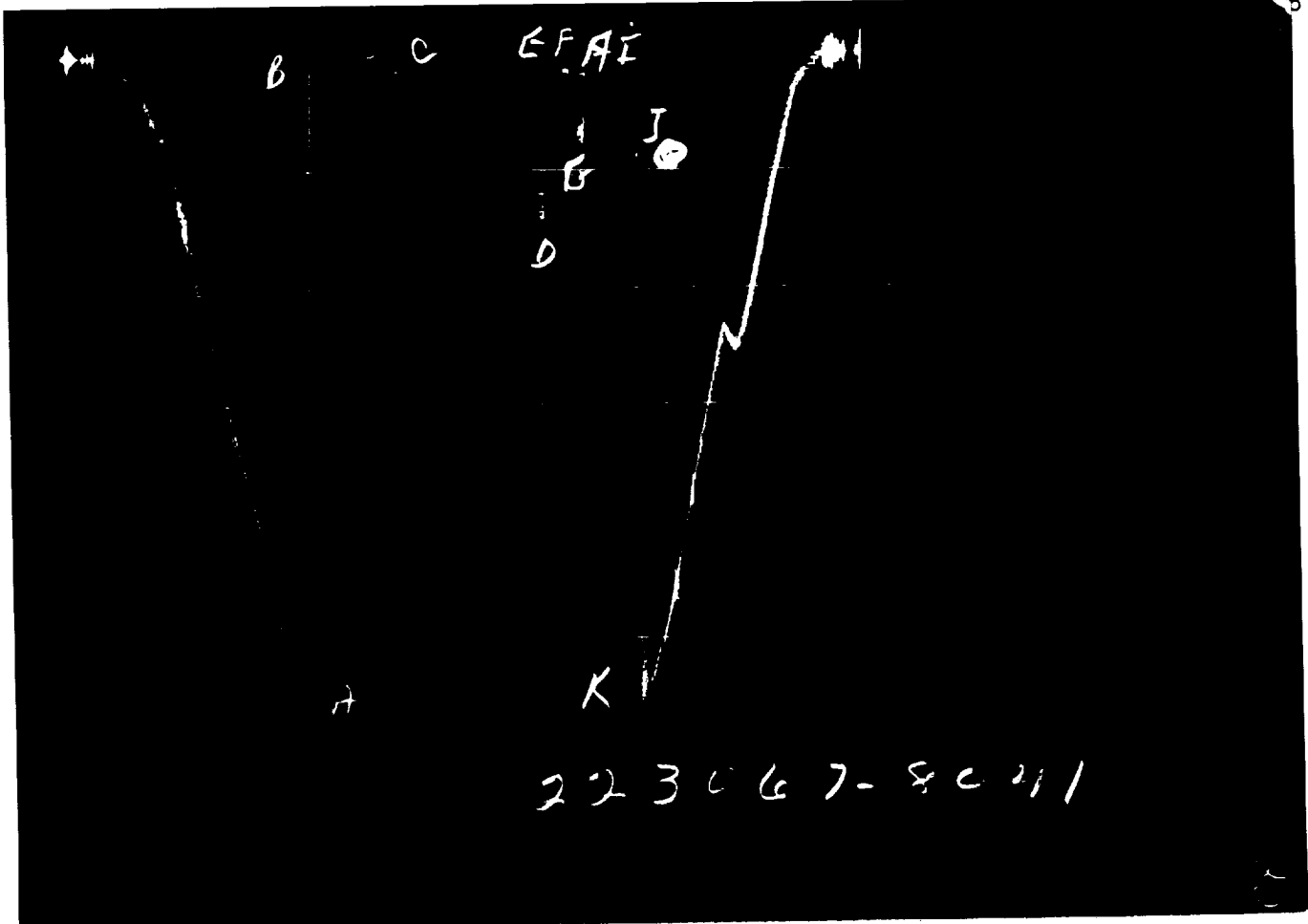




TICKET NO. 22306700
14-NOV-86
HOBBS

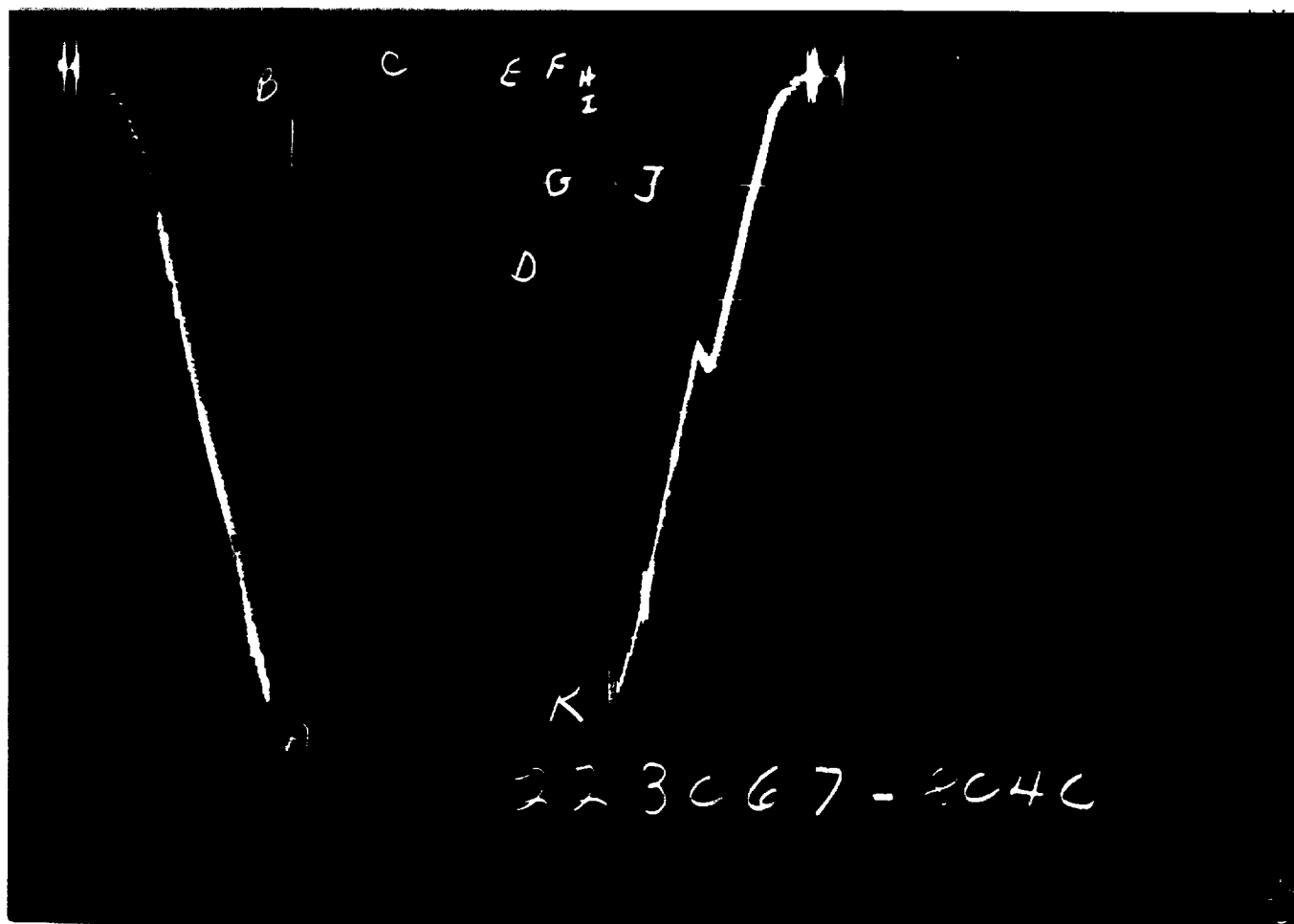
FORMATION TESTING SERVICE REPORT

CHEVRON STATE	1	2	11245.0 - 11285.0	HONDO DRILLING COMPANY INCORPORATED
LEASE NAME	WELL NO.	TEST NO.	TESTED INTERVAL	LEASE OWNER/COMPANY NAME
LEGAL LOCATION SEC. - TWP. - RNG.	18-16S-33E	FIELD AREA	NORTH SANMRL. PENN.	COUNTY
			LER	STATE NEW MEXICO DR



