

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 2-26-81			
Company Amoco Production Company				Connection Gas Company of New Mexico					
Pool Buffalo				Formation Penn				Unit	
Completion Date 8 6 80		Total Depth 13700		Plug Back TD 13653		Elevation 3696		Farm or Lease Name Nellis Federal <i>Gas Com</i>	
Csg. Size 5.500	Wt. 17.0	d 4.778	Set At 13700	Perforations: From 13552 To 13620		Well No. 1			
Tbg. Size 2.375	Wt. 4.7	d 1.995	Set At 13410	Perforations: From 0 To 0		Unit H	Sec. 188	Twp. 19S	Rge. 33E
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 13341		County Lea			
Producing Thru Tubing		Reservoir Temp. °F 178 @ 13586		Mean Annual Temp. °F 60.0		Baro. Press. - P _g 13.2		State New Mexico	
L 13586	H 13586	G _g 0.664	% CO ₂ 0.70	% N ₂ 0.59	% H ₂ S 0	Prover 0	Meter Run 4.0	Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							3728	56			46.5
1.	4.00 x 2.250			436	5.3	73	3398	61	0	0	1.0
2.	4.00 x 2.250			449	17.6	75	2900	66	0	0	1.0
3.	4.00 x 2.250			484	29.2	75	2472	73	0	0	1.0
4.	4.00 x 2.250			512	45.6	75	1871	73	0	0	1.0
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	25.68	48.75	449.2	0.9877	1.2268	1.0435	1583
2	25.68	90.30	462.2	0.9859	1.2268	1.0443	2929
3	25.68	120.41	497.2	0.9859	1.2268	1.0477	3919
4	25.68	154.69	525.2	0.9859	1.2268	1.0504	5048
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio <u>17.2</u> Mcf/bbl.
1.	0.67	533.	1.42	0.918	A.P.I. Gravity of Liquid Hydrocarbons <u>55.0</u> Deg.
2.	0.69	535.	1.42	0.917	Specific Gravity Separator Gas <u>0.664</u> X X X X X X X X
3.	0.74	535.	1.42	0.911	Specific Gravity Flowing Fluid <u>X X X X X</u> 0.814
4.	0.78	535.	1.42	0.906	Critical Pressure <u>671.</u> P.S.I.A. 664. P.S.I.A.
5.					Critical Temperature <u>376.</u> R 423. R

P _c <u>3754.6</u> P _c ² <u>14097</u>						
NO.	P _r ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.4283$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.3330$
1	11636.	3431.	11770.	2326.	$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 6729.$	
2	8487.	2965.	8790.	5306.		
3	6176.	2570.	6605.	7492.		
4	3550.	2056.	4227.	9870.		
5						

Absolute Open Flow <u>6729.</u> Mcfd @ 15.025	Angle of Slope θ <u>51.1</u>	Slope, n <u>0.806</u>
Remarks:		

Approved By <i>Signed by</i> Jerry S. <i>Supr.</i> Dist. L. <i>Supr.</i>	Conducted By: John West Eng.	Calculated By: Chris Van Doren	Checked By: Larry Sheppard
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