

Type Test				Test Date			
☒ Initial ☐ Annual ☐ Special				10-13-78			
Company				Connection			
Mewbourne Oil Company				Nat. Gas Pipe Line Company			
Pool				Formation			
Wildcat				Atoka			
Completion Date		Total Depth		Plug Back TD		Elevation	
10-8-78		13008		12750		4161 GR	
Casing Size		Casing Wt.		Set At		Perforations	
5.5		17		13008		From 12474 To 12490	
Tubing Size		Tubing Wt.		Set At		Perforations	
2.375		4.7		12320		From To	
Type Well - Single - Rodenthead - G.G. or G.O. Multiple				Packer Set At			
Single Completion				12320			
Producing thru				Reservoir Temp. °F			
Tubing				189 °			
Mean Annual Temp. °F				60			
Baro. Press. - P _a				13.2			
State				New Mexico			
L		H		Gg		% CO ₂	
12482		12482		.687		0	
				% N ₂		0	
				% H ₂ S		0	
Prover		Meter Run		Taps			
		X					

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
1	3.0	1.75		680	4.8	76	2855	72			1 hr.
2	3.0	1.75		680	5.8	76	2361	72			1 hr.
3	3.0	1.75		680	7.6	76	2081	72			1 hr.
4	3.0	1.75		680	8.8	76	1635	72			1 hr.
5											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	15.87	57.68	693.2	.9850	1.206	1.077	1171
2	15.87	63.41	693.2	.9850	1.206	1.077	1287
3	15.87	72.58	693.2	.9850	1.206	1.077	1474
4	15.87	78.10	693.2	.9850	1.206	1.077	1586
5							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	1.04	536	1.38	.862	22992	52.0	.687	.815	669	388
2	1.04	536	1.38	.862						
3	1.04	536	1.38	.862						
4	1.04	536	1.38	.862						
5										

P _r 4461.2 P _c ² 19902				
NO.	P _r ²	P _w	P _w ²	P _c ² - P _w ²
1	3038.3	9231	10671	
2	2533.1	6417	13485	
3	2144.8	4600	15302	
4	1730.2	2994	16908	
5				

$$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.1771$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1791$$

$$(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.12973$$

Absolute Open Flow	1791	Mcf/d @ 15.025	Angle of Slope °	53.5	Slope, n	.748
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Remarks:

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	Johnny Ellis		