

## NEW MEXICO OIL CONSERVATION COMMISSION

ELVIS A. UTZ  
GAS ENGINEER

Form C-122

## HOBBS OFFICE OCC

Revised 12-1-55

## MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

1956 OCT 8 PM 2:22

Pool Eumont Formation Queens County LeaInitial X Annual \_\_\_\_\_ Special \_\_\_\_\_ Date of Test 5-31-56  
6-8-56Company The Texas Company Lease State of N.M. "G" NCT-6 Well No. 1Unit J Sec. 6 Twp. 19-S Rge. 37-E Purchaser Permian Basin Pipe Line Co.Casing 5 1/2 Wt. 14.0 I.D. 5.012 Set at 3570 Perf. Open Hole To \_\_\_\_\_Tubing 2 3/8 Wt. 4.70 I.D. 1.995 Set at 3573 Perf. 3569 To 3572Gas Pay: From 3570 To 3890 L 3569 xG .685 -GL \_\_\_\_\_ Bar.Press. 13.2Producing Thru: Casing \_\_\_\_\_ Tubing X Type Well Single

Single-Bradenhead-G. G. or G.O. Dual

Date of Completion: 2-16-54 Packer None Reservoir Temp. \_\_\_\_\_ $CO_2 = 1.08\%$   $N_2 = 4.22\%$ 

## OBSERVED DATA

Tested Through (Proven) (Choke) (Meter) Type Taps Pipe

No.	Flow Data					Tubing Data		Casing Data		Duration of Flow Hr.
	(Reever) (Line) Size	(Choke) (Orifice) Size	Press. psig	Diff. h <sub>w</sub>	Temp. °F.	Press. psig	Temp. °F.	Press. psig	Temp. °F.	
SI						1002.2		1002.2		73 1/4
1.	4	2.00	439.5	8.8	78	896.2		923.2		23 2/3
2.	4	2.00	443.8	15.8	78	816.0		853.8		24
3.	4	2.00	445.9	22.3	74	724.6		799.8		23 1/2
4.	4	2.00	442.6	29.5	81	628.4		745.9		23
5.										

## FLOW CALCULATIONS

No.	Coefficient (24-Hour)	$\sqrt{h_{wpf}}$	Pressure psia	Flow Temp. Factor F <sub>t</sub>	Gravity Factor F <sub>g</sub>	Compress. Factor F <sub>pv</sub>	Rate of Flow Q-MCFPD @ 15.025 psia
1.	29.92	63.12	452.7	.9831	.9359	1.039	1,805
2.	29.92	84.98	457.0	.9831	.9359	1.040	2,433
3.	29.92	101.2	459.1	.9868	.9359	1.042	2,914
4.	29.92	116.0	455.8	.9804	.9359	1.039	3,309
5.							

## PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio \_\_\_\_\_ cf/bbl.

Gravity of Liquid Hydrocarbons \_\_\_\_\_ deg.

F<sub>c</sub> \_\_\_\_\_ (1-e<sup>-s</sup>)Specific Gravity Separator Gas .685

Specific Gravity Flowing Fluid \_\_\_\_\_

P<sub>c</sub> 1015.4 P<sub>c</sub><sup>2</sup> 1031.0

No.	P <sub>w</sub> psia P <sub>t</sub> (psia)	P <sub>t</sub> <sup>2</sup>	F <sub>c</sub> Q	(F <sub>c</sub> Q) <sup>2</sup>	(F <sub>c</sub> Q) <sup>2</sup> (1-e <sup>-s</sup> )	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>	Cal. P <sub>w</sub>	P <sub>w</sub> P <sub>c</sub>
1.	926.4					876.4	154.2		.92
2.	857.0					741.7	279.3		.85
3.	813.0					661.0	370.0		.80
4.	759.1					576.2	454.8		.75
5.									

Absolute Potential: 5,600 MCFPD; n .64COMPANY The Texas CompanyADDRESS Box 1270, Midland, TexasAGENT and TITLE L. I. Baker, District Gas Man *L. I. Baker*WITNESSED H. E. BarrettCOMPANY Permian Basin Pipe Line Company

REMARKS

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

$Q$  = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.

$P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia

$P_w$  = Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia

$P_t$  = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia

$P_f$  = Meter pressure, psia.

$h_w$  = Differential meter pressure, inches water.

$F_g$  = Gravity correction factor.

$F_t$  = Flowing temperature correction factor.

$F_{pv}$  = Supercompressability factor.

$n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .