

FORMATION RECORD

FROM	TO	THICKNESS IN FEET	FORMATION
0	20	20	Sand & Caliche
20	250	230	Red Bed
250	300	50	Sand & Red Bed
300	371	71	Caliche & Red Bed
371	575	204	Caliche & Red Bed
575	750	175	Red Bed & Shells
750	950	200	Red Bed & Shells
950	1051	101	Lime
1051	1096	45	Red Bed, Shale & Shells
1096	1153	57	Shale, Shells & Salt
1153	1280	127	Anhydrite & Red Bed
1280	1450	170	Anhydrite & Potash
1450	1614	164	Anhydrite, Potash & Salt
1614	1788	174	Salt, Anhydrite & Red Bed
1788	1985	197	Anhydrite, Potash & Salt
1985	2095	110	Anhydrite, Potash, Salt & Gypsum
2095	2275	180	Salt & Red Bed
2275	2310	35	Lime & Anhydrite
2310	2345	35	Lime & Shale
2345	2370	25	Lime
2370	2452	82	Anhydrite & Lime
2452	2458	6	Lime
2458	2499	41	Lime & Anhydrite
2499	2530	31	Lime & Gypsum
2530	2570	40	Anhydrite
2570	2603	33	Anhydrite & Gypsum
2603	2670	67	Lime & Anhydrite
2670	2732	62	Lime, Gypsum, Shale & Anhydrite
2732	2893	161	Lime & Anhydrite
2893	4191	1298	Lime
4191	4240	49	Lime & Gypsum
4240	4351	111	Lime
4351	4370	19	Lime & Dolomite
4370	4940	570	Lime
4940	4994	54	Lime & Gypsum
4994	8307	3313	Lime
8307	8311	4	Lime & Chert
8311	8318	7	Lime
8318	8323	5	Lime & Chert
8323	8325	2	Lime & Chert
8325	8330	5	Lime
8330	8337	7	Lime & Chert
8337	8745	408	Lime
8745	9113	368	Lime
9113	9120	7	Lime & Chert
9120	9125	5	Lime
9125	9131	6	Lime & Chert
9131	9705	574	Lime
9705	9710	5	Lime & Chert
9710	10007	297	Lime
10007	10027	20	Lime & Dolomite
10027	10085	58	Lime
10085	10095	10	Shale
10095	10110	15	Lime & Shale
10110	10138	28	Lime
10138	10165	23	Lime & Shale
10165	10177	12	Lime
10177	10209	32	Lime & Shale
10209	10219	10	Lime
10219	10230	11	Lime & Shale
10230	10242	12	Lime
10242	10263	32	Shale & Sand
10263	10300	37	Sandy Lime & Shale
10300	10330	30	Shale & Sand
10330	10351	21	Shale, Lime & Sand
10351	10377	26	Lime & Sand
10377	10394	17	Lime
10394	10426	32	Sand & Shale
10426	10441	15	Lime
10441	10476	35	Lime & Shale
10476	10522	46	Shale & Lime
10522	10523	1	Lime
10523	10539	16	Lime & Shale
10539	10554	15	Shale & Sand
10554	10568	14	Sandy Lime & Shale
10568	10573	5	Lime
10573	10580	7	Shale & Sand
10580	10614	34	Lime
10614	10625	11	Sandy Lime & Shale

TOPS

Elevation	3568'
Anhydrite	935'
Yates	2460'
Glorietta	5165'
Tubbs Sand	6310'
Pennsylvania	7920'
Devonian	8460'
Silerian	9115'
Montoya	9710'
Simpson	10020'
McKee	10304'
Reworked Ellenberger	10582'
T. D.	10625'

TOTAL DEPTH

DRILL STEM TESTS

DATE	PACKER	TOTAL DEPTH	RECOVERY
1. 11/18/47	5630'	- 5675'	75' drilling mud
2. 12/12/47	7160'	- 7342'	330' black, muddy sulphur water
3. 12/19/47	7550'	- 7629'	370 gas cut mud, sulphur odor
4. 12/22/47	7710'	- 7768'	126' oil cut drilling mud
5. 12/24/47	7765'	- 7868'	3800' salty sulphur water
6. 1/5/48	8388'	- 8455'	720' water blanket - 1080' salt water
7. 1/22/48	9115'	- 9205'	600' water blanket - 420' black muddy : salt water - 90' clean mud - 570' salty sulphur water
8. 3/1/48	10295'	- 10330'	Packer would not seat
9. 3/2/48	10308'	- 10332'	1500' water blanket - 630' mud- 6121' salt water
10. 3/12/48	10584'	- 10605'	Misrun. Packer would not go to bottom
11. 3/14/48	10590'	- 10625'	1500' water blanket - 725' drilling mud 5940' salty sulphur water

3/15/48 - Ran Schlumberger
 3/22/48 - Ran temperature survey. Indicated top of cement 4565'.
 3/23/48 - Ran a Lane Wells Gamma Ray and Neutron Survey.

