

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 10-11-77	
Company AMOCO PRODUCTION COMPANY				Connection EL PASO NATURAL GAS COMP	
Pool LUSK MORRON				Formation MORRON GAS	
Completion Date 9-27-77		Total Depth 12957.		Plug Back TD 12907.	
Elevation 3621.		Form or Lease Name State DR			
Csg. Size 5.500	Id. 15.5	d 4.950	Set At 12957.	Perforations: From 12603. To 12831.	
Thq. Size 2.375	Id. 4.7	d 1.905	Set At 12486.	Perforations: From 0. To 0.	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple PERES				Packer Set At 12472.	
Producing Thru TUBING		Reservoir Temp. °F 177.0 12885.		Mean Annual Temp. °F 58.0	
Baro. Press. - P ₀ 13.2		State NEW MEXICO			
L 12885.	H 12885.	G _g 0.655	% CO ₂ 0.63	% N ₂ 0.52	% H ₂ S 0.
Prover 0.		Meter Run 4.0		Taps FLANGE	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
Sl											
1.	4.00	X	2.000	534.	6.8	88.	3973.	55.			464.0
2.	4.00	X	2.000	534.	16.0	86.	3624.	66.	0.	0.	1.0
3.	4.00	X	2.000	542.	32.5	76.	3464.	66.	0.	0.	1.0
4.	4.00	X	2.000	542.	57.8	67.	3258.	66.	0.	0.	1.0
5.							3025.	65.	0.	0.	1.0

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	19.83	60.82	547.2	0.9741	1.2356	1.0469	1520.
2.	19.83	93.57	547.2	0.9759	1.2356	1.0476	2344.
3.	19.83	134.31	555.2	0.9850	1.2356	1.0517	3410.
4.	19.83	179.08	555.2	0.9933	1.2356	1.0548	4595.
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ 19.8 _____ Mcf/bbl.
1.	0.81	548.	1.47	0.912	A.P.I. Gravity of Liquid Hydrocarbons _____ 53.9 _____ Deg.
2.	0.81	546.	1.46	0.911	Specific Gravity Separator Gas _____ 0.655 _____
3.	0.83	536.	1.44	0.904	Specific Gravity Flowing Fluid _____ X X X X X _____
4.	0.83	527.	1.41	0.899	Critical Pressure _____ 672. _____ P.S.I.A. _____ 605. _____ P.S.I.A.
5.					Critical Temperature _____ 373. _____ R _____ 414. _____ R

P_r 4000.3 P_w 16002.

NO.	P _r ²	P _w ²	P _r ² - P _w ²
1	3229.	3544.	13280.
2	2091.	3503.	12274.
3	10701.	3334.	11115.
4	9231.	3162.	10001.
5			

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.6664$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.6664$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 12261.$

Absolute Open Flow _____ 12261. _____ Mcfd @ 15.025 Angle of Slope _____ 45.0 Slope, n _____ 0.00

Remarks: _____

Approved By: _____	Conducted By: John West Engineering	Calculated By: DJC (AMOCO)	Checked By: RMB (AMOCO)
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RECEIVED

JAN 20 1978

GIL CONSERVATION COMM.
HOBBS, N. M.