Ramonde

PORTEN CAR CARTE DOC

Form C-122
Revised 12-1-55

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

			_						
Initial		Annual_	x	Spec	ial		Date of	Test	/9 thru 6/17
Company	• Chie Oil	Company		Lease	State "A'	"-3071 -D	We	ell No.	1
Unit	_Sec. 28	_Twp1	. 9-3 Re	ge	Purc	haser_	Permian B	asia Pi	peline Compa
Casing 5.5	Wt. 17	I.D	. 892 Se	t at_ 3	969 Pe:	rf. 355	0-3602	**	3640-3702
Tubing 2.375	_Wt	1.D1	. .995 Se	t at	28 Pe	rf	3525	To	3526
Gas Pay: Fro	om 3550 7	ro 3702	L	15 x	g 0.67	_GL	1372	Bar.Pr	ess. 13.2
roducing Thi	ru: Casir	ıg	Tu	bing 1		Type W	 ell	Single	
Producing Throate of Compl	Letion:	41 25, 1	955 Packe	r_ Name	Sing	gle-Brad Reserv	enhead-G.	G. or	G.O. Dual
				OBSERVE					
ested Throug	gh (Trover) (choke) (Meter)				Type Ta	P	De
	Flo	w Data		— т	Tubing	Data			T
o. (Line)			s. Diff.	Temp.		Temp.	Casing Press.	Temp.	Durati
`Size´	Size	psi	g h _w	o _F .	psig	°F.	psig	⊳ _F .	of Flo
· Pa	2"	 bb5		35	832.3	83	873.3	83	784 hr. 8.1
. 40	20	450.	9.0	79	772.4	85	0,018	88	24-1/4 hr.
	7 2 -	145.		71	670.5 571.9	88 88	765.1	88	2)-3/4 hr.
,									23-1/2 hr.
	cient		ressure	LOW CALC	ULATIONS	Gravity	Compa		D-1 - 0 D3
(2)H	0117)/	$\sqrt{h_{\mathbf{w}}p_{\mathbf{f}}}$ psia		ractor		Gravity Compre Factor Factor		r	Rate of Flor
27.92			ps1a	0.9741		F _g	pv		9 17.027 ps.
27.72	6	14.6Z	464.0	0.7622	0,	MI.	1,04		1169
29.92		2,02	461.3	0.9913		941	1.00		\$278
+		1000	der 13	VAJUSO	G2,	941	1.04	7	
									3279
Liquid Hydr vity of Liqu	ocarbon Ra	utio	Gas	SSURE CAI		NS Special	fic Gravi	ty Sepa	rator Gas ing Fluid
Liquid Hydr vity of Liqu Pw Pt (psia)	rid Hydroca	rbons	Gas	SSURE CAI	LCU ATION	Special Special PcP_2	fic Gravi fic Gravi 886.5 P _c -P _w ²	ty Sepa ty Flow P2	rator Gas_ing Fluid
P _w Pt (psia)	rid Hydroca	rbons(1-e ^{-s})	Gas	SSURE CAI	LCU ATION	Special Special PcP_2	fic Gravi fic Gravi 886.5 P _c -P _w ²	ty Sepa ty Flow P ²	rator Gas_ing Fluid
Liquid Hydr vity of Liqu P _W P _t (psia)	rid Hydroca	rbons(1-e ^{-s})	Gas	SSURE CAI	LCU ATION	Special Special Pc-Pw2	fic Gravi fic Gravi 886.5 P _C -P _W	ty Sepa ty Flow P2	rator Gas_ing Fluid_785.9
P _w Pt (psia)	rid Hydroca	rbons(1-e ^{-s})	Gas	SSURE CAI	LCU ATION	Special Special PcP_2	fic Gravi fic Gravi 886.5 P _C -P _W	ty Sepa ty Flow P2	rator Gas_ing Fluid
Pw Pt (psia)	P ² _t	F _c Q	(F _c Q) ²	SSURE CAI	LCU ATION	Special Special Pc-	fic Gravi fic Gravi 886.5 P _C -P _W	ty Sepa ty Flow P2	rator Gas_ing Fluid_785.9
Pw Pt (psia) 745-7 solute Potent	Pt Pt tial:	F _c Q 7,800 Company (7, Lobbi	$(F_cQ)^2$	SSURE CAI cf/bbl. deg. (FcQ (1-e	LCU ATION	Special Special Pc-	fic Gravi fic Gravi 886.5 P _C -P _W	ty Sepa ty Flow P2	rator Gas_ing Fluid_785.9
Pw Pt (psia) Pt (psia) Pt (psia) Pt (psia) Pt (psia)	Pt tial: Chie Cal	F _c Q 7,800 Company (7, Lobbi	$(F_cQ)^2$	SSURE CAI cf/bbl. deg. (FcQ (1-e	LCU ATION	Specing Specing P _C	fic Gravi fic Gravi 886.5 P _C -P _W	ty Sepa ty Flow PC Ca:	rator Gas ing Fluid 785.9

NOTE: Due to impreper alignment of points on back pressure curve, well will be re-tested.

INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

- Q = Actual rate of flow at end of flow period at W. H. working pressure ($P_{\rm W}$). MCF/da. @ 15.025 psia and 60° F.
- Pc= 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- Pw Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw Differential meter pressure, inches water.
- Fg Gravity correction factor.
- F_t Flowing temperature correction factor.
- Fnv Supercompressability factor.
- n I Slope of back pressure curve.
- Note: If $P_{\rm W}$ cannot be taken because of manner of completion or condition of well, then $P_{\rm W}$ must be calculated by adding the pressure drop due to friction within the flow string to $P_{\rm t}$.