

## NEW MEXICO OIL CONSERVATION COMMISSION

11045 OFFICE FILE  
1961 JUN 20  
Form C-122  
Revised 12-2-55

## MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Pool EUMONT Formation QUEEN SAND County LEA  
Initial X Annual \_\_\_\_\_ Special \_\_\_\_\_ Date of Test 5-30-61  
Company CHAMBERS & KENNEDY Lease MONUMENT STATE Well No. 1  
Unit J Sec. 34 Twp. 19S Rge. 37E Purchaser NOT TIED IN  
Casing 5-1/2" Wt. 14.0 I.D. 5.012 Set at 3964' Perf. 3584' To 3700'  
Tubing 2-1/2" Wt. 8.50 I.D. 2.441 Set at 3729' Perf. 3722' To \_\_\_\_\_  
Gas Pay: From 3584' To 3700' L 3584' xG 6.50 -GL 2330 Bar. Press. 13.2  
Producing Thru: Casing \_\_\_\_\_ Tubing X Type Well G. O. DUAL  
Date of Completion: 5-18-61 Packer 3725 Reservoir Temp. 99°  
Single-Bradenhead-G. G. or G.O. Dual

## OBSERVED DATA

Tested Through (Prover) ~~(XXXXXX)~~ ~~(XXXXXX)~~Type Taps CRITICAL FLOW PROVER

No.	Flow Data					Tubing Data		Casing Data		Duration of Flow Hr.
	(Prover) <del>(XXXXXX)</del> Size	<del>(XXXXXX)</del> (Orifice) Size	Press. PROVER psig	Diff. h <sub>w</sub>	Temp. °F.	Press. psig	Temp. °F.	Press. P <sub>w</sub> psig	Temp. °F.	
SI						500		567		S.I. 72 HRS.
1.	2"	5/16"	476	-	78	477		511		3 HRS.
2.	2"	7/16"	368	-	76	370		457		3 HRS.
3.	2"	5/8"	265	-	74	268		393		3 HRS. 15 MIN.
4.	2"	3/4"	190	-	72	194		372		3 HRS.
5.										

## FLOW CALCULATIONS

No.	Coefficient (24-Hour)	$\sqrt{h_w P_f}$	Pressure (PROVER) psia	Flow Temp. Factor F <sub>t</sub>	Gravity Factor F <sub>g</sub>	Compress. Factor F <sub>pv</sub>	Rate of Flow Q-MCFPD @ 15.025 psia
1.	2.1577	-	489.2	.9831 ✓	.9608 ✓	1.045 ✓	1042 ✓
2.	4.3337 ✓	-	331.2	.9850 ✓	.9608	1.034 ✓	1641 ✓
3.	8.3555 ✓	-	278.2	.9868 ✓	.9608	1.025 ✓	2259 ✓
4.	12.2023 ✓	-	203.2	.9887 ✓	.9608	1.019 ✓	2400 ✓
5.							

## PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio NONE cf/bbl.  
Gravity of Liquid Hydrocarbons --- deg.  
F<sub>c</sub> (1-e<sup>-S</sup>)

Specific Gravity Separator Gas .650  
Specific Gravity Flowing Fluid -  
P<sub>c</sub> 580.2 P<sub>c</sub><sup>2</sup> 336.6

No.	P <sub>w</sub> P <sub>t</sub> (psia)	P <sub>t</sub> <sup>2</sup>	F <sub>c</sub> Q	(F <sub>c</sub> Q) <sup>2</sup>	(F <sub>c</sub> Q) <sup>2</sup> (1-e <sup>-S</sup> )	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>	Cal. P <sub>w</sub>	P <sub>w</sub> /P <sub>c</sub>
1.	524.2					274.8 ✓	51.3 ✓		9
2.	470.2					221.1 ✓	115.5 ✓		16.7
3.	406.2					165.0 ✓	171.6 ✓		70.1
4.	385.2					148.4 ✓	188.2 ✓		1.9
5.									

Absolute Potential: 3750 MCFPD; n .75221COMPANY CHAMBERS & KENNEDYADDRESS 607 MIDLAND NATIONAL BANK - MIDLAND, TEXASAGENT and TITLE APEX ENGINEERING COMPANY - BY: Harry E. Legendre

WITNESSED

COMPANY \_\_\_\_\_

## REMARKS

WELL FLOWING THROUGH TUBING FOR TEST, CASING NOT SEALED. LOWER ZONE SEALED OFF BY SIDE DOOR CHOKE ASSEMBLY AT 3722'.

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

$Q$  = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.

$P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia

$P_w$  = Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia

$P_t$  = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia

$P_f$  = Meter pressure, psia.

$h_w$  = Differential meter pressure, inches water.

$F_g$  = Gravity correction factor.

$F_t$  = Flowing temperature correction factor.

$F_{pv}$  = Supercompressability factor.

$n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .