## HOBBS OFFICE OCC

Form C-122

Revised 12-1-55

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Poo	1 Euroni	; 		F	ormation	Quec	ก	(11 5	Count <i>y</i> _	Lea		
Ini	tial	<del></del>	Annua]	L		,					11-18-56	
Com	pany Conti	nental	011 Co	mpan	7	Lease	State A	-6	We	ll No	1	
Jni	t <u>n</u>	Sec	<b>6</b> Twp.	19	<b>93</b> Re	ge <b>37</b> E	Purc	haser	EPNG			
Cas	ing 5 1/2	Wt	<b>LA_</b> I.I	<u>5</u> .	. <b>012</b> Se	t at _ 3	<b>884</b> Pe	rf360	00	То	3862	
	ing <b>None</b>						*					
	Pay: From					_						
	ducing Thru											
)at	e of Complet	tion:_	9-2-54	,	Packe	r None	Sin	gle-Brade Reserve	enhead-G.	G. or	6.0. Dual	
							ED DATA				<del> </del>	
est	ed Through	(PYXI	ekk) (KK	okr <b>i</b>	(Meter)		22 2		Type Tap	s Pl	Lange	
Flow Data							Tubing					
٥.	( <b>XXXXX</b> ) (Line)	(638)	P	ress	Diff.	Temp.	Press.				I .	
٠.	Size	Si	ice) ze	psig	h <sub>w</sub>	° <sub>F</sub> .	psig	°F.	psig	⊃ <sub>F</sub> .	of Flo	
I									870	<del> </del>	72	
	<u> </u>	2,00			6.76	60			268		24	
:	4	2,00			56.25	63		<u> </u>	92	<u> </u>	24	
	<u> </u>	2.00		50 43	55.50 46.92	86 73			232	<del> </del>	24, 24,	
					,	DT ON OAT	CIT AMTON	,				
Т	Coefficient						CULATIONS Temp.			ess. Rate of Flow		
٠.				1					Factor			
	(24-Hour) $$		$\sqrt{h_{\mathbf{w}}p_{\mathbf{f}}}$	h <sub>w</sub> p <sub>f</sub> psia		Ft		${\mathtt F}_{\mathtt g}$	· F <sub>pv</sub>		@ 15.025 psi	
	25.58		M;.50			1.0000		·9325	1.03	3	1096	
4	25.58		60.47			a 9971.		۰ <b>9325</b>	1.03		1439	
+	25.58		59.23			3 <b>9759</b>		•9325	1.033		1377	
+	25.58	<del></del>	51.26	-		.9877		•9325	1.03	,	1208	
vi	iquid Hydro ty of Liqui •9002	d Hydr	ocarbons		.157	cf/bbldeg.		Speci Speci		ty Flow	rator Gas ing Fluid <b>30.0</b>	
_				<del> </del>			······································	·	<del></del>			
•	P <sub>w</sub>	$P_{t}^{2}$	F <sub>c</sub> Q		$(F_cQ)^2$	(F	$\left(\frac{Q}{e^{-s}}\right)^2$	P <sub>w</sub> 2	$P_c^2 - P_w^2$	Ca P		
$\dagger$	301.2	90.7	- 99	, -	<del>98</del>	-1.15	<del>~ /   9</del>	0.6	689.2	303.	• • • • • • • • • • • • • • • • • • •	
I	105.2	11.1	1.30		1.69	.27	1	1.4	768.6	106.	3 .12	
1	131.2	17.2	1.2		1.54	,, 24,		7.5	762.5	132.		
+++	245.2	60,1	1.09	<u>'</u>	1.19	.19	6	0.3	719.7	245.	• 28	
	lute Potent ANY <b>Cont</b>		1 011 Cc			MCFPD;	n_ 1.00	00				
DR EN		427. H	obbs, Na . Howard	rsv Mos	<u>xico</u> s <u>Taste</u> r							

This well would not produce into E.P.N.G. high-pressure athering at sufficient rate to accomplish back-pressure test. Test separator was installed and gas vented thru meter rule. Slope greater than 1.00 - average slope of 1.000 drawn thru highest rate of flow. provious attempts to test this well were unauccessful.

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- Q = Actual rate of flow at end of flow period at W. H. working pressure ( $P_{\rm W}$ ). MCF/da. @ 15.025 psia and 60° F.
- P<sub>c</sub>= 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- Pw Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw Differential meter pressure, inches water.
- Fg Gravity correction factor.
- Ft Flowing temperature correction factor.
- $F_{pv}$  Supercompressability factor.
- n I Slope of back pressure curve.
- Note: If  $P_{\rm W}$  cannot be taken because of manner of completion or condition of well, then  $P_{\rm W}$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_{\rm t}$ .