## NEW MEXICO OIL CONSERVATION COMMISSION

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		Wt. 4.	L•U•	<b>1.995</b> S	et at <u>1</u>	5430 Pe Nix	rf. Open	ended	_To	
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ate of	Comple	tion:	11/8/61	Packe	er <u>13</u> ,(	200	Reserve	pir Temp.	160%	
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ested T	h <b>roug</b> h	(Prove	<u>r) (Chok</u>	e) (Meter)	) (Meter)			Type Taps Plange		
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•	(24-Hour				Fac	tor	Factor Fact		or Q-MCFPD	
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vity of	Liqui	d Hydrod		53	cf/bbl. deg.		Speci: Speci:	fic Gravit fic Gravit	ty Separa ty Flowir	tor Gas <u>0.</u> ng Fluid <u>0.7</u>
	9.936	8 = 0.7	(1-e <sup>-5</sup>	) 0.517	4		Pc	4366.2	P <sup>2</sup> 19	.064
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	ps1a)	263.4	175.3	307.3	(1.	-e <sup>-s</sup> ) 9.0	422.4	18,642	P. 649.9	P. 0.1488
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IPANY DRESS	Pan A	Hobh	Petrolen	n Cerpera	Elon					
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Low productivity necessitated one-point test at delivery pressure. Well produced (a bbls. distillate during 24 hour test. Slope assumed 1.000.

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- Q = Actual rate of flow at end of flow period at W. H. working pressure ( $P_W$ ). MCF/da. @ 15.025 psia and 60° F.
- P<sub>c</sub>= 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- PwT Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw Differential meter pressure, inches water.
- FgI Gravity correction factor.
- $F_t$  Flowing temperature correction factor.
- F<sub>pv</sub>: Supercompressability factor.
- n I Slope of back pressure curve.
- Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .