NEW XICO OIL CONSERVATION COMMSSIC

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special			Test Date: 9-8-69	
Company: AVANCE OIL & GAS COMPANY	Connection: NONE YET			STATE LEASE NO. E-704
Pool: WILDCAT	Formation: MORROW			Unit: 160 ACRES
Completion Date: 9-4-69	Total Depth: 13,365	Plug Back TD: 11,900	Elevation: 4037' DF	Farm or Lease Name: STATE ETA
Csg. Size: 5.5 / Wt.: 17.0 / d: / Set At: 13,004	Perforations: From To			Well No.: 2
Tbg. Size: 2 / Wt.: 4.7 / d: 1.995 / Set At: 11,702	Perforations: From 11770 To 11786			Unit: I / Sec.: 8 / Twp.: 16-S / Rge.: 35-E
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: SINGLE		Packer Set At: 11,702		County: LEA
Producing Thru: TUBING	Reservoir Temp. °F: 165 @ 11778	Mean Annual Temp. °F:	Baro. Press. – P_a: 13.2	State: NEW MEXICO

L	H	Gg	% CO_2	% N_2	% H_2S	Prover	Meter Run	Taps
11,702	11,702	.631	.40	.78	0		4.026	FLANGE

	FLOW DATA					TUBING DATA		CASING DATA		
NO.	Prover Line Size	X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI	4.026	2.000				4802	72	PACKER	ATM.	270 MIN
1.	4.026	2.000	630	22	56	4050	83			270 MIN.
2.	4.026	2.000	635	37	51	3547	83			75 MIN.
3.	4.026	2.000	660	52	50	2775	85			120 MIN.
4.	4.026	2.000	670	71	62	2165	85			90 MIN.
5.										

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	19.81	119.0	643.2	1.0039	1.259	1.064	3170
2.	19.81	154.9	648.2	1.0088	1.259	1.067	4158
3.	19.81	187.1	673.2	1.0098	1.259	1.071	5046
4.	19.81	220.2	683.2	.9981	1.259	1.065	5838
5.							

NO.	P_t	Temp. °R	T_r	Z
1	.96	516	1.41	.883
2.	.97	511	1.40	.879
3.	1.00	510	1.39	.871
4.	1.02	522	1.43	.882
5.				

Gas Liquid Hydrocarbon Ratio 124.069 Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons 53.6 Deg.
Specific Gravity Separator Gas .631 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX .655
Critical Pressure 671 P.S.I.A. 671 P.S.I.A.
Critical Temperature 366 R 373 R

P_c 4815.2 P_c^2 23,186

NO	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1	16510	4132.3	17076	6110
2	12675	3658.0	13381	9805
3	7774	3010.5	9063	14123
4	4744	2422.5	5869	17317
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2}$ = 1.33892 (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n$ = 1.181

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n$ = 6891

Absolute Open Flow 6891 Mcfd @ 15.025 Angle of Slope θ 58.5 Slope, n .597

Remarks:

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	LARRY D. CONE	LARRY D. CONE	LARRY D. CONE