

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 5-12-72							
Company TEXACO Inc.				Connection							
Pool Hartb Vacuum Morrow				Formation Morrow							
Completion Date		Total Depth 12,500		Plug Back TD 12,500							
				Elevation 4001							
Farm or Lease Name N. Mexico DK State											
Csg. Size 4.5	Wt. 11.6	Set At 12,500	Perforations: From 11,485 To 11,856								
Thg. Size 2.375	Wt. 4.5	Set At 12,410	Perforations: From To								
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 11,410							
Producing Thru Tubing		Reservoir Temp. °F 165 @ 12,410		Mean Annual Temp. °F 60							
				Baro. Press. - P _a 13.2							
L 11,630	H 11,670	Gg 0.638	% CO ₂ 0.32	% N ₂ 0.80	% H ₂ S 0.0						
				Prover	Meter Run 4.026						
				Taps Flange							
FLOW DATA											
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI							4856				30 hrs.
1.	4 x 1.5			256.0	16.2	70	4565	60			1 hr.
2.	4 x 1.5			266.5	25.9	63	4384	60			1 hr.
3.	4 x 1.5			266.5	43.2	65	4145	60			1 hr.
4.	4 x 1.5			641.7	40.5	63	3551	60			1 hr.
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super. Compress. Factor, Fpv	Rate of Flow Q, Mcfd				
1	10.84	66.1	269.2	.9905	1.252	1.025	955				
2	10.84	85.1	279.7	.9971	1.252	1.026	1240				
3	10.84	110.0	279.7	.9952	1.252	1.026	1599				
4	10.84	162.9	654.9	.9971	1.252	1.062	2456				
5											
NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio 13.5 Mcf/bbl.						
					A.P.I. Gravity of Liquid Hydrocarbons 43.2 Deg.						
1.	0.40	530	1.45	0.953	Specific Gravity Separator Gas 0.638	XXXXXXX					
2.	0.42	523	1.43	0.949	Specific Gravity Flowing Fluid XXXXX	0.871					
3.	0.42	525	1.43	0.950	Critical Pressure 670 P.S.I.A.	658 P.S.I.A.					
4.	0.98	523	1.43	0.886	Critical Temperature 366 °R	433 °R					
5.											
P _c 4869 P _c ² 23709.1					(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 2.127$						
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.678$						
1	20960	4584	21015	2694	AGF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 4121$						
2	19335	4407	19422	4287							
3	17366	4183	17501	6208							
4	12704	3603	12981	10728							
5											
Absolute Open Flow 4121 Mcfd @ 15.025					Angle of Slope θ 55.6		Slope, n .686				
Remarks: Calculated by computer											
Approved By Commission:		Conducted By:		Calculated By:		Checked By:					

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OL CONSERVATION DIV.
WASH. D.C.