GAUGE NO: 8041 DEPTH: 11227.0 BLANKED OFF: NO HOUR OF CLOCK: 24

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC	5486	5440.1			
B	INITIAL FIRST FLOW	86	55.8	96.0	101.6	F
C	FINAL FIRST FLOW	129	119.1			
C	INITIAL FIRST CLOSED-IN	129	119.1	180.0	171.5	C
D	FINAL FIRST CLOSED-IN	1333	1350.1			
E	INITIAL SECOND FLOW	129	71.9	30.0	32.0	F
F	FINAL SECOND FLOW	172	126.8			
F	INITIAL SECOND CLOSED-IN	172	126.8	80.0	18.4	C
G	FINAL SECOND CLOSED-IN		682.7			
H	INITIAL THIRD FLOW		140.4		1.4	F
I	FINAL THIRD FLOW		140.4			
I	INITIAL THIRD CLOSED-IN		140.4		61.0	C
J	FINAL THIRD CLOSED-IN	901	916.4			
K	FINAL HYDROSTATIC	5486	5455.5			



GAUGE NO: 8040 DEPTH: 11282.0 BLANKED OFF: YES HOUR OF CLOCK: 24

ID	DESCRIPTION	PRESSURE		TIME		TYPE
		REPORTED	CALCULATED	REPORTED	CALCULATED	
A	INITIAL HYDROSTATIC	5573	5523.8			
B	INITIAL FIRST FLOW	44	77.1			
C	FINAL FIRST FLOW	133	140.5	96.0	101.6	F
C	INITIAL FIRST CLOSED-IN	133	140.5			
D	FINAL FIRST CLOSED-IN	1419	1423.9	180.0	171.5	C
E	INITIAL SECOND FLOW	89	87.5			
F	FINAL SECOND FLOW	133	146.0	30.0	32.0	F
F	INITIAL SECOND CLOSED-IN	133	146.0			
G	FINAL SECOND CLOSED-IN		740.4	80.0	18.4	C
H	INITIAL THIRD FLOW		165.9			
I	FINAL THIRD FLOW		165.9		1.4	F
I	INITIAL THIRD CLOSED-IN		165.9			
J	FINAL THIRD CLOSED-IN	931	977.5		61.0	C
K	FINAL HYDROSTATIC	5573	5537.8			

EQUIPMENT & HOLE DATA

FORMATION TESTED: CISCO
 NET PAY (ft): 8.0
 GROSS TESTED FOOTAGE: 40.0
 ALL DEPTHS MEASURED FROM: KB (GL+ 14')
 CASING PERFS. (ft): _____
 HOLE OR CASING SIZE (in): 7.875
 ELEVATION (ft): 4259.4 GROUND LEVEL
 TOTAL DEPTH (ft): 11285.0
 PACKER DEPTH(S) (ft): 11240, 11245
 FINAL SURFACE CHOKE (in): 0.25000
 BOTTOM HOLE CHOKE (in): 0.750
 MUD WEIGHT (lb/gal): 9.20
 MUD VISCOSITY (sec): 44
 ESTIMATED HOLE TEMP. (°F): _____
 ACTUAL HOLE TEMP. (°F): 143 @ 11281.0 ft

TICKET NUMBER: 22306700

DATE: 11-5-86 TEST NO: 2

TYPE DST: OPEN HOLE

HALLIBURTON CAMP:
HOBBS

TESTER: JIM TULL

WITNESS: JACK JOHNSON

DRILLING CONTRACTOR:
HONDA RIG #4

FLUID PROPERTIES FOR RECOVERED MUD & WATER

SOURCE	RESISTIVITY	CHLORIDES
MUD PITS	<u>0.093 @ 57 °F</u>	<u>49435</u> ppm
TOP OF RECOVERY	<u>0.110 @ 70 °F</u>	<u>40000</u> ppm
MIDDLE RECOVERY	<u>0.101 @ 70 °F</u>	<u>46357</u> ppm
TOOL TOP	<u>0.101 @ 70 °F</u>	<u>46830</u> ppm
	<u> @ °F</u>	<u> </u> ppm
	<u> @ °F</u>	<u> </u> ppm

SAMPLER DATA

Psig AT SURFACE: 15.0
 cu.ft. OF GAS: 0.100
 cc OF OIL: 250.0
 cc OF WATER: _____
 cc OF MUD: _____
 TOTAL LIQUID cc: 250.0

HYDROCARBON PROPERTIES

OIL GRAVITY (°API): 41.2 @ 60 °F
 GAS/OIL RATIO (cu.ft. per bbl): _____
 GAS GRAVITY: _____

CUSHION DATA

TYPE	AMOUNT	WEIGHT
_____	_____	_____
_____	_____	_____

RECOVERED:

310' OF GAS AND OIL CUT MUD

MEASURED FROM
TESTER VALVE

REMARKS:

THE TOOLS DID NOT OPEN AND CLOSE AS REPORTED IN THE JOB DESCRIPTION. IT APPEARS THAT THE TOOLS WERE OUT OF SEQUENCE AND THEREFORE THE TEST WAS NOT CONDUCTED AS REPORTED.

[illegible]

TICKET NO: 22306700

CLOCK NO: 16511 HOUR: 24



GAUGE NO: 8041

DEPTH: 11227.0

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
FIRST FLOW					
B 1	0.0	55.8			
2	5.0	57.7	1.9		
3	10.0	65.5	7.7		
4	15.0	72.3	7.3		
5	20.0	78.3	5.8		
6	25.0	83.5	4.9		
7	30.0	88.0	4.5		
8	35.0	91.4	3.4		
9	40.0	94.2	2.8		
10	45.0	96.8	2.6		
11	50.0	100.2	3.4		
12	55.0	101.7	1.5		
13	60.0	104.3	2.6		
14	65.0	107.3	3.0		
15	70.0	107.3	0.0		
16	75.0	110.5	3.2		
17	80.0	112.5	1.9		
18	85.0	112.5	0.0		
19	90.0	115.5	3.0		
20	95.0	115.5	0.0		
21	100.0	119.3	3.9		
C 22	101.6	119.1	-0.2		

FIRST CLOSED-IN

C 1	0.0	119.1			
2	1.0	190.4	71.3	1.0	2.002
3	2.0	279.2	160.1	1.9	1.724
4	3.0	362.1	243.0	2.9	1.546
5	4.0	417.9	298.8	3.9	1.419
6	5.0	469.8	350.7	4.8	1.327
7	6.0	525.8	406.7	5.7	1.255
8	7.0	565.5	446.4	6.6	1.189
9	8.0	608.5	489.3	7.4	1.139
10	9.0	642.8	523.7	8.3	1.090
11	10.0	677.2	558.0	9.1	1.049
12	12.0	740.3	621.1	10.7	0.976
13	14.0	790.3	671.1	12.3	0.918
14	16.0	839.2	720.1	13.8	0.866
15	18.0	880.4	761.3	15.3	0.822
16	20.0	919.0	799.9	16.7	0.784
17	22.0	951.2	832.1	18.1	0.749
18	24.0	982.1	863.0	19.4	0.719
19	26.0	1007.9	888.8	20.7	0.691
20	28.0	1034.5	915.4	22.0	0.665
21	30.0	1055.3	936.1	23.2	0.642
22	35.0	1101.7	982.6	26.0	0.592
23	40.0	1140.8	1021.7	28.7	0.549
24	45.0	1171.9	1052.8	31.2	0.513
25	50.0	1196.1	1077.0	33.5	0.482
26	55.0	1216.4	1097.3	35.7	0.454

