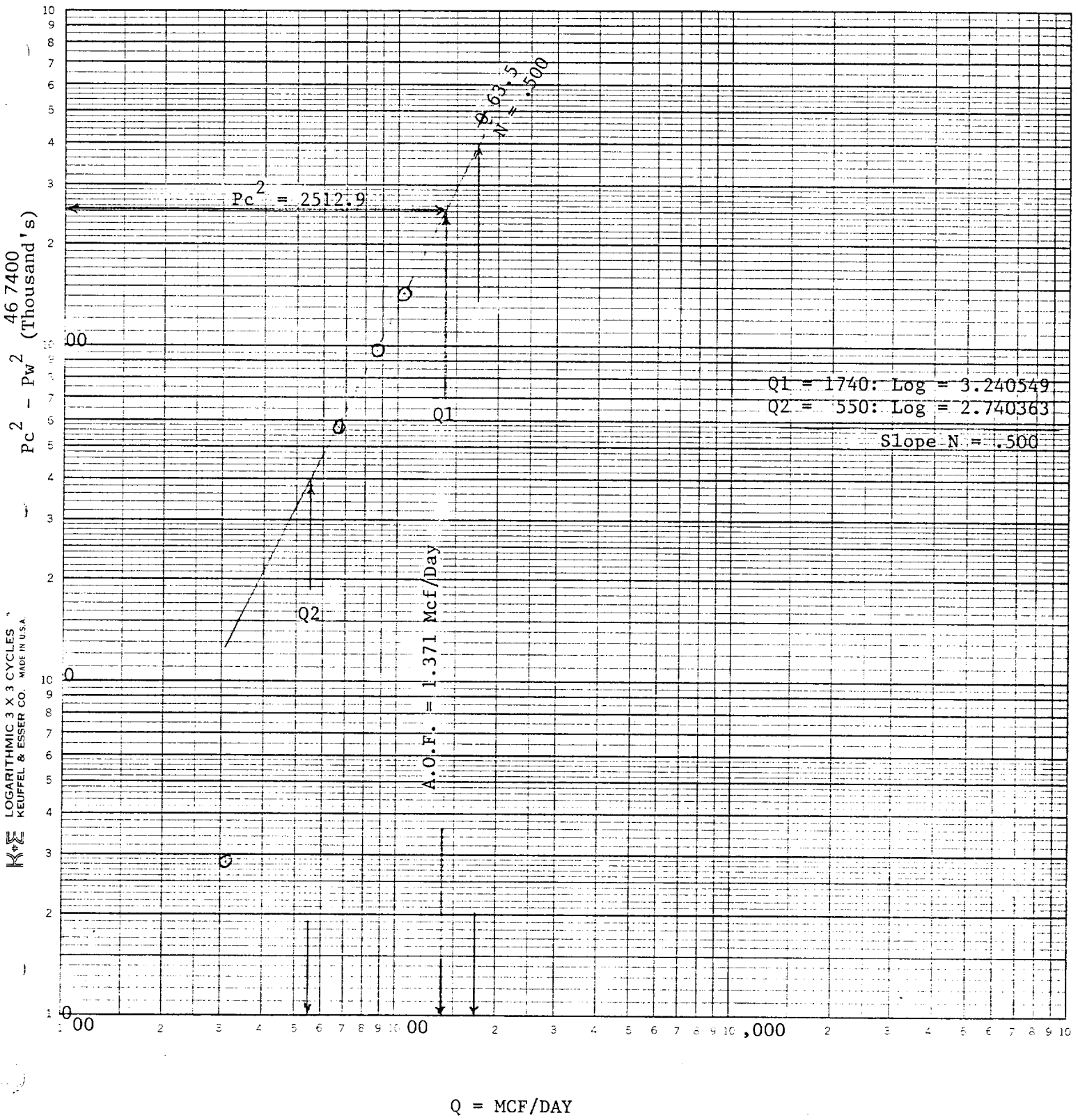


Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 3-3-88	
Company C.W. Trainer			Connection Llano		
Pool Undesignated N. Vacuum			Formation Atoka		Unit
Completion Date 2-20-88		Total Depth 12,150'		Plug Back TD 12121	Elevation 3984.3
Farm or Lease Name Betty State					
Csq. Size 5 1/2"	Wt. 17#	d 4.892	Set At 12150	Perforations: From 12006 To 12021	
Well No. 1					
Tbg. Size 2 7/8"	Wt. 6.5#	d 2.441	Set At 11957	Perforations: From Open-Ended	
Unit L		Soc. 16	Twp. 17-S	Rge. 35E	
Type Well - Single - Bradenhead - G.C. or G.O. Multiple Single				Packer Set At 11922	
County Lea					
Producing Thru Tubing		Reservoir Temp. °F 194° @ 11955		Mean Annual Temp. °F 60°	
Baro. Press. - P _a 13.2		State N.M.			
L 11957	H 11957	Gg .633	% CO ₂ 0.397	% N ₂ 0.781	% H ₂ S
Prover		Meter Run 3.068		Taps Flange	
FLOW DATA					
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w
SI					Temp. °F
1.	3	X	1.000	585	4.00
2.	3	X	1.000	600	20.00
3.	3	X	1.000	585	34.00
4.	3	X	1.000	585	46.00
5.					
TUBING DATA					
				Press. p.s.i.g.	Temp. °F
				1572	
				1444	
				1278	
				1117	
				870	
CASING DATA					
				Press. p.s.i.g.	Temp. °F
				PKR	CHOKE
					6/64
					9/64
					11/64
					14/64
RATE OF FLOW CALCULATIONS					
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg
					Super Compress. Factor, Fpv
					Rate of Flow Q, Mcfd
1	4.789	48.92	59	.9962	1.257
2	4.789	110.74	613.2	.9535	1.257
3	4.789	142.61	598.2	.9619	1.257
4	4.789	165.88	598.2	.9786	1.257
5					
Gas Liquid Hydrocarbon Ratio No Fluid Mcf/bbl.					
A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.					
Specific Gravity Separator Gas .633 X X X X X X X X					
Specific Gravity Flowing Fluid X X X X X					
Critical Pressure 670 P.S.I.A.					
Critical Temperature 368 °R					
P _c 1585.2 P _c ² 2512.9					
NO.	P _c ²	P _w	R _w ²	P _c ² - R _w ²	
1	2256.2	1576.2	2484.4	28.5	(1) $\frac{P_c^2}{P_c^2 - R_w^2} = 1.772$
