## NEW MEXICO OIL CONSERVATION COMMISSION

HOBES OFFICE OCC

Revised 12-1-55

Form C-122

No. (Line) (Orifice) Size Size psig h <sub>w</sub> o <sub>F</sub> . psig o <sub>F</sub> . psig o <sub>F</sub> . Hr.  SI 975.3  2. 94.0  3. 12.5  4. 21.5  5. FLOW CALCULATIONS  Coefficient Pressure Flow Temp. Gravity Factor Factor Factor Factor Factor Gravity Factor Factor Factor Q-MCFPD	Pool	Zumo	et					SSURE TES		. AM g:	43.	
Sec. 20   Twp. 195   Rge. 165   Purchaser   Permian Baria   Pl. Co.	[niti	al		_Annu	al		Spec	cial		Date of	Test	5-31-56
nit	ompa	ny Culf	011 Cor	paret	ion .		Lease B	11, R. R	· · · · ·	We]	Ll No	3
asing 7 Wt. 1.D. 1995 Set at 3686 Perf. To  ubing 1375 Wt. 1.T.D. 1995 Set at 3692 Perf. To  as Pay: From 3700 To 3715 L 363 xG												
Noting   1375   No.   1.0.   1375   Set at   1385   Perf.   To   1700   To   13715   L   1385   xg   400   GL   Bar, Press.   11   Type Well   Single-Bradenhead-G. G. or G.O. Dual   Reservoir Temp.   Single-Bradenhead-G. G. or G.O. Dual   Reservoir Temp.   Gravity   Type Taps   Tipe   Thou Data   Tubing Data   Casing Data   Casing Data   Gravity   Compress.   Temp.   Press.   Temp.   Press.   Temp.   Press.   Temp.   Or F.   Factor   Press.   Pres									<del></del> _			
Size   Pass   Press   Press   Press   Durat   Press												
Tubing   Type Well   Single-Bradenhead-G. G. or G.O. Dual   Reservoir Temp.												
ested Through  Flow Data  Flow Data  OFFICE (Line) (Orifice) Size   psig   hw   OFF   psig   OFF   psig   OFF   psig   OFF   Press   Temp   OFF   Press   OFF												
ested Through  Flow Data  Flow Data  OFFICIAL CONTINUE  Flow Data  OFFICIAL CONTINUE  Flow Calculations  Flo	ate d	of Complet	tion:		6-6-5	Packer	, Ho	Sin	gle-Brade	enhead-G.	G. or	G.O. Dual
Flow Data  Flow Data  Flow Data  Flow Data  Flow Data  (Chinge) (Orifice)  Size   psig   hw   OF   psig   OF   psig   OF   Hr.  FLOW CALCULATIONS  FLOW CALCULATIONS  FLOW CALCULATIONS  FLOW Temp.   Gravity   Compress   Rate of Flow Temp.   Factor		- Jone 1				r dono.				orr remp.		
Flow Data Tubing Data Casing Data  O. (Line) (Orifice) Press. Diff. Temp. Press. Temp. Press. Temp. Of F. Size Size psig hw OF. psig OF. psig OF. Hr.  I	aetar	d Through	(2000			(Motom)		DED DATA		Trans To	. 2	ine
O. (Proce) (Chine) Press. Diff. Temp. Press. Temp. Press. Temp. Of F. (Line) Size Size psig hw OF. psig OF. psig OF. Hr.  I		- moden	_			(Heret.)		m	Dot -			<u> </u>
Coefficient	Т	(Prover)	ru rono) 🕆	OW DE	Press.	Diff.	Temp.					]   Duration
FLOW CALCULATIONS  FLOW CALCULATIONS  Coefficient  (24-Hour)  Pressure  Flow Temp. Factor Fac	٥.	$(\mathtt{Line})$	(Orifi	ce)			_		_			of Flo
PRESSURE CALCULATIONS  A Specific Gravity Separator Gas Specific Gravity Flowing Fluid Pc	-	DIZE	512	se		w <sup>n</sup>	г.			L		
FLOW CALCULATIONS    Coefficient   Pressure   Flow Temp.   Gravity   Compress.   Rate of Flow Temp.   Factor		<u> </u>					- 27			927.5		*