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
FIRST CLOSED-IN - CONTINUED					
27	60.0	1233.3	1114.1	37.7	0.431
28	65.0	1247.3	1128.2	39.7	0.409
29	70.0	1260.5	1141.3	41.5	0.389
30	75.0	1272.1	1153.0	43.2	0.372
31	80.0	1281.0	1161.9	44.8	0.356
32	85.0	1290.1	1170.9	46.3	0.342
33	90.0	1295.9	1176.8	47.7	0.328
34	95.0	1303.0	1183.9	49.1	0.316
35	100.0	1308.2	1189.1	50.4	0.305
36	105.0	1315.1	1196.0	51.7	0.294
37	110.0	1318.6	1199.5	52.8	0.284
38	120.0	1326.4	1207.2	55.0	0.256
39	135.0	1336.1	1217.0	58.0	0.244
40	150.0	1343.6	1224.5	60.6	0.225
41	165.0	1350.1	1231.0	62.9	0.208
D 42	171.5	1350.1	1231.0	63.8	0.202

SECOND FLOW

E 1	0.0	71.9			
2	2.0	73.6	1.7		
3	4.0	73.6	0.0		
4	6.0	80.4	6.9		
5	8.0	103.2	22.8		
6	10.0	116.3	13.1		
7	12.0	120.1	3.9		
8	14.0	121.6	1.5		
9	16.0	121.6	0.0		
10	18.0	121.6	0.0		
11	20.0	121.6	0.0		
12	22.0	121.6	0.0		
13	24.0	122.7	1.1		
14	26.0	122.7	0.0		
15	28.0	124.4	1.7		
16	30.0	124.9	0.4		
F 17	32.0	126.8	1.9		

SECOND CLOSED-IN

F 1	0.0	126.8			
2	1.0	229.6	102.8	1.0	2.135
3	2.0	284.6	157.8	2.0	1.830
4	3.0	338.4	211.6	3.0	1.655
5	4.0	372.3	245.5	3.9	1.539
6	5.0	409.7	282.9	4.8	1.446
7	6.0	447.9	321.1	5.8	1.366
8	7.0	478.8	352.0	6.7	1.303
9	8.0	504.8	378.0	7.6	1.247
10	9.0	533.7	406.9	8.5	1.198
11	10.0	561.2	434.4	9.3	1.158
12	12.0	606.5	479.7	11.0	1.083
13	14.0	638.3	511.5	12.7	1.022

REMARKS:

TICKET NO: 22308700

CLOCK NO: 16511 HOUR: 24



GAUGE NO: 8041

DEPTH: 11227.0

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
SECOND CLOSED-IN - CONTINUED					
14	16.0	680.3	553.5	14.3	0.971
G 15	18.4	682.7	555.9	16.2	0.917

THIRD FLOW

H 1	0.0	140.4			
I 2	1.4	140.4	0.0		

THIRD CLOSED-IN

I 1	0.0	140.4			
2	1.0	183.6	43.1	1.0	2.146
3	2.0	239.2	98.8	2.0	1.829
4	3.0	278.9	138.5	2.9	1.662
5	4.0	330.2	189.8	3.9	1.540
6	5.0	363.3	222.8	4.8	1.449
7	6.0	394.8	254.4	5.8	1.368
8	7.0	422.5	282.1	6.6	1.308
9	8.0	445.3	304.8	7.6	1.252
10	9.0	471.0	330.6	8.5	1.204
11	10.0	491.4	351.0	9.3	1.162
12	12.0	532.2	391.8	11.0	1.088
13	14.0	569.8	429.4	12.7	1.026
14	16.0	602.2	461.8	14.3	0.975
15	18.0	631.2	490.7	15.9	0.929
16	20.0	655.2	514.8	17.4	0.889
17	22.0	680.6	540.1	18.9	0.854
18	24.0	701.2	560.7	20.4	0.821
19	26.1	723.7	583.3	21.8	0.791
20	28.0	740.2	599.8	23.2	0.766
21	30.0	757.6	617.2	24.6	0.740
22	35.0	791.7	651.3	27.8	0.687
23	40.0	823.7	683.3	30.9	0.641
24	45.0	851.0	710.5	33.7	0.602
25	50.0	874.6	734.2	36.5	0.569
26	55.0	896.3	755.8	39.1	0.538
J 27	61.0	916.4	776.0	42.0	0.507

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
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REMARKS:

TICKET NO: 22306700

CLOCK NO: 27306 HOUR: 24



HALLIBURTON

 SERVICES

GAUGE NO: 8040

DEPTH: 11232.0

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
FIRST FLOW					
B 1	0.0	77.1			
2	5.0	79.5	2.4		
3	10.0	85.9	7.3		
4	15.0	92.9	6.0		
5	20.0	98.8	6.0		
6	25.0	103.9	5.1		
7	30.0	108.4	4.4		
8	35.0	111.9	3.5		
9	40.0	114.4	2.4		
10	45.0	117.2	2.9		
11	50.0	119.5	2.2		
12	55.0	121.7	2.2		
13	60.0	123.3	2.2		
14	65.0	126.1	2.2		
15	70.0	128.3	2.2		
16	75.0	130.3	2.2		
17	80.0	131.4	0.9		
18	85.0	133.9	2.4		
19	90.0	135.2	1.3		
20	95.0	136.8	1.6		
21	100.0	138.5	1.8		
C 22	101.6	140.5	2.0		

FIRST CLOSED-IN

C 1	0.0	140.5			
2	1.0	157.6	17.1	1.0	2.013
3	2.0	177.1	36.6	1.9	1.723
4	3.0	266.3	125.7	2.9	1.548
5	4.0	335.7	195.2	3.9	1.417
6	5.0	401.1	260.6	4.7	1.330
7	6.0	466.5	326.0	5.7	1.251
8	7.0	522.0	381.4	6.6	1.189
9	8.0	567.9	427.3	7.4	1.137
10	9.0	615.1	474.6	8.3	1.090
11	10.0	655.5	514.9	9.1	1.048
12	12.0	737.5	597.0	10.7	0.976
13	14.0	813.4	672.8	12.3	0.916
14	16.0	867.0	726.5	13.8	0.866
15	18.0	919.8	779.3	15.3	0.823
16	20.0	961.1	820.5	16.7	0.785
17	22.0	997.7	857.1	18.1	0.751
18	24.0	1029.2	888.6	19.4	0.718
19	26.0	1056.4	915.9	20.7	0.691
20	28.0	1084.2	943.6	21.9	0.666
21	30.0	1107.9	967.4	23.1	0.643
22	35.0	1161.3	1021.2	26.0	0.592
23	40.0	1203.0	1062.5	28.7	0.549
24	45.0	1235.2	1094.6	31.2	0.513
25	50.0	1262.0	1121.5	33.5	0.482
26	55.0	1282.6	1142.1	35.7	0.455

