Submit in duplicate to appropriate district office.
See Rule 401 & Rule 1122

State of New Mexico
Energy Minerals and Natural Resources
Oil Conservation Division
2040 South Pacheco
Santa Fe, NM 87505

Form C-122
Revised October, 1999

30-025-35821

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator: CHEVRON/TEXACO		Lease or Unit Name: SHOE BAR	
Type Test: ☑ Initial ☐ Annual ☐ Special		Test Date: 5/8/02	Well No.: 2
Completion Date	Total Depth	Plug Back TD	Elevation
Unit Ltr - Sec - TWP - Rge: M-4-17s-35e			
Csg. Size / Wt. / d / Set At	Perforations: From: To:	County: LEA	
Tbg. Size: 2 7/8 / Wt.: 6.5 / d: 2.441 / Set At	Perforations: From: To:	Pool	
Type Well-Single-Bradenhead-G.G. or G.O. Multiple: SINGLE	Packer Set At	Formation: ATOKA	
Producing Thru: Tubing	Reservoir Temp. °F: 163.5	Mean Annual Temp. °F: 60	Baro. Press.-P_a: 13.2
Connection: AIR			

L	H	Gg	%CO_2	%N_2	%H_2S	Prover	Meter Run	Taps
12270	12270	0.656	0.45	1.318	N/A	N/A	4.026	FLG

No.	Prover Line Size x Orifice Size	Press p.s.i.g.	Diff. h_w	Temp. °F	TUBING DATA Press p.s.i.g.	TUBING DATA Temp. °F	CASING DATA Press p.s.i.g.	CASING DATA Temp. °F	Duration of Flow
SI					1749	N/A	PKR	N/A	
1	4.026 X 2.000	120	4	100	1595				1 HR
2	4.026 X 2.000	120	14	100	1444				1 HR
3	4.026 X 2.000	120	28	95	1346				1 HR
4	4.026 X 2.000	120	44	83	1153				1 HR
5									

RATE OF FLOW CALCULATIONS

No.	COEFFICIENT (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor F_g	Super Compress Factor F pv	Rate of Flow Q. Mcfd
1	19.81	21.3	113.2	0.9636	1.235	1.044	523
2	19.81	39.8	113.2	0.9636	1.235	1.044	979
3	19.81	55.04	108.2	0.968	1.235	1.045	1362
4	19.81	65.05	96.2	0.9786	1.235	1.047	1630
5							

No.	P_r	Temp. °R	T_r	Z
1	0.83	560	1.5	0.918
2	0.83	560	1.5	0.918
3	0.82	555	1.49	0.916
4	0.8	543	1.46	0.912
5				

Gas Liquid Hydrocarbon Ratio	N/A	Mcf bbl.
A.P. I. Gravity of Liquid Hydrocarbons	N/A	Deg.
Specific Gravity Separator Gas	0.656	XXXXXXX
Specific Gravity Flowing Fluid	XXXXX	
Critical Pressure	673	P.S.I.A. P.S.I.A.
Critical Temperature	371	R. R

P_c 1795.1 P_c^2 3222.4

No.	P_t^2	P_w	P_w^2	$P_c^2 - P_w^2$
1		1653.8	2735	487.4
2		1529.5	2339.4	883
3		1414	1999.4	1223
4		1240.5	1538.8	1683.6
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.91$ $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n = 1.82$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n$ 2966.6

Absolute Open Flow 2966.6 Mcfd @ 15.025 | Angle of Slope (): 47.19 | Slope n: 0.9263

Remarks: * CALCULATED FROM KNOWN BOTTOM HOLE PRESSURES. NO LIQUID MADE DURING TEST.

Approved By Division:	Conducted By:	Calculated By:	Checked By:
	PRO WELL TESTING	MERV BUECKER	BM

ORIGINAL SIGNED BY
PAUL F. KAUTZ
PETROLEUM ENGINEER

JUN 1 4 2002

RECEIVED
MAY 2002
HOBBS
OCD