NEW MEXICO OIL CONSERVATION COMMISSION

HOBBS OFFICE OCC

Form C-122

Revised 12-1-55

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

OCT 30 PM 2:47

Pool **Eumont** Formation **Queen** County **Lea**

Initial ____ Annual **X** Special ____ Date of Test **10/3 to 11/57**

Company **Anderson-Prichard Oil Corp.** Lease **Britt "B"** Well No. **1**

Unit **N** Sec. **5** Twp. **20S** Rge. **37E** Purchaser **Permian Basin Pipe Line Co.**

Casing **9 5/8** Wt. **40.0#** I.D. **8.835"** Set at **2437** Perf. **Open** To **Hole**

Casing **7.0** Wt. **24.0#** I.D. **6.336"** Set at **3700'** Perf. ____ To ____

Gas Pay: From **2585'** To **2690'** L **2585** xG **0.695** -GL **1797'** Bar.Press. **13.2**

Producing Thru: Casing **X** Tubing ____ Type Well **Bradenhead**
Single-Bradenhead-G. G. or G.O. Dual

Date of Completion: **4/27/57** Packer **---** Reservoir Temp. ____

OBSERVED DATA

Tested Through (Choke) (Meter) Type Taps **Pipe**

No.	Flow Data (Prover) (Line) Size	Flow Data (Choke) Size	Flow Data Press. psig	Flow Data Diff. h_w	Flow Data Temp. °F.	Tubing Data Press. psig	Tubing Data Temp. °F.	Casing Data Press. psig	Casing Data Temp. °F.	Duration of Flow Hr.
SI								958.7		72 hour SIP
1.	2.00 x 4		479.3	4.6	90			832.8		24 hour
2.	2.00 x 4		483.4	12.5	54			749.9		24 hour
3.	2.00 x 4		483.3	18.8	75			710.2		24 hour
4.	2.00 x 4		486.8	34.7	72			675.1		24 hour
5.										

FLOW CALCULATIONS

No.	Coefficient (24-Hour)	$\sqrt{h_w p_f}$	Pressure psia	Flow Temp. Factor F_t	Gravity Factor F_g	Compress. Factor F_{pv}	Rate of Flow Q-MCFPD @ 15.025 psia
1.	29.92	47.60		0.9723	0.9292	1.039	1337
2.	29.92	78.79		1.0058	0.9292	1.054	2322
3.	29.92	96.61		0.9859	0.9292	1.043	2762
4.	29.92	131.70		0.9887	0.9292	1.045	3783
5.							

PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio **Dry Gas** cf/bbl.

Gravity of Liquid Hydrocarbons **None** deg.

P_c **no friction** $(1-e^{-s})$ ____

Specific Gravity Separator Gas **.695**

Specific Gravity Flowing Fluid **None**

P_c **958.7** P_c^2 **944.6**

No.	P_w / P_t (psia)	P_t^2	F_cQ	$(F_cQ)^2$	$(F_cQ)^2 (1-e^{-s})$	P_w^2	$P_c^2-P_w^2$	Cal. P_w	P_w/P_c
1.	846.0	715.7				715.7	228.9		.87
2.	763.1	582.3				582.3	362.3		.79
3.	723.4	523.3				523.3	421.3		.74
4.	688.3	473.8				473.8	470.8		.71
5.									

Absolute Potential: **7589** MCFPD; n **1.00 (Limited)**

COMPANY **Anderson-Prichard Oil Corp.**

ADDRESS **Box 196, Midland, Texas**

AGENT and TITLE ____

WITNESSED **None**

COMPANY **Permian Basin Pipe Line Co.**

REMARKS

Good point alignment, but resulting slope in excess of 1.00, therefore, a slope of 1.00 was drawn through the high rate of flow data point to calculate the potential. Well will be retested at a later date.

INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

Q = Actual rate of flow at end of flow period at W. H. working pressure (P_w). MCF/da. @ 15.025 psia and 60° F.

P_c = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia

P_w = Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia

P_t = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia

P_f = Meter pressure, psia.

h_w = Differential meter pressure, inches water.

F_g = Gravity correction factor.

F_t = Flowing temperature correction factor.

F_{pv} = Supercompressability factor.

n = Slope of back pressure curve.

Note: If P_w cannot be taken because of manner of completion or condition of well, then P_w must be calculated by adding the pressure drop due to friction within the flow string to P_t.