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
FIRST CLOSED-IN - CONTINUED					
27	60.0	1302.6	1162.1	37.7	0.430
28	65.0	1320.3	1179.8	39.6	0.409
29	70.0	1332.5	1192.0	41.5	0.390
30	75.0	1343.6	1203.1	43.1	0.372
31	80.0	1354.5	1214.0	44.8	0.356
32	85.0	1361.1	1220.6	46.3	0.342
33	90.0	1370.0	1229.5	47.7	0.328
34	95.0	1377.8	1237.2	49.1	0.316
35	100.0	1382.2	1241.7	50.4	0.305
36	105.0	1386.6	1246.1	51.7	0.294
37	110.0	1391.3	1250.8	52.8	0.284
38	120.0	1399.5	1259.0	55.0	0.266
39	135.0	1409.0	1268.5	58.0	0.244
40	150.0	1414.6	1274.1	60.6	0.225
41	165.0	1422.6	1282.0	62.9	0.209
D 42	171.5	1423.9	1283.4	63.8	0.202

SECOND FLOW

E 1	0.0	87.5			
2	2.0	88.8	1.3		
3	4.0	88.8	0.0		
4	6.0	89.9	1.1		
5	8.0	103.2	13.3		
6	10.0	126.1	22.8		
7	12.0	133.8	7.8		
8	14.0	137.2	3.3		
9	16.0	138.1	0.9		
10	18.0	138.1	0.0		
11	20.0	138.3	0.2		
12	22.0	139.4	1.1		
13	24.0	141.2	1.8		
14	26.0	142.1	0.9		
15	28.0	142.9	0.9		
16	30.0	143.8	0.9		
F 17	32.0	146.0	2.2		

SECOND CLOSED-IN

F 1	0.0	146.0			
2	1.0	163.8	17.7	1.0	2.118
3	2.0	218.8	72.7	2.0	1.833
4	3.0	286.6	140.6	3.0	1.656
5	4.0	339.2	193.2	3.9	1.532
6	5.0	384.2	238.2	4.8	1.445
7	6.0	435.2	289.2	5.8	1.364
8	7.0	478.7	332.7	6.7	1.301
9	8.0	512.4	366.4	7.5	1.250
10	9.0	548.1	402.1	8.5	1.199
11	10.0	581.2	435.1	9.3	1.156
12	12.0	632.9	486.8	11.0	1.085
13	14.0	678.5	532.5	12.7	1.024

REMARKS:

TICKET NO: 22306700

CLOCK NO: 27306 HOUR: 24



GAUGE NO: 8040

DEPTH: 11282.0

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
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SECOND CLOSED-IN - CONTINUED

	14	16.0	712.7	566.6	14.3	0.972
G	15	18.4	740.4	594.4	16.2	0.917

THIRD FLOW

H	:	0.0	165.3			
I	2	1.4	165.3	0.0		

THIRD CLOSED-IN

I	1	0.0	165.9			
	2	1.0	207.2	41.3	1.0	2.149
	3	2.0	262.4	96.5	1.9	1.844
	4	3.0	306.8	140.9	3.0	1.660
	5	4.0	344.9	179.0	3.9	1.543
	6	5.0	381.9	216.0	4.8	1.449
	7	6.0	412.6	246.7	5.8	1.371
	8	7.0	450.9	285.0	6.7	1.307
	9	8.0	475.6	309.9	7.6	1.252
	10	9.0	502.2	336.3	8.5	1.203
	11	10.0	527.0	361.1	9.3	1.161
	12	12.0	570.9	405.0	11.0	1.088
	13	14.0	614.9	448.9	12.7	1.026
	14	16.0	649.5	483.5	14.3	0.975
	15	18.0	678.3	512.4	15.9	0.930
	16	20.0	705.8	539.9	17.4	0.889
	17	22.0	730.2	564.3	18.9	0.853
	18	24.0	753.7	587.8	20.4	0.821
	19	26.0	772.6	606.6	21.8	0.792
	20	28.0	792.3	626.4	23.2	0.766
	21	30.0	811.6	645.9	24.5	0.741
	22	35.0	853.1	687.2	27.8	0.686
	23	40.0	886.1	720.2	30.9	0.641
	24	45.0	912.7	746.8	33.8	0.602
	25	50.0	938.7	772.8	36.5	0.569
	26	55.0	960.0	794.0	39.1	0.538
J	27	61.0	977.5	811.6	42.0	0.507

REF	MINUTES	PRESSURE	ΔP	$\frac{t \times \Delta t}{t + \Delta t}$	$\log \frac{t + \Delta t}{\Delta t}$
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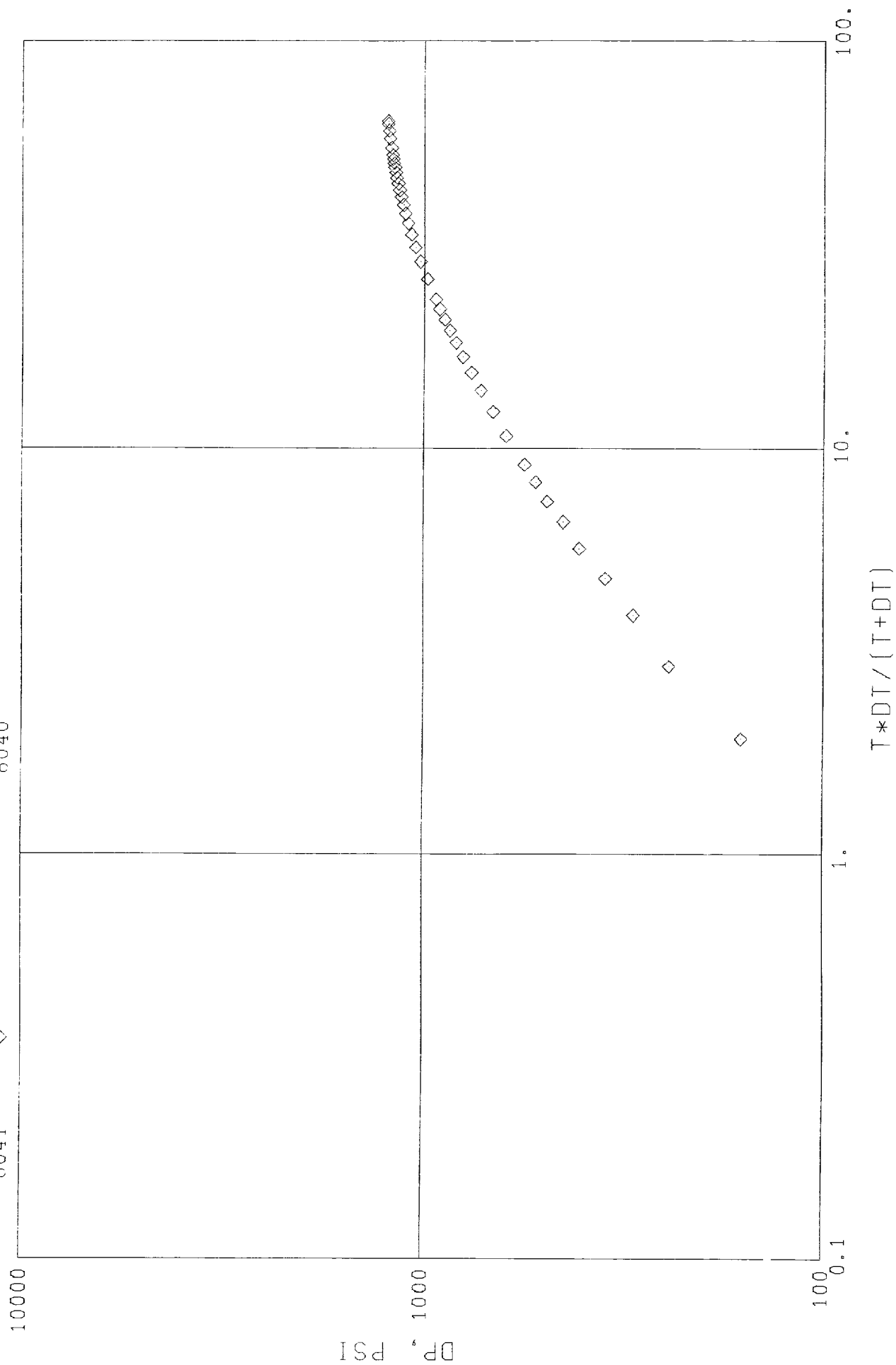
REMARKS:

