

## NEW MEXICO OIL CONSERVATION COMMISSION

Form C-122

## MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Revised 12-1-55

Pool South Vacuum Formation McKee County Lea  
Initial X Annual \_\_\_\_\_ Special \_\_\_\_\_ Date of Test 10-27-58  
Company The Pure Oil Company Lease South Vacuum Unit Well No. 2-35  
Unit I Sec. 35 Twp. 18-S Rge. 35-E Purchaser Phillips Petroleum Company  
Liner 5" Wt. 17.93 I.D. 4.276 Set at 13881 Perf. 13620 To 13823  
Tubing 2 Wt. 4.70 I.D. 1.995 Set at 13622 Perf. Open Ended To \_\_\_\_\_  
Gas Pay: From 13620 To 13823 L 13722 xG 0.601 -GL 11000 Bar.Press. 30.18" Hg.  
Producing Thru: Casing \_\_\_\_\_ Tubing X Type Well G. O. Dual  
Date of Completion: 9-28-58 Packer Quiberson Hookwall Reservoir Temp. 200° F 165° F

## OBSERVED DATA

Tested Through Quiberson (Globe) (Meter)Type Taps Flange

No.	Flow Data					Tubing Data		Casing Data		Duration of Flow Hr.
	(Prover) (Line) Size	(Choke) (Orifice) Size	Press. psig	Diff. h <sub>w</sub>	Temp. °F.	Press. psig	Temp. °F.	Press. psig	Temp. °F.	
SI						3498	78	Packer		64
1.	4.026	2.000	26	11	44	368	76			9
2.	4.026	2.000	26	11	44	211	76			3
3.	4.026	2.000	26	11	45	110	75			3
4.	4.026	2.000	26	11	45	82	75			3
5.	4.026	2.000	26	11	44	53	75			24

## FLOW CALCULATIONS

No.	Coefficient (24-Hour)	$\sqrt{h_w P_f}$	Pressure psia	Flow Temp. Factor F <sub>t</sub>	Gravity Factor F <sub>g</sub>	Compress. Factor F <sub>pv</sub>	Rate of Flow Q-MCFPD @ 15.025 psia
1.	25.580	20.8	44.392	1.0157	0.9325		502.0
2.	25.580	20.8	26.392	1.0157	0.9325		502.0
3.	25.580	20.8	26.392	1.0157	0.9325		502.0
4.	25.580	20.8	26.392	1.0157	0.9325		502.0
5.	25.580	20.8	26.392	1.0157	0.9325		502.0

## PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio 22,300 cf/bbl.  
Gravity of Liquid Hydrocarbons 56.3 @ 60 deg.  
F<sub>c</sub> 9.936 (1-e<sup>-s</sup>) 0.570

Specific Gravity Separator Gas 0.688  
Specific Gravity Flowing Fluid 0.801  
P<sub>c</sub> 3498 P<sub>c</sub><sup>2</sup> 1223600  
3511 12,329

No.	P <sub>w</sub> P <sub>t</sub> (psia)	P <sub>t</sub> <sup>2</sup>	F <sub>c</sub> Q	(F <sub>c</sub> Q) <sup>2</sup>	(F <sub>c</sub> Q) <sup>2</sup> (1-e <sup>-s</sup> )	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>	Cal. P <sub>w</sub>	P <sub>w</sub> P <sub>c</sub>
1.	368 381.2	135.2	4975.498	24.75 24.88	12.10 14.18	148.34 9.38	12088	384.5	10.72
2.	211 224.2	46.0	4975	24.75	13.10	57.64 4.48	12178	240.0	6.85
3.	110 125.2	15.6	4975	24.75	13.10	25.22 9.36	12211	158.0	4.51
4.	82 85.2	7.06	4975	24.75	13.10	19.84 23.26	12216	141.0	4.04
5.	53 60.2	4.38	4975	24.75	13.10	15.91 18.32	12220	126.0	3.61

Absolute Potential: 502 MCFPD; n = 00COMPANY The Pure Oil CompanyADDRESS Box 2107, Fort Worth, TexasAGENT and TITLE L.M. Williams Production EngineerWITNESSED H. J. LittlejohnCOMPANY The Pure Oil Company

REMARKS

EXHIBIT A

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

$Q$  = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.

$P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia

$P_w$  = Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia

$P_t$  = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia

$P_f$  = Meter pressure, psia.

$h_w$  = Differential meter pressure, inches water.

$F_g$  = Gravity correction factor.

$F_t$  = Flowing temperature correction factor.

$F_{pv}$  = Supercompressibility factor.

$n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .