

MULTIPOINT AND ONE POINT BACK PRESSURE TEST, OR GAS WELL

Form C-127
Revised 5-1-65

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 6-25-77	
Company UNION TEXAS PETROLEUM CORP.		Connection Northern Natural Gas Company	
Pool Eumont		Formation Queen	
Completion Date 2-1-77		Total Depth 5713	Plug Back TD 3483
		Elevation 3562' DF	Form or Lease Name
Csg. Size 5 1/2"	Wt. 15.5	d 4950	Set At 5712
Thg. Size 2.375	Wt. 4.7#	d 1.995	Set At 3161
Perforations: From 3206 To 3287		Well No. 12	
Perforations: From -- To --		Unit C	
Type Well - Single - Brdenhead - G.G. or G.O. Multiple Single		Packer Set At 3155	County Lea
Producing thru Tubing	Reservoir Temp. °F 90 @ 3246	Mean Annual Temp. °F 70 ⁰	Baro. Press. - P _a 13.2
State New Mexico			
L 3246	H 3246	G _g .672	% CO ₂ --
		% N ₂ --	% H ₂ S --
Prover --		Meter Run 4"	Taps Pipe

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI							420				97.3
1.	4 x 1.500			91	.5	76	407	70	0	0	1.0
2.	4 x 1.500			92	1.0	75	396	70	0	0	1.0
3.	4 x 1.500			95	2.0	75	381	70	0	0	1.0
4.	4 x 1.500			99	4.0	73	352	70	0	0	1.0
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super. Compress. Factor, F _{pv}	Rate of Flow Q, Mcf/d
1	11.82	7.22	104.2	.9850	1.2199	1.0100	104
2	11.82	10.26	105.2	.9859	1.2199	1.0102	147
3	11.82	14.71	108.2	.9859	1.2199	1.0104	211
4	11.82	21.18	112.2	.9877	1.2199	1.0109	305
5							

NO.	P _i	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	.16	536	1.41	.980	0	--	.672	XXXXXX	669	381
2	.16	535	1.40	.980						
3	.16	535	1.40	.979						
4	.17	533	1.40	.978						
5										

P _c 432.6 P _c ² 187			
NO.	P _i ²	P _w	P _w ²
1	177	420	176
2	167	409	167
3	155	394	155
4	133	366	134
5			

(1) $\frac{P_c^2}{P_i^2 - P_w^2} = 3.5255$		(2) $\left[\frac{P_c^2}{P_i^2 - P_w^2} \right]^n = 2.3703$	
ADP = Q $\left[\frac{P_c^2}{P_i^2 - P_w^2} \right]^n = 723$			

Absolute Open Flow	723	Mcf/d @ 15.025	Angle of Slope θ	55.6	Slope, n	.635
Remarks:						

Approved by Commission:	Conducted by:	Calculated by:	Checked by:
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