		O.D.	I.D.	LENGTH	DEPTH
1					
	DRILL PIPE.....	4.500	3.826	10601.0	
3					
	DRILL COLLARS.....	6.250	2.250	422.0	
50					
	IMPACT REVERSING SUB.....	6.125	2.875	1.2	11023.0
3					
	DRILL COLLARS.....	6.250	2.250	182.0	
5					
	CROSSOVER.....	5.750	2.500	1.0	
62					
	MULTIPLE CIP SAMPLER.....	5.000	0.750	9.0	11215.0
14					
	EXTENSION JOINT.....	5.000	0.870	5.0	
14					
	EXTENSION JOINT.....	5.000	0.870	5.0	
80					
	AP RUNNING CASE.....	5.000	2.250	4.0	11227.0
15					
	JAR.....	5.000	1.750	5.0	
16					
	VR SAFETY JOINT.....	5.000	1.000	3.0	
70					
	OPEN HOLE PACKER.....	7.000	1.530	5.0	11240.0
70					
	OPEN HOLE PACKER.....	7.000	1.530	5.0	11245.0
20					
	FLUSH JOINT ANCHOR.....	5.750	3.000	33.0	
81					
	BLANKED-OFF RUNNING CASE.....	5.750		4.0	11282.0
TOTAL DEPTH					11285.0

EQUIPMENT DATA

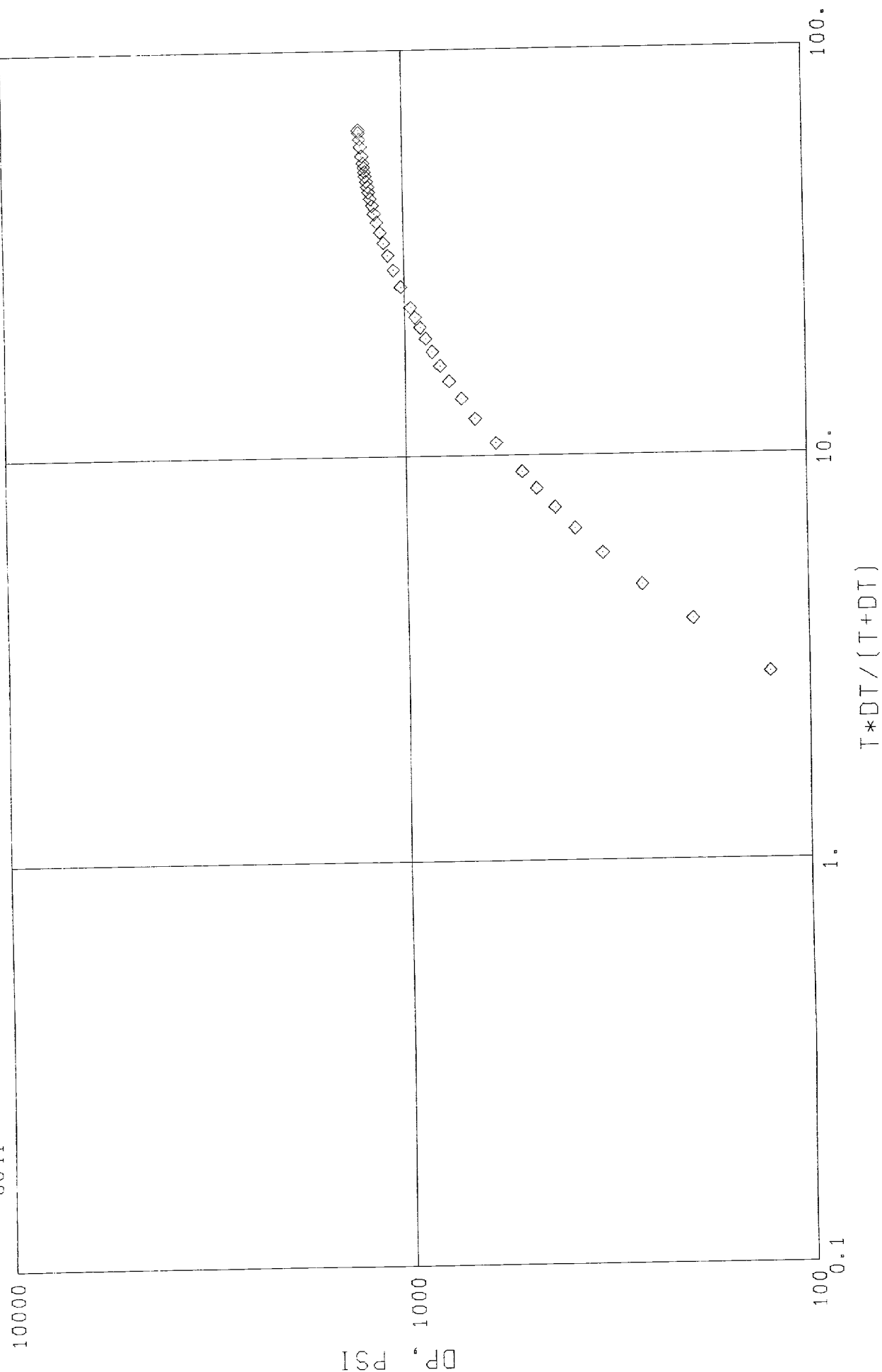
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GAUGE NO CIP 1 2 3
8041 8040



