

NEW MEXICO OIL CONSERVATION COMMISSION

Form C-122

Revised 12-1-55

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Pool Dumont Formation Yates, 7 Rivers & Queen County Lea  
 Initial \_\_\_\_\_ Annual \_\_\_\_\_ Special X Date of Test 7-15-56  
 Company Continental Oil Company Lease Sanderson A-11 Well No. 1  
 Unit I Sec. 11 Twp. 20 Rge. 36 Purchaser EPNG  
 Casing 5 1/2 Wt. 17 I.D. - Set at 3778 Perf. - To -  
 Tubing 2 1/2 Wt. 6.5 I.D. - Set at - Perf. - To -  
 Gas Pay: From 2453 To 3000 2453 xG .670 -GL 1644 Bar.Press. 13.2  
 Producing Thru: Casing X Tubing \_\_\_\_\_ Type Well Bradenhead  
 Date of Completion: 9-30-36 Packer - Single-Bradenhead-G. G. or G.O. Dual  
 Reservoir Temp. 900

OBSERVED DATA

Tested Through (Prover) (Choke) (Meter) Type Taps Flange

No.	Flow Data					Tubing Data		Casing Data		Duration of Flow Hr.
	(Prover) (Line) Size	(Choke) (Orifice) Size	Press. psig	Diff. h <sub>w</sub>	Temp. °F.	Press. psig	Temp. °F.	Press. psig	Temp. °F.	
SI								828		72
1.	4"	1.500	585	.8	92			811		24
2.	4"	1.500	578	57.8	75			654		24
3.	4"	1.500	558	74.0	70			630		24
4.	4"	1.500	504	56.3	74			636		24
5.										

FLOW CALCULATIONS

No.	Coefficient (24-Hour)	$\sqrt{h_{wpf}}$	Pressure psia	Flow Temp. Factor F <sub>t</sub>	Gravity Factor F <sub>g</sub>	Compress. Factor F <sub>pv</sub>	Rate of Flow Q-MCFPD @ 15.025 psia
1.	13.99	21.64		.9706	.9463	1.062	295
2.	13.99	182.78		.9859	.9463	1.062	2534
3.	13.99	203.20		.9905	.9463	1.058	2819
4.	13.99	184.40		.9868	.9463	1.065	2566
5.							

\*Note - I-10 chart used.

PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio \_\_\_\_\_ cf/bbl.  
 Gravity of Liquid Hydrocarbons \_\_\_\_\_ deg.  
 F<sub>c</sub> Not applicable (1-e<sup>-s</sup>) Not applicable  
 Specific Gravity Separator Gas = \_\_\_\_\_  
 Specific Gravity Flowing Fluid = \_\_\_\_\_  
 P<sub>c</sub> 841.2 P<sub>c</sub> 707.6

No.	P <sub>w</sub> P <sub>t</sub> (psia)	P <sub>t</sub> <sup>2</sup>	F <sub>c</sub> Q	(F <sub>c</sub> Q) <sup>2</sup>	(F <sub>c</sub> Q) <sup>2</sup> (1-e <sup>-s</sup> )	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>	Cal. P <sub>w</sub>	P <sub>w</sub> /P <sub>c</sub>
1.	824.2	679.3	-	-	-	679.3	28.3	824.2	.98
2.	667.2	445.2	-	-	-	445.2	262.4	667.2	.79
3.	643.2	413.7	-	-	-	413.7	293.9	643.2	.76
4.	649.2	421.5	-	-	-	421.5	286.1	649.2	.77
5.			6,600						

Absolute Potential: \_\_\_\_\_ MCFPD; n .97  
 COMPANY Continental Oil Company  
 ADDRESS Box 427, Hobbs, New Mexico  
 AGENT and TITLE D. Howard, Gas Tester  
 WITNESSED \_\_\_\_\_  
 COMPANY \_\_\_\_\_

REMARKS

Although three points on curve line up, this test by Operator is considered unsuccessful since water-logging caused Rate Nos. 3 and 4 to develop in improper sequence. Pipeline also attempted a back-pressure test on this well, without success, prior to the above test.

ELVIS A. UTZ  
GAS ENGINEER

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- $Q$  = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.
- $P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia
- $P_w$  = Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- $P_t$  = Flowing wellhead pressure (tubing if flowing through tubing, casing if  
flowing through casing.) psia
- $P_f$  = Meter pressure, psia.
- $h_w$  = Differential meter pressure, inches water.
- $F_g$  = Gravity correction factor.
- $F_t$  = Flowing temperature correction factor.
- $F_{pv}$  = Supercompressability factor.
- $n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .