Submit in duplicate to appropriate district office.
See Rule 401 & Rule 1122

30-025-35111

State of New Mexico
Energy Minerals and Natural Resources

Oil Conservation Division
1220 South St. Francis Dr.
Santa Fe, NM 87504

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OCD - ARTESIA

Form C-122
Revised October, 1999

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator: E.O.G. Resources Inc.							Lease or Unit Name: Bullwinkle				
Type Test: [X] Initial [ ] Annual [ ] Special							Test Date:			Well No.: 1	
Completion Date:		Total Depth:		Plug Back TD:			Elevation:			Unit Ltr. - Sec. - TWP - Rge.: V 6 16 35	
Csg. Size: 5½	Wt.: 17	d:	Set At: 13075	Perforations: From: 12588 To: 12614						County: ~~Eddy~~ Lea	
Tbg. Size: 2 7/8	Wt.: 6.5	d: 2.441	Set At: 12525	Perforations: From: To:						Pool:	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple: Single				Packer Set At: 12458						Formation: ~~Atoka~~	
Producing Thru: Tbg	Reservoir Temp. °F		Mean Annual Temp. °F: 60	Baro. Press - P_a: 13.2						Connection:	
L: 12525	H: 12525	Gg: .699	%CO_2: .817	%N_2: 1.870	%H_2S:	Prover:	Meter Run: 2"	Taps: Flg			

FLOW DATA					TUBING DATA		CASING DATA		
No.	Prover Line Size X Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration Of Flow
SI					3089		Pkr		48 Hrs
1.	2 X	376		56	2799		Pkr		1 Hr
2.	2 X	376		57	2531		Pkr		1 Hr
3.	2 X	378		57	2417		Pkr		1 Hr
4.	2 X	379		58	2100		Pkr		1 Hr
5.									

RATE OF FLOW CALCULATIONS

No.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg.	Super Compress. Factor, Fpv.	Rate of Flow Q, Mcfd
1.		Total Flow Meter					451
2.							633
3.							1084
4.							1480
5.							

No.	P_r	Temp. °R	T_r	Z
1.				
2.				
3.		N/A		
4.				
5.				

Gas Liquid Hydrocarbon Ratio 9.048 Mcf/bbl.
A. P. I. Gravity of Liquid Hydrocarbons 42.8 @ 60 Deg.
Specific Gravity Separator Gas .699 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX G Mix=1.036
Critical Pressure *668 P.S.I.A. 655 P.S.I.A.
Critical Temperature *385 R. 500 R

P_c 3102.2 P_c^2 9623.6

No.	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1.		2812.8	7911.9	1711.7
2.		2545.4	6479.2	3144.4
3.		2433.9	5923.7	3699.9
4.		2120.2	4495.4	5128.2
5.				

(1) $\frac{P_c^2}{P_c^2 - P_w^2}$ = 1.877 (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n$ = 1.877

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n$ = 2.777

Absolute Open Flow 2,777 Mcfd@ 15.025 Angle of Slope θ: 45 Slope, n: 1,000

Remarks: * = Corrected to 1.870% N2

Approved By Division	Conducted By:	Calculated By:	Checked By:
	HRC Petroleum Svc	BM	BM