GAUGE NO CIP 1 2 3
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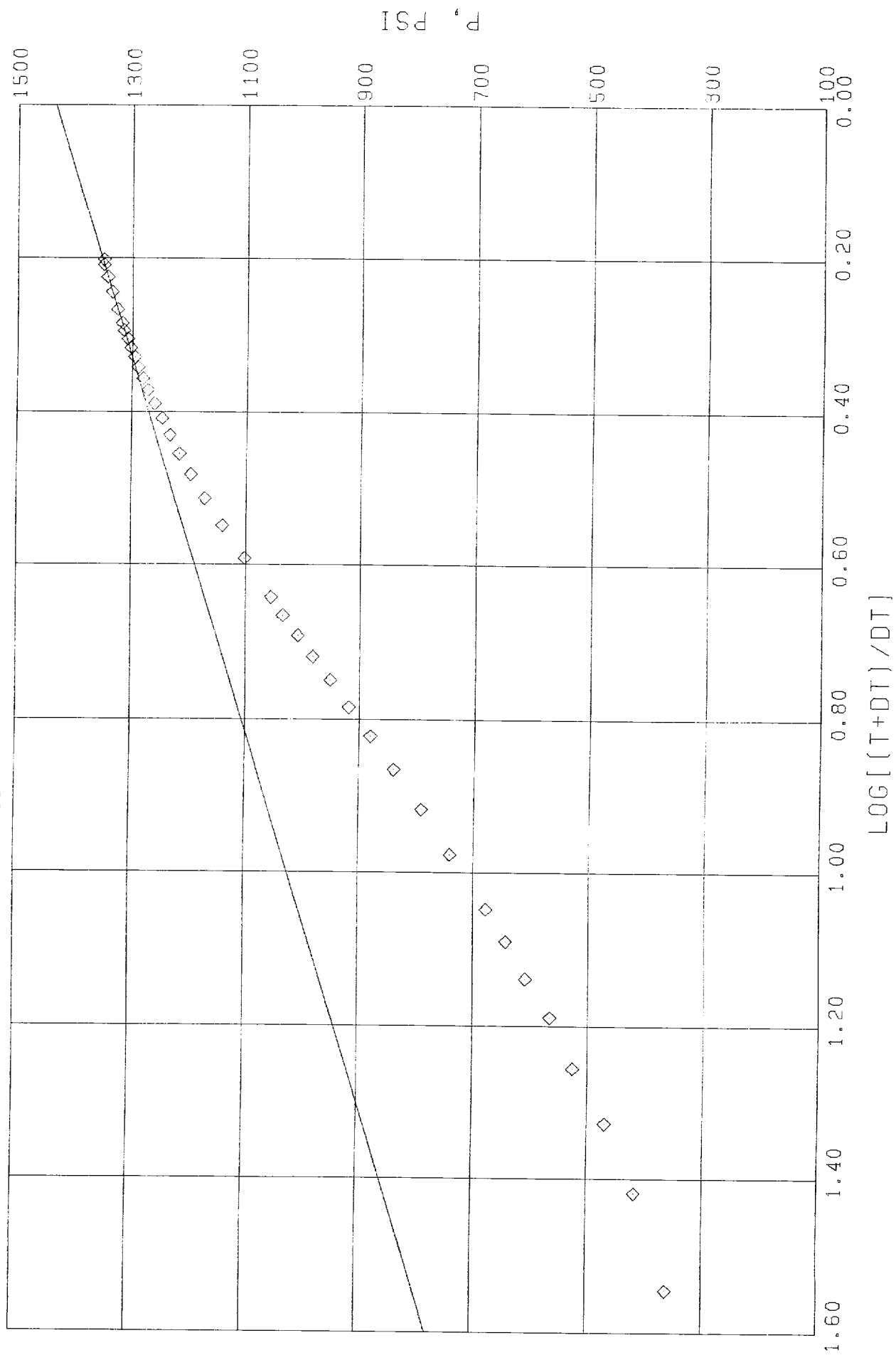
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TICKET NO 22306700

