

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 12/14/69	
Company Jack L. McClellan		Connection None	
Pool Undes. Bluit San Andres Gas		Formation San Andres	
Completion Date 10/19/69		Total Depth 4909	Plug Back TD 4884
Elevation 3997 DF		Farm or Lease Name Atlantic Federal	
Csg. Size 4 1/2	Wt. 9.5	d 4.090	Set At 4909
Perforations: From 4802 To 4821.5		Well No. 1	
Tbg. Size 2 3/8	Wt. 4.7	d 1.995	Set At 4874
Perforations: From open ended To		Unit Sec. Twp. Rge. I 24 8S 37E	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single		Packer Set At none	
County Roosevelt		State New Mexico	
Producing Thru Tubing		Reservoir Temp. °F @ unknown	Mean Annual Temp. °F 60°
Baro. Press. - P _a 13.2		Prover X	
L 4874	H 4874	Gg .785	% CO ₂ % N ₂ % H ₂ S — — —
Meter Run		Taps	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							1235		1235		72
1.	2	x	3/16	1137		68	1137		1152		1
2.	2	x	1/4	1001		68	1001		1025		1
3.	2	x	5/16	833		69	833		915		1
4.	2	x	1 3/8	38		28	650		784		1
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	.6082		1150.2	.9924	1.129	1.214	952
2	1.087		1014.2	.9924	1.129	1.182	1460
3	1.672		846.2	.9915	1.129	1.137	1801
4	33.95		51.2	1.032	1.129	1.000	2025
5							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	1.73	528	1.26	.678	TSTM		.785	X X X X X X X X	666	418
2.	1.52	528	1.26	.716			X X X X X			
3.	1.27	529	1.27	.773						
4.	0.08	488	1.17	*						
5.										

NO.	P _c	P _w	P _c ²	P _w ²	P _c ² - P _w ²
1	1248.2	1165.2	1558.0	1357.7	200.3
2		1038.2		1077.9	480.1
3		928.2		861.6	696.4
4		797.2		635.5	922.5
5					

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 3.245$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2630$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.8014$$

Absolute Open Flow	2630	Mcfd @ 15.025	Angle of Slope θ	Slope, n 0.50
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Remarks: ***Pr below limits of table.**

Approved By Commission	Conducted By: H. L. Smith	Calculated By: Donna Helles	Checked By:
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