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appropriate district office.
See Rule 401 & Rule 1122

State of New Mexico
Energy Minerals and Natural Resources

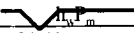
Form C-122
Revised October, 1999

Oil Conservation Division
2040 South Pacheco
Santa Fe, NM 87505

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator David H. Arrington Oil & Gas, Inc.						Lease or Unit Name Mayfly "14" State Com					
Type Test ☒ Initial ☐ Annual ☐ Special						Test Date June 16, 2000			Well No. #1		
Completion Date		Total Depth 12,479'		Plug Back TD		Elevation			Unit Ltr. - Sec. - TWP - Rge. D 14-16-35		
Csg. Size 5 1/2	Wt. 17#	d	Set At	Perforations: From: 11,884' To: 11,907'			County Lea County				
Thg. Size 2 7/8	Wt. 4.7	d	Set At 1,995 11,924'	Perforations: From: To:			Pool				
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At 11,924			Formation Mudstone		
Producing Thru Tubing		Reservoir Temp. °F		Mean Annual Temp. °F 60		Baro. Press - P _a 13.2			Connection		
L 11,924'	H 11,924'	Gg 814	%CO ₂ .424	%N ₂ 1.134	%H ₂ S	Prover		Meter Run 4.026	Taps FLG		

FLOW DATA						TUBING DATA		CASING DATA		Duration Of Flow
No.	Prover Line Size	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI						1500		Packer		24 hrs.
1.	4 x 2.500		163	98.00	86	734		11		24 hrs.
2.										
3.										
4.										
5.										

RATE OF FLOW CALCULATIONS							
No.	COEFFICIENT (24 HOUR)		Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg.	Super Compress. Factor, F pv.	Rate of Flow Q, Mcfd
1.	32.64	131.41	176.2	.9759	1.108	1.023	4.745
2.							
3.							
4.							

No.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	.26	546	1.28	.956	71.894	
2.					A. P. I. Gravity of Liquid Hydrocarbons 70.0	Deg.
3.					Specific Gravity Separator Gas 814	XXXXXXXXXX
4.					Specific Gravity Flowing Fluid XXXXX	6 min = 848
5.					Critical Pressure *664 P.S.I.A. 664	P.S.I.A.
					Critical Temperature *425	R 438 R

P _c 1513.2		P _c ² 2289.8	
No.	P _i ²	P _w	P _w ²
1.		1148.1	1318.1
2.			
3.			
4.			
5.			

(1) $P_c^2 = 2.356$

$\frac{P_c^2 - P_w^2}{P_c^2 - P_w^2}$

AOF = Q

$\frac{P_c^2}{P_c^2 - P_w^2} = 11.179$

(2) $P_c^2 = 2.356$

$\frac{P_c^2}{P_c^2 - P_w^2}$

Absolute Open Flow 11,179 Mcfd@ 15.025		Angle of Slope θ: 45	Slope, n: 1.000
Remarks: Well produced 66.0 Bbbls 70 GR - Condensate *Corrected to 1.134% Nz			
Approved By Division	Conducted By: Metering & Testing	Calculated By: BM	Checked By: BM