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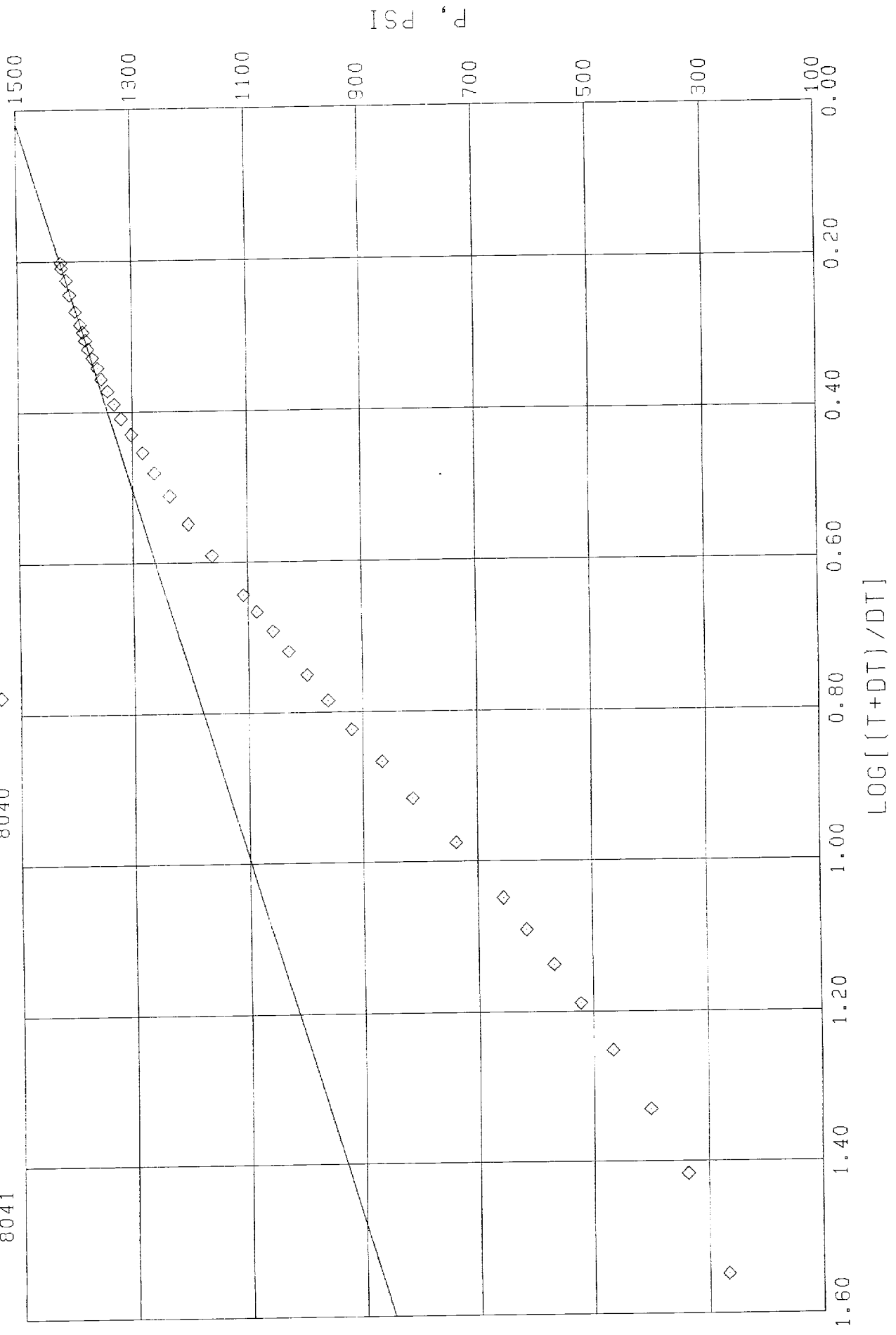
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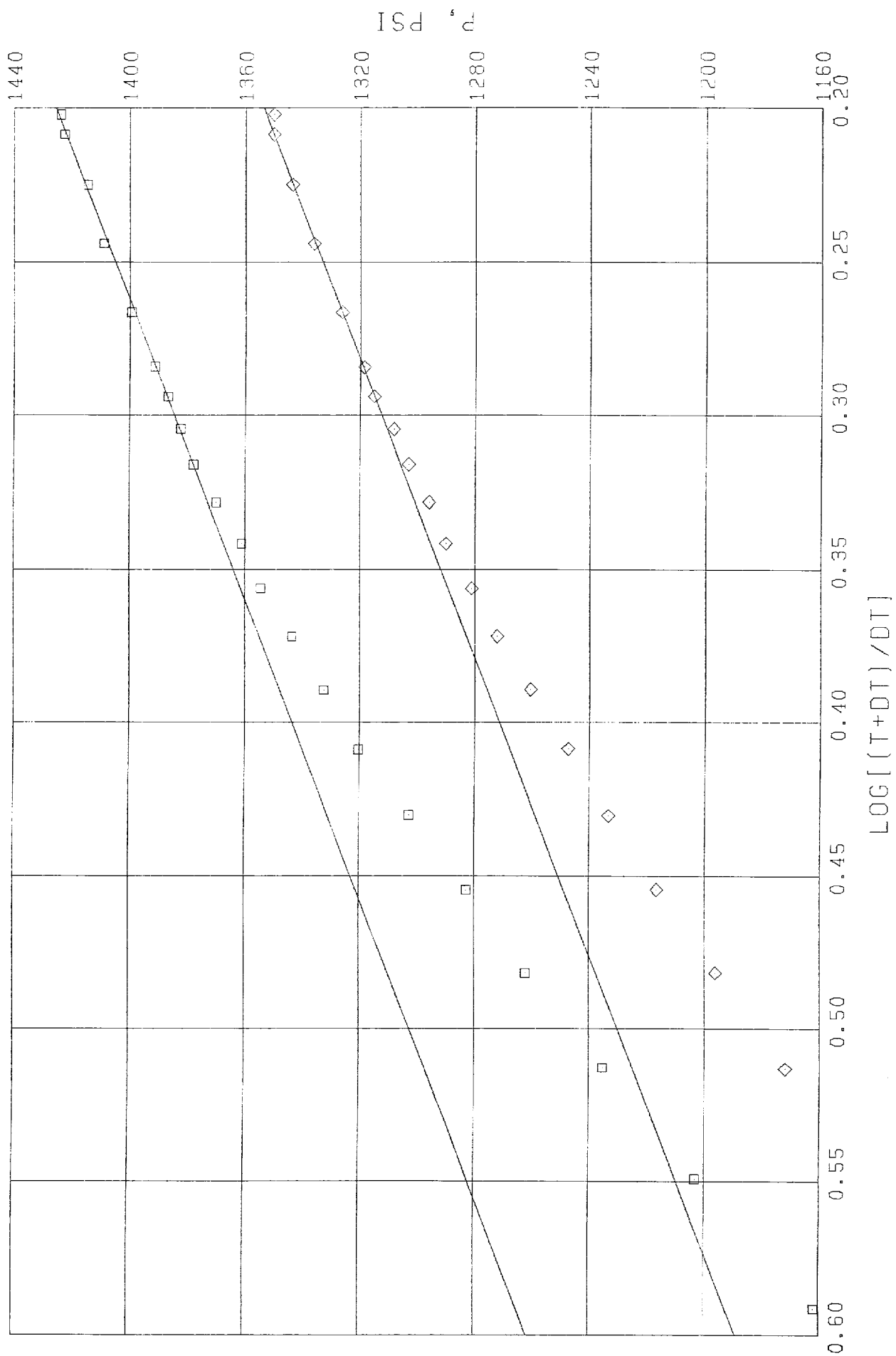
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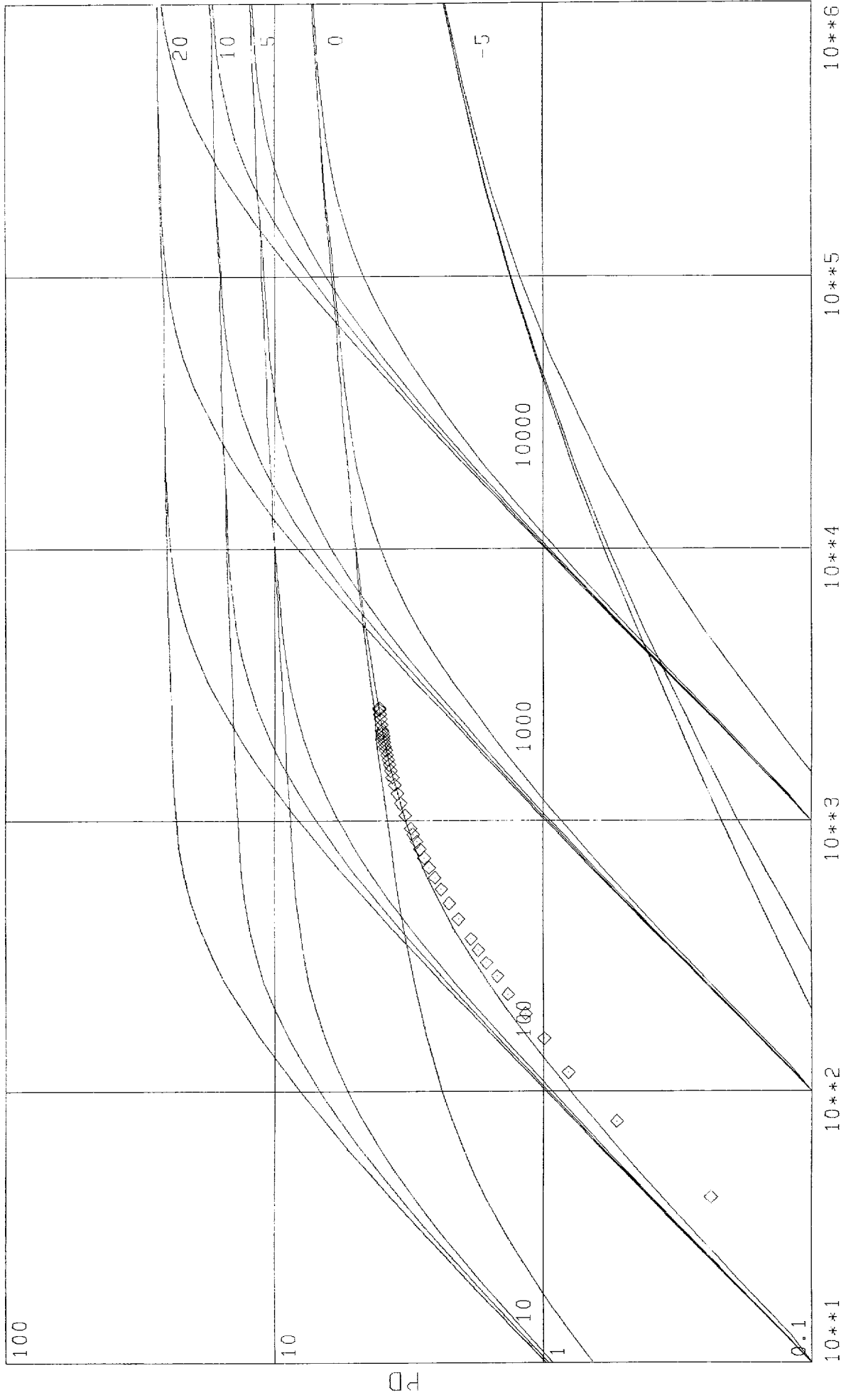
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8041



