								•	. .	90 90 1		FORM U-1 2 5d 10 -1- 5	
				MULTI	E-POINT I	BACK PRE	SSURE T	EST FOR	s Wells		Revise	30 14-1-)	
Poo	l Lust	(Morr	.om)	F	Formation Morrow				County Lea				
Initial X Annual Special Date of Test August 21.												21.1.96	
					Texaco - Cities Lease Service State					· · · · · · · · · · · · · · · · · · ·			
Unit <u>G</u> Sec. <u>32</u> Twp. <u>19-S</u> Rge. <u>32-E</u> Purchaser <u>None</u> Casing <u>2-7/8</u> Wt. <u>6.50</u> I.D. <u>2.441</u> Set at <u>12.987</u> Perf. <u>12.332</u> To <u>12.388</u>													
Tubing None Wt. I.D. Set at Perf. To													
Gas Pay: From 12,332 To 12,388 L 12,332 xG.675 _GL8324 Bar.Press. 13.													
	Producing Thru: Casing X Tubing Type Well Dual G. O. Single-Bradenhead-G. G. or G.O. Dual												
Data	Date of Completion: July 16, 1964 Packer Single-Bradenhead-G. G. or G.O. Dual Reservoir Temp.												
Day	c or compre	01011. <u>0</u>	<u> </u>	<u></u>	ou racke				orr remb.				
							ED DATA	4					
Tes	ted Through	Pra	weekr) Ku	Olifok k)	(Meter)	<u>-</u>			Type Tar	os <u>Fla</u>	ange		
	Flow Data			ata	Tubi			ng Data	Casing I	Data			
	XXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXXX	(XX	dk/ex	Press	. Diff.	Temp.	Press		Press.		I	Duration	
No.	, ,				1	o _F .		0,		277		of Flow	
	Size	5.	ıze	psig	h _w	F.	ps1g	°F.	psig	F.		Hr.	
SI		1 7 7	00	25	1200	100	 		00/0	- 70		72	
1. 2.	3.008	1.500		65 12.0 93 23.0		102			2960 2683	79 79			
<u>3.</u>	11	11	11		39.0	102	 		2303	79		1	
4.	11	11		134	57.0	93			1902	80		i	
5.													
TT OUT OUT I TO TO TO													
	Coefficient				ressure	Flow CAL	CULATIONS Temp. Gravity		Compress.		Rate of Flow		
No.	00011101	LCIIU		1.	ressure		tor	Factor			Q-MC		
	(24-Hour)		$\sqrt{h_{w}}$) f	psia	,		Fg	Fpv		@ 15.025 p		
-			30.6		78.2				- Pv				
1. 2. 3.			49.4		06.2	.961 .960		.9427		+	398.8		
$\frac{3}{3}$	14.36				23.2	-961		11	1.00	10	642.6 910.9		
4.					47.2	969		ff	1.01		1217	•7	
Д. 5.													
					PR	ESSURE C	ALCULAT	'IONS					
_													
	Liquid Hydro				<u>v</u>	cf/bbl.		Spec	ific Gravi	ty Sepa	rator	Gas675	
	ity of Liqui	га нуаг	rocarbo 1	ons L-e ^{-s})	- 12/	deg.		Spec	ific Gravi	ty Flow	ing Fi	.uid	
c	5.866		(_	L-e 3/	. 436)		Pc	3916.2	_ ^P c̃_ 15 ,	337		
	$P_{\mathbf{w}}$,		^		2		2 0				
No.	_	Pt	F	,Q	$(F_cQ)^2$	(F	cQ) ² -e ^{-s})	$P_{\mathbf{w}}^2$	$P_c^2 - P_w^2$	Ca	Į.	$P_{\mathbf{W}}$	
	Pt (psia)	<u> </u>						•		P	w_	Pw Pc	
1. 2.	2973.2	8840			5.471	2.3		8842	6495	2974		7594	
۲۰	2696.2	7269				6.191		7275	8062	2697		6887	
2• 1	2316.2				28.55	12.		5377	9960	2319		5921	
3. 4. 5.	1915.2	1915.2 3668		39	50.96	22.	22	3690	1,647	1921		1905	
_	.7	• - 3					<u> </u>		 				
Absolute Potential: 1600 MCFPD; n 1.00													
COMPANY TEXACO Inc. ADDRESS Box 1270 Hidland. Texas													
	IT and TITLE					t Supp	rvisor	(Gas)	5 m. 7	ner			
	NESSED				<u></u>	- <u> </u>	·- • • • · · · · · · · · · · · · · · · ·	<u>1</u>	* ************************************				
COME	PANY												

REMARKS

INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

- Q I Actual rate of flow at end of flow period at W. H. working pressure ($P_{\rm W}$). MCF/da. @ 15.025 psia and 60° F.
- PcI 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- PwT Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) ps:a
- P_{t} Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw Differential meter pressure, inches water.
- FgI Gravity correction factor.
- F_t Flowing temperature correction factor.
- Fpw Supercompressability factor.
- n I Slope of back pressure curve.
- Note: If $F_{\rm W}$ cannot be taken because of manner of completion or condition of well, then $P_{\rm W}$ must be calculated by adding the pressure trop due to friction within the flow string to $P_{\rm t}$.