PERFORATIONS

3/22/48	-	6806'	-	6856'	195 holes	100 sacks cement	No squeeze
3/25/48	-	5184'	-	5180'	12 holes	250 sacks cement	3500' pressure
3/25/48	-	5544'	-	5540'	12 holes	200 sacks cement	
3/29/48	-	5265'	-	5250'	60 holes	150 sacks cement	Acidized w/1500 gal. & 3000 gal.
4/2/48	-	5242'	-	5220'	88 holes	100 sacks cement	
4/7/48	-	5210'	-	5190'	80 holes		Acidized w/1500 gal.
4/8/48	-	5190'	-	5172'	72 holes	Set plug - 5112'-5237'	& 3000 gal.
4/11/48	-	Mixed mud to 9.8. Cut 7" casing at 3100' and pulled.					
4/12/48	-	Set plug w/100 sacks at bottom of 9 5/8".					
4/12/48	-	Set plug w/180 sacks at top of 9 5/8". Well capped with 4" pipe marker.					

TOTCOS

DEPTH	INCLINATION	DEPTH	INCLINATION
150'	$\frac{1}{2}$	4380'	2 1/8
330'	$\frac{1}{2}$	4435'	2 $\frac{1}{2}$
630'	3/4	4475'	2 $\frac{1}{2}$
1234'	3/4	4500'	2
1550'	3/4	4555'	2
2230'	2	4610'	2
2330'	2 1/3	4665'	1 3/4
2360'	2 1/3	4720'	1 3/4
2390'	2 $\frac{1}{2}$	4829'	1 3/4
2415'	2 $\frac{1}{2}$	4870'	1 $\frac{1}{2}$
2445'	2	4980'	1 $\frac{1}{2}$
2500'	2 $\frac{1}{2}$	5150'	1 $\frac{1}{2}$
2537'	2 1/8	5275'	1 $\frac{1}{2}$
2565'	2 1/8	5540'	1 $\frac{1}{2}$
2590'	1 7/8	5600'	1 $\frac{1}{2}$
2700'	1 $\frac{1}{2}$	5875'	2
2832'	1 3/4	5905'	1 3/4
3000'	1 3/8	6020'	2
3200'	1 3/4	6060'	1 $\frac{1}{2}$
3350'	1 3/4	6250'	2 3/4
3440'	1 3/4	6300'	1 $\frac{1}{2}$
3535'	1 7/8	6312'	1 $\frac{1}{2}$
3750'	1 $\frac{1}{2}$	6450'	1 $\frac{1}{2}$
3960'	1 3/4	6522'	1 $\frac{1}{2}$
4125'	2	6600'	1 $\frac{1}{2}$
4250'	2 $\frac{1}{2}$	6620'	1 $\frac{1}{2}$
4280'	2 $\frac{1}{2}$	6725'	1 $\frac{1}{2}$
4350'	2	6733'	1 3/4

TOTCOS (cont'd)

<u>DEPTH</u>	<u>INCLINATION</u>
6850'	1 $\frac{1}{4}$
6975'	1
7150'	1 $\frac{3}{4}$
7200'	1 $\frac{3}{4}$
7250'	1 $\frac{1}{4}$
7355'	1
7450'	1 $\frac{1}{4}$
7560'	$\frac{3}{4}$
7900'	1
8225'	$\frac{3}{4}$
8375'	1 $\frac{1}{4}$
8649'	1 $\frac{1}{4}$
8800'	1 $\frac{1}{4}$
9100'	1 $\frac{1}{4}$
9630'	2
9700'	3
9885'	2 $\frac{1}{4}$
10010'	3 $\frac{3}{4}$
10060'	3 $\frac{3}{4}$
10105'	3
10135'	3 $\frac{1}{4}$
10225'	2 $\frac{3}{4}$

Tests by Snabbing.

6806	6856	Sulphur water	
5250	5285	"	"
5220	5242	"	"
5172	5190	"	"
			Show of oil

[Signature]
Dist. Supt.

