	534	534	534	534
2	Ts(B.H. R)	644.2	644.2	644.2	644.2	644.2	644.2	644.2	644.2
3	T=(Tw+Ts/2)	589.1	589.1	589.1	589.1	589.1	589.1	589.1	589.1
4	Z (EST.)	0.827	0.753	ERR	ERR	ERR	ERR	ERR	ERR
5	TZ	487	444	ERR	ERR	ERR	ERR	ERR	ERR
6	GH/TZ	17.260	18.950	ERR	ERR	ERR	ERR	ERR	ERR
7	eS(TABLE XIV)	1.910	2.035	ERR	ERR	ERR	ERR	ERR	ERR
8	Pf or Ps	3100.2	3100.2	0	0	0	0	0	0
9	Pf2 or Ps2	9611.2	9611.2	0.0	0.0	0.0	0.0	0.0	0.0
10	Pc2=Pf/eS or Pw2=Ps2/eS	5031.3	4722.3	ERR	ERR	ERR	ERR	ERR	ERR
11	Pc or Pw	2243	2173	ERR	ERR	ERR	ERR	ERR	ERR
12	P=(Pw+Ps/2)or(Pc+Pf/2)	2672	2637	ERR	ERR	ERR	ERR	ERR	ERR
13	Pr=(P/PCR)	3.93	3.88	ERR	ERR	ERR	ERR	ERR	ERR
14	Tr(T/TCR)	1.49	1.49	1.49	1.49	1.49	1.49	1.49	1.49
15	Z (TABLE XI)	0.753	0.752	ERR	ERR	ERR	ERR	ERR	ERR

Pc

1 : 2173.1 PW 2 : ERR PW 3 : ERR PW 4 : ERR

WORK SHEET FOR CALCULATION OF WELLHEAD PRESSURE (Pc or Pw)
FROM KNOWN BOTTOM HOLE PRESSURE (Pf or Ps)

FORM C-122F

COMPANY BRIGHT & CO. LEASE : APACHE WELL NO. : 1 DATE 3 11 93
UNIT E SECTION : 5 TOWNSHIP : 9 RANGE : 34
L 11016 H : 11016 L/H : 1 G/GMIX : 0.7630
CO2 : 4.476 N2 : 3.041 H2S :
GH : 8405.2 PCR : 679 TCR : 395

LINE		1	2	3	4	5	6	7	8
1	TW(W.H. R)	534	534	534	534	534	534	534	534
2	Ts(B.H. R)	644.2	644.2	644.2	644.2	644.2	644.2	644.2	644.2
3	T=(Tw+Ts/2)	589.1	589.1	589.1	589.1	589.1	589.1	589.1	589.1
4	Z (EST.)	0.822	0.751	0.763	0.750	0.759	0.749	0.755	0.748
5	TZ	484	443	450	442	447	441	445	441
6	GH/TZ	17.350	18.994	18.690	19.032	18.809	19.062	18.908	19.070
7	eS(TABLE XIV)	1.917	2.039	2.016	2.041	2.025	2.044	2.032	2.044
8	Pf or Ps	3021.2	3021.2	2960.2	2960.2	2844.2	2844.2	2730.2	2730.2
9	Pf2 or Ps2	9127.6	9127.6	8762.8	8762.8	8089.5	8089.5	7454.0	7454.0
10	Pc2=Pf/eS or Pw2=Ps2/eS	4762.2	4477.4	4347.6	4292.3	3995.7	3958.0	3668.2	3646.0
11	Pc or Pw	2182	2116	2085	2072	1999	1989	1915	1909
12	P=(Pw+Ps/2)or(Pc+Pf/2)	2602	2569	2523	2516	2422	2417	2323	2320
13	Pr=(P/PCR)	3.83	3.78	3.72	3.71	3.57	3.56	3.42	3.42
14	Tr(T/TCR)	1.49	1.49	1.49	1.49	1.49	1.49	1.49	1.49
15	Z (TABLE XI)	0.751	0.751	0.750	0.750	0.749	0.748	0.748	0.748

PW 1 : 2116.0 PW 2 : 2071.8 PW 3 : 1989.5 PW 4 : 1909.4