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appropriate district office
See Rule 401 & Rule 1122

State of New Mexico
Energy, Minerals and Natural Resources Department

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator OCEAN ENERGY, INC				Lease or Unit Name CARLISLE STATE COM			
Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 7-16-98		Well No. 1 Y	
Completion Date 7-22-96		Total Depth 12285		Plug Back TD 12240		Elevation	
Csg. Size 5 1/2		Wt. 20#		Set At 12285		Perforations: From: 12068 To: 12120	
Tbg. Size 2 7/8		Wt. 6.5		Set At 11961		Perforations: From: To:	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE				Packer Set At 11961		Formation	
Producing Thru TB6		Reservoir Temp. °F 183.8 @ 11961		Mean Annual Temp. °F 60		Baro. Press. - P. 15.2	
L 11961		II 11961		Gg 718		% CO ₂ 45.7	
				% N ₂ 8.28		% H ₂ S	
				Prover		Meter Run 4.026	
						Taps 116	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI										
1.	4 X	2.500	831	1.96	80	1606		PRR		7.2 NRS
2.	4 X	2.500	853	4.84	85	1542		"		1 NR
3.	4 X	2.500	976	22.09	85	1397		"		"
4.	4 X	2.500	911	35.44	87	1259		"		"
5.										"

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	32.64	410.68	844.2	.9813	1.180	1.102	1,694
2.	32.64	64.75	844.2	.9768	1.180	1.105	2,692
3.	32.64	140.15	885.2	.9768	1.180	1.108	5,842
4.	32.64	188.48	924.2	.9750	1.180	1.113	7,878
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	1.26	540	1.36	.863	A.P. I. Gravity of Liquid Hydrocarbons 58.0 @ 60°	Deg.
2.	1.29	545	1.37	.819	Specific Gravity Separator Gas .718	XXXXXXXXXX
3.	1.33	545	1.37	.814	Specific Gravity Flowing Fluid	XXXXXX
4.	2.38	547	1.38	.807	Critical Pressure 668	P.S.I.A. 666
5.					Critical Temperature 395	R 418

P _c 1619.3 P _c ² 2621.8				
NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²
1.		1591.4	2532.6	89.2
2.		1581.3	2500.5	121.3
3.		1541.9	2377.3	244.5
4.		1526.8	2331.2	290.6
5.				

$$1) \frac{P_c^2}{P_c^2 - P_w^2} = \underline{9.022} \quad (2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{9.022}$$

$$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = \underline{71.075}$$

Absolute Open Flow 71.075	Mcf/d @ 15.025	Angle of Slope θ 45	Slope, n 1.000
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Remarks: **WELL PRODUCED 18.0 BBL 58.0 API CONDENSATE.**

Approved By Division	Conducted By: METER & TESTING	Calculated By: BM	Checked By: BM
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