2	2101.2	1405.2	1974.6	538.3	(2) $\left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n = 1.331$
3	1866.2	1249.4	1561.0	951.9	
4	1653.2	1032.7	1066.5	1418.4	AOF = Q $\left[\frac{P_c^2}{P_c^2 - R_w^2} \right]^n = 1.371$
5	1358.2				
Absolute Open Flow 1,371 Mcfd @ 15.025 Angle of Slope @ 63.5 Slope, n .500					
Remarks: * Shut-in BHP Test calculated from known BHP.					
** Flowing BHP'S					
No Fluid Produced during Test.					
Approved By Commission:		Conducted By:		Calculated By:	
		W.S.		B.M.	
				B.M.	

REC-100
MAR 7 - 1988
OCD
HOBBS OFFICE

C.W. TRAINER
 BETTY STATE NO. 1
 L-16-17S-35E.
 Lea County, New Mexico
 March 3, 1988



RECEIVED

MAR 7 - 1988
OCD
HOBBS OFFICE

COMPANY C. W. TRIMMER LEASE ELBERT STOPP WELL NO. 1 DATE 3-6-68

LOCATION: Unit _____ Section 16 Township 17 S Range 36 E
L. 11959 H. 11959 L/H 1.600 G. 653 % CO₂ 0.399 % N₂ 0.081 % H₂S _____

GH 7568.78 P_{cr} 690 T_{cr} 368
TABLE IX & X TABLE IX & X

187 20.1 300 474

NE	1	2	3	4	5	6	7	8
1	T _w (W.H. °R)	534	534	534	534	534	534	534
2	T _s (B.H. °R)	654	654	654	654	654	654	654
3	T = ($\frac{T_w + T_s}{2}$)	594	594	594	594	594	594	594
4	Z (Est.)	1.853	1.831	1.865	.842	.898	.852	.900
5	TZ	506.6	493.6	513.8	506.1	521.5	516.0	524.6
6	GH/TZ	13.775	15.333	14.781	15.123	14.502	14.928	14.159
7	e ^s (Table XIV)	1.676	1.799	1.737	1.935	1.913	1.751	1.700
8	P _f or P _s	2101.2	2101.2	1866.2	1866.2	1653.2	1666.2	1358.2
9	P _f ² or P _s ²	4415.0	4415.0	3482.7	3482.7	2738.1	2738.1	1844.9
10	P _f ² = P _f ² /e ^s or P _w ² = P _s ² /e ^s	2633.8	2484.3	7044.5	1944.3	1385.9	1434.9	1066.5
11	P _c or P _w	1622.9	1536.2	1415.8	1403.2	1234.4	1124.4	1032.7
12	P _w = ($\frac{P_w + P_s}{2}$) or ($\frac{P_c + P_f}{2}$)	1882.0	1838.7	1601.0	1235.9	1145	1104.4	1195.5
13	P _r = (P/P _{cr})	2.077	2.074	2.044	2.044	2.17	1.17	1.08
14	T _r = (T/T _{cr})	1.61	1.61	1.61	1.61	1.61	1.61	1.61
15	Z (Table XI)	.831	.831	.842	.842	.853	.853	.872

100-100000-1000
MAR 7 - 1988
GCD
HOBBS OFFICE