GAUGE NO 8041

CIP 1

TICKET NO 22306700

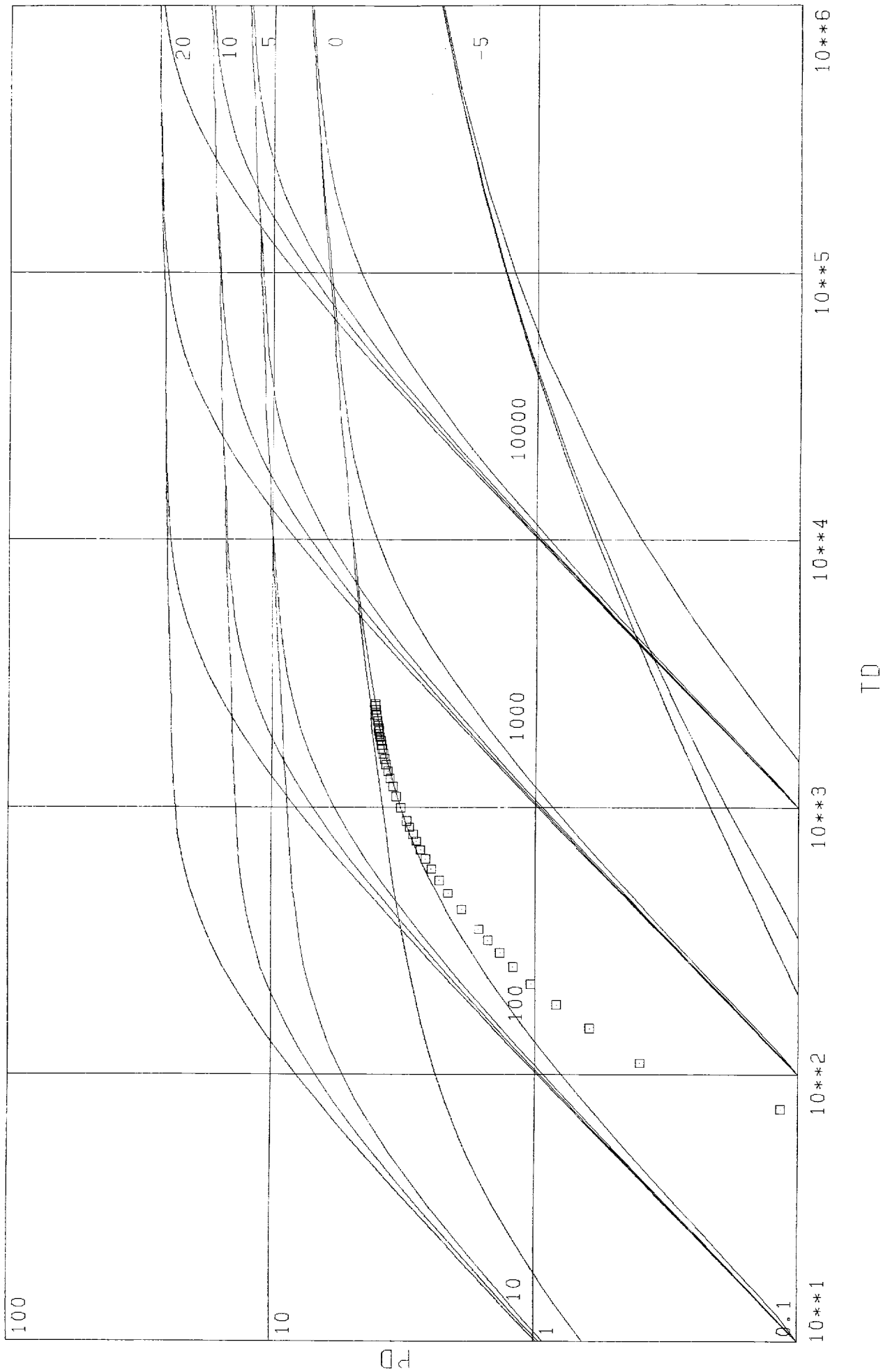


TD

GAUGE NO 8040

CIP 1

TICKET NO 22306700



SUMMARY OF RESERVOIR PARAMETERS

USING HORNER METHOD FOR LIQUID WELLS

OIL GRAVITY 41.2 °API@60°F WATER SALINITY 0.0 % SALT
 GAS GRAVITY 0.700 FLUID GRADIENT 0.3550 psi/ft
 GAS/OIL RATIO 379.5 SCF/STB FLUID PROPERTIES AT 1507.7 psig
 TEMPERATURE 143.0 °F VISCOSITY 0.726 cp
 NET PAY 8.0 ft FMT VOL FACTOR 1.233 Rvol/3vol
 POROSITY 10.0 % SYSTEM COMPRESSIBILITY 18.48 $\times 10^{-6}$ vol/vol/psi
 PIPE CAPACITY FACTORS 0.00492 0.01422 bbl/ft

GAUGE NUMBER		8041	8040					
GAUGE DEPTH		11227.0	11282.0					
FLOW AND CIP PERIOD		1	1					UNITS
FINAL FLOW PRESSURE	P_f	119.1	140.5					psig
TOTAL FLOW TIME	t	101.6	101.6					min
EXTRAPOLATED PRESSURE	P^*	1436.0	1507.7					psig
ONE CYCLE PRESSURE		1024.2	1097.4					psig
PRODUCTION RATE	Q	11.9	11.5					BPD
TRANSMISSIBILITY	kh/μ	5.8	5.6					md-ft cp
FLOW CAPACITY	kh	4.21782	4.06299					md-ft
PERMEABILITY	k	0.52723	0.50787					md
SKIN FACTOR	S	-0.4	-0.2					
DAMAGE RATIO	DR	0.9	0.9					
POTENTIAL RATE	Q_1	11.9	11.5					BPD
RADIUS OF INVESTIGATION	r_i	26.1	25.6					ft

REMARKS: THE RATE USED AS BASIS OF ANALYSIS WAS OBTAINED BY USING THE PRESSURE CHANGE METHOD FOR CALCULATING A PRODUCTION RATE. IT WAS ASSUMED THAT THE PRESSURE INCREASES DURING THE FIRST FLOW PERIOD WERE DUE TO OIL BEING PRODUCED INTO THE ANNULUS, FORCING THE MUD INTO THE TOOL STRING.

THE HORNER EXTRAPOLATION MAY BE SOMEWHAT IN ERROR DUE TO MARGINAL DEVELOPMENT OF THE FIRST CIP BUILDUP CURVE. IF THIS IS THE CASE, THE P^* VALUE WILL BE TOO HIGH AND THE SLOPE (M) WILL BE LESS THAN SHOWN. HOWEVER, THE CIP DATA WAS MATCHED ON THE RADIAL FLOW TYPE CURVE AND YIELDED RESULTS THAT WERE SIMILAR TO THE HORNER CALCULATIONS.

NOTICE:

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SUMMARY OF RESERVOIR PARAMETERS

USING CURVE MATCH METHOD FOR LIQUID WELLS

OIL GRAVITY 41.2 °API@60°F WATER SALINITY 0.0 % SALT
 GAS GRAVITY 0.700 FLUID GRADIENT 0.3550 psi/ft
 GAS/OIL RATIO 379.5 SCF/STB FLUID PROPERTIES AT 1507.7 psig
 TEMPERATURE 143.0 °F VISCOSITY 0.726 cp
 NET PAY 8.0 ft FMT VOL FACTOR 1.233 Rvol/Svol
 POROSITY 10.0 % SYSTEM COMPRESSIBILITY 18.48 $\times 10^{-6}$ vol/vol/psi
 PIPE CAPACITY FACTORS 0.00492 0.01422 bbl/ft

GAUGE NUMBER		8041	8040					
GAUGE DEPTH		11227.0	11282.0					
FLOW AND CIP PERIOD		1	1					UNITS
FINAL FLOW PRESSURE	P_f	119.1	140.5					psig
TOTAL FLOW TIME	t	101.6	101.6					min
PRODUCTION RATE	Q	11.9	11.5					BPD
t_d AT 1 HOUR		1522.	1446.					
P_d AT 100 psi		0.333	0.314					
C_d		76.0	283.7					
SKIN	S	0.0	0.0					
TRANSMISSIBILITY	kh/μ	6.9	6.3					$\frac{md-ft}{cp}$
FLOW CAPACITY	kh	5.02001	4.55284					md-ft
PERMEABILITY	k	0.62750	0.56911					md
DAMAGE RATIO	DR	1.0	1.0					
POTENTIAL RATE	Q_i	11.9	11.5					BPD
RADIUS OF INVESTIGATION	r_i	28.5	27.1					ft

REMARKS: -----SEE THE REMARKS SHOWN ON THE HORNER RESULTS PAGE-----

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