

**NEW XICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL**

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 12-21-72			
Company TEXACO Inc.				Connection None					
Pool Vacuum Morrow North				Formation Morrow				Unit J	
Completion Date 12-21-72		Total Depth 12515		Plug Back TD 12447		Elevation 3991		Farm or Lease Name N. M. "DN" State	
Csg. Size 4 1/2	Wt. 13.5	d 3.92	Set At 12515	Perforations: From 11.550 To 12066			Well No. 1		
Thq. Size 2 3/8	Wt. 4.7	d 1.995	Set At 11490	Perforations: From To 			Unit J Sec. 18 Twp. 17 Rge. 35		
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 11490		County Lea			
Producing Thru Tubing		Reservoir Temp. °F 173 @ 11808		Mean Annual Temp. °F 60°		Baro. Press. - P _a 13.2		State New Mexico	
L 11808	H 11808	G _g 0.731	% CO ₂ 0.500	% N ₂ 1.990	% H ₂ S 0.0	Prover	Meter Run 4"	Taps Flange	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							4149	60			
1.	4 x 2.00			202.2	4.8	65	4004	68			1 hr.
2.	4 x 2.000			360.6	7.8	65	3832	74			1 hr.
3.	4 x 2.000			423.0	10.2	65	3677	77			1 hr.
4.	4 x 2.000			784.9	10.2	65	3466	78			1 hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	19.810	32.3	215.4	0.9952	1.170	1.008	823
2	19.810	54.1	373.8	0.9952	1.170	1.011	1384
3	19.810	66.8	436.2	0.9952	1.170	1.013	1712
4	19.810	90.4	798.1	0.9952	1.170	1.028	2351
5							

NO.	P _t	Temp. °R	T _t	Z	Gas Liquid Hydrocarbon Ratio 6.8 Mcf/bbl.
1.	0.33	525	0.96	0.985	A.P.I. Gravity of Liquid Hydrocarbons 43.0 Deg.
2.	0.57	525	0.96	0.978	Specific Gravity Separator Gas 0.731 X X X X X X X X
3.	0.66	525	0.96	0.975	Specific Gravity Flowing Fluid X X X X X 1.165
4.	1.21	525	0.96	0.946	Critical Pressure 663 P.S.I.A. 658 P.S.I.A.
5.					Critical Temperature 387 R 544 R

P _c 4162 P _c ² 17324				(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{17323.9}{5158.6}$		(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.364$	
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²			
1	16138	4020	16163	1161			
2	14786	3859	14890	2434			
3	13618	3713	13783	3541			
4	12105	3525	12426	4898			
5							

Absolute Open Flow 5556 Mcfd @ 15.025				Angle of Slope θ 54.6		Slope, n 0.710	
Remarks:							

Approved By Commission:	Conducted By: Lee	Calculated By: Computer	Checked By:
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