

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

DUPLICATE

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 4-11-66	
Company BENZOL COMPANY			Connection NONE		
Pool UNDESIGNATED			Formation MORROW		Unit
Completion Date 4-11-66		Total Depth 12150		Plug Back TD -	Elevation 4062' RB
Farm or Lease Name BRIDGES STATE					
Csg. Size 7"	Wt. 20	d 6.184	Set At 12150	Perforations: From 11060 To 11070	
Well No. No. 1					
Tbg. Size 2 3/8	Wt. 4.7	d 1.995	Set At 11911	Perforations: From OPEN To ENDED	
Unit Sec. Twp. Rge. 1 11 17S 34E					
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE				Packer Set At 11900'	
County LEA					
Producing Thru TBG		Reservoir Temp. °F 176 @ 11850		Mean Annual Temp. °F 60	
Baro. Press. - P _a 13.2		State NEW MEXICO			
L 11911	H	G _g .669	% CO ₂ 0.29	% N ₂ 0.40	% H ₂ S 0.00
Prover		Meter Run 3"		Taps FLANGE	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Flow
SI							4770	70	PKP		82
1.	3 x 1.500			600	22	68	2778	80	-	-	4.00
2.	3 x 1.500			600	37	75	2174	80	-	-	2.25
3.	3 x 1.500			620	44	82	1836	76	-	-	1.75
4.	3 x 1.500			600	59	84	1397	76	-	-	2.0
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	11.13	131.05	613.2	.9924	1.223	1.061	1878.3
2	11.13	150.63	613.2	.9850	1.223	1.058	2128.7
3	11.13	166.91	633.2	.9795	1.223	1.056	2350.0
4	11.13	190.20	613.2	.9777	1.223	1.055	2670.4
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	.91	528	1.41	.888	A.P.I. Gravity of Liquid Hydrocarbons	48.6
2.	.91	535	1.43	.893	Specific Gravity Separator Gas	.669
3.	.91	542	1.45	.896	Specific Gravity Flowing Fluid	X X X X X
4.	.91	544	1.45	.898	Critical Pressure	673 P.S.I.A.
5.					Critical Temperature	374 R

NO.	P _c	P _w	P _r	P _c ²	P _w ²	P _r ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.157$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.152$
1		4242.2	1796.3	1796.3	273.531				
2		3640.2	1325.1	1325.1	175.582				
3		3171.2	1005.5	1005.5	101.109				
4		2480.2	615.1	615.1	378.080				
5									

Absolute Open Flow				3154 Mcfd @ 15.025		Angle of Slope θ		Slope, n	
								.97	
Remarks:									
Approved By Commission:			Conducted By: COLEMAN PETE. ENGR. CO.			Calculated By: JOE A. COLEMAN		Checked By: JOE A. COLEMAN	

SECOND STAGE RATE OF FLOW CALCULATIONS 2 x 4 OMT							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	71.93	-	10"	9913	9468	-	66.8
2	71.93	-	10"	9913	9468	-	66.8
3	71.93	-	10"	9850	9468	-	67.1
4	71.93	-	10"	9850	9468	-	67.1
5.							