FLOW CALCULATIONS  FLOW CALCULATIONS  Coefficient  (24-Hour)  Pressure Flow Temp. Gravity Factor Fac	• [				A		- 23	723.1				1 77
PLOW CALCULATIONS  Coefficient  Pressure Flow Temp. Gravity Compress. Rate of Flow Temp.  Factor Factor Factor Factor Factor Provided Prov	•	-								The second second	· ·	1
Coefficient  (24-Hour)  (34-Hour)											İ	
PRESSURE CALCUTATIONS  Sa Liquid Hydrocarbon Ratio cf/bbl. Specific Gravity Separator Gasavity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid Pc Pc Pc Calcut Pc Pc Pc Pc Calcut Pc		Coeffici	ent		Pn					Company		Pate of Flow
PRESSURE CALCUTATIONS  Station of Liquid Hydrocarbon Ratio of bl. Specific Gravity Separator Gas Specific Gravity Flowing Fluid Pc Pc Pc Cal. Py Pc Pc Pc Cal. Py Pc Pc Pc Cal. Py Pc	o •	(24-Hour)		/		cssure			Factor	Factor Fpv		Q-MCFPD
PRESSURE CALCULATIONS  S Liquid Hydrocarbon Ratio cf/bbl. Specific Gravity Separator Gas Specific Gravity Flowing Fluid Pc Pc Pc Cal. Py Fc (1-e-s) Pw Pt Fc MCFPD; n						psia	F	t.	Fg			@ 15.025 psia
PRESSURE CALCUTATIONS  Solution by the second secon						•		9		4.00		
PRESSURE CALCUTATIONS  Solution by the second secon	:-	15.06		244.7						1.0		
PRESSURE CALCUTATIONS  Solution by the second secon	-	15.26		152.5	<b>)</b>					1.0	17	
PRESSURE CALCULATIONS  Solute Potential:  MCFPD; n  PRESSURE CALCULATIONS  Specific Gravity Separator Gas Specific Gravity Flowing Fluid Pc	<u>, T</u>								- 0	02 - 1.9	75	
avity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid $P_c$ $P_w$ $P_c$						PRE	ESSURE C	ALCUIATIO	ons I	2-2-1	\$	
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P <sub>w</sub> P <sub>t</sub> F <sub>c</sub> Q (F <sub>c</sub> Q) <sup>2</sup> (F <sub>c</sub> Q) <sup>2</sup> P <sub>w</sub> 2 P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup> Cal. P <sub>w</sub> P <sub>c</sub> P <sub>c</sub> P <sub>w</sub> P <sub>w</sub> P <sub>c</sub> P <sub>w</sub> P <sub>c</sub> P <sub>w</sub>					ons -e <sup>-s</sup> )		deg.	_	Speci P <sub>c</sub> _	fic Gravi	ty Flor	ring Fluid
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DORESS MCFPD; n	P	w	P1	न	Q	(F <sub>2</sub> O) <sup>2</sup>	ম)	20)2	P. 2	P <sup>2</sup> -P <sup>2</sup>	Ca	11. P.
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MCFPD; n				<del></del>	3920				.80			
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## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- Q = Actual rate of flow at end of flow period at W. H. working pressure  $(P_W)$ . MCF/da. @ 15.025 psia and 60° F.
- PcI 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- Pw Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- $P_{f}$  Meter pressure, psia.
- hw Differential meter pressure, inches water.
- Fg Gravity correction factor.
- $F_t$  Flowing temperature correction factor.
- Fpv Supercompressability factor.
- n I Slope of back pressure curve.
- Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .