

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 12-4-71	
Company V-F PETROLEUM				Connection NONE YET		
Pool UNDESIGNATED				Formation ATOKA		Unit
Completion Date		Total Depth 12,978'		Plug Back TD 11,472'		Elevation 3987 G.L.
Csg. Size 7" O.D.		Wt. 26-35#		Perforations: From 11,417 To 11,435		Well No. 1
Tbg. Size 2" EUE		Wt. 4.70#		Perforations: From OPEN END To		Unit Sec. Twp. Rge. J 15 16S 35E
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE				Packer Set At 11,330'		County LEA
Producing Thru TUBING		Reservoir Temp. °F 175 @ 11,325'		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2
L 11,325'		H 11,325'		G _g 0.636	% CO ₂ 1.12	% N ₂ 0.55
				% H ₂ S NONE	Prover X	Meter Run -
						Taps -

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							3461	64	PACKER		
1.	2.000	x	0.750	92		19	3355	71	"		1-HR
2.	2.000	x	0.750	179		23	3196	76	"		1-HR
3.	2.000	x	0.750	284		25	2971	79	"		1-HR
4.	2.000	x	0.750	370		30	2730	79	"		1-HR
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	9.453		105.2	1.042	1.254	*1.000	1299
2	9.453		192.2	1.038	1.254	1.023	2419
3	9.453		297.2	1.035	1.254	1.035	3774
4	9.453		383.2	1.030	1.254	1.045	4889
5						*NOT APPLICABLE	

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	.16	479	1.32	*1.000	13.90	62.6	0.636	X X X X X X X X		
2	.29	483	1.33	.956				X X X X X		
3	.44	485	1.33	.933						
4	.57	490	1.35	.916						
5	*VALUE NOT INCLUDED IN TABLES									

NO.	P _c	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$
1	4869.2	23,709.1				
2		4765.2	22707.1	1002.0		
3		4627.2	21411.0	2298.1		
4		4450.2	20592.0	3117.1		
5		4266.2	18200.5	5508.6		

Absolute Open Flow 15,200 Mcfd @ 15.025		Angle of Slope 52°	Slope, n 0.784
Remarks:			
Approved By Commission:		Conducted By: HARRY E. LEGENDRE	Checked By:

APEX ENGINEERING COMPANY - MIDLAND, TEXAS