

MAIN OFFICE OCC

HOBBS OFFICE OCC

Revised 12-1-55

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Pool Summit AM 3:17 Formation San Juan 8 PM 2:21 County Lee

Initial I Annual \_\_\_\_\_ Special \_\_\_\_\_ Date of Test 6-15-56

Company Simclair Oil & Gas Company Lease E. J. Barber Well No. 7

Unit E Sec. 8 Twp. 20 S Rge. 37 E Purchaser KiPass Natural Gas Company

Casing 7" Wt. 24 I.D. 6.375 Set at 3000' Perf. None To \_\_\_\_\_

Tubing 2-1/2" Wt. 6.70 I.D. 2.442 Set at 3035' Perf. 3025' To 3000'

Gas Pay: From 3025' To 3000' L 3025' xG .660 -GL 0.119 Bar.Press. 13.2

Producing Thru: Casing \_\_\_\_\_ Tubing I' Type Well Single  
Single-Bradenhead-G. G. or G.O. Dual

Date of Completion: 3-2-50 Packer 3047' Reservoir Temp. 119

## OBSERVED DATA

Tested Through (Prover) (Choke) (Meter) \_\_\_\_\_ Type Taps \_\_\_\_\_

No.	Flow Data					Tubing Data		Casing Data		Duration of Flow Hr.
	(Prover) (Line) Size	(Choke) (Orifice) Size	Press. psig	Diff. h <sub>w</sub>	Temp. °F.	Press. psig	Temp. °F.	Press. psig	Temp. °F.	
SI										
1.	<u>1</u>	<u>1.00</u>	<u>970</u>	<u>14.2</u>	<u>75</u>	<u>977</u>	<u>75</u>	<u>970</u>		<u>72</u>
2.	<u>1</u>	<u>1.00</u>	<u>971</u>	<u>14.1</u>	<u>67</u>	<u>978</u>	<u>75</u>			<u>74</u>
3.	<u>1</u>	<u>1.00</u>	<u>968</u>	<u>14.3</u>	<u>68</u>	<u>976</u>	<u>75</u>			<u>74</u>
4.	<u>1</u>	<u>1.00</u>	<u>605</u>	<u>81.0</u>	<u>66</u>	<u>912</u>	<u>75</u>			<u>74</u>
5.										

## FLOW CALCULATIONS

No.	Coefficient (24-Hour)	$\sqrt{h_{wpf}}$	Pressure psia	Flow Temp. Factor F <sub>t</sub>	Gravity Factor F <sub>g</sub>	Compress. Factor F <sub>pv</sub>	Rate of Flow Q-MCFPD @ 15.025 psia
1.	<u>11.99</u>	<u>24.346</u>	<u>981.2</u>	<u>.989</u>	<u>.978</u>	<u>1.006</u>	<u>1398</u>
2.	<u>11.99</u>	<u>24.346</u>	<u>981.2</u>	<u>.979</u>	<u>.978</u>	<u>1.006</u>	<u>2291</u>
3.	<u>11.99</u>	<u>24.346</u>	<u>981.2</u>	<u>.983</u>	<u>.978</u>	<u>1.006</u>	<u>2081</u>
4.	<u>11.99</u>	<u>24.346</u>	<u>611.2</u>	<u>.973</u>	<u>.978</u>	<u>1.006</u>	<u>309</u>
5.							

## PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio \_\_\_\_\_ cf/bbl.

Gravity of Liquid Hydrocarbons \_\_\_\_\_ deg.

F<sub>c</sub> 5.566 (1-e<sup>-S</sup>) .136

Specific Gravity Separator Gas .660

Specific Gravity Flowing Fluid \_\_\_\_\_

P<sub>c</sub> 1000.2 P<sub>c</sub> 1000.4

No.	P <sub>w</sub> P <sub>t</sub> (psia)	P <sub>t</sub> <sup>2</sup>	F <sub>c</sub> Q	(F <sub>c</sub> Q) <sup>2</sup>	(F <sub>c</sub> Q) <sup>2</sup> (1-e <sup>-S</sup> )	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>	Cal. P <sub>w</sub>	P <sub>w</sub> P <sub>c</sub>
1.	<u>981.2</u>	<u>962</u>	<u>7.678</u>	<u>58.97</u>	<u>5.01</u>	<u>977.02</u>	<u>21.03</u>	<u>978.5</u>	<u>959</u>
2.	<u>971.2</u>	<u>943</u>	<u>13.146</u>	<u>172.87</u>	<u>26.92</u>	<u>967.98</u>	<u>32.32</u>	<u>961.4</u>	<u>943</u>
3.	<u>968.2</u>	<u>938</u>	<u>14.756</u>	<u>217.82</u>	<u>35.74</u>	<u>959.74</u>	<u>46.46</u>	<u>954.7</u>	<u>923</u>
4.	<u>605.2</u>	<u>366</u>	<u>14.989</u>	<u>224.68</u>	<u>16.79</u>	<u>908.99</u>	<u>99.12</u>	<u>909.2</u>	<u>549</u>
5.									

Absolute Potential: 13.176 MCFPD; n .587

COMPANY Simclair Oil & Gas Company

ADDRESS 500 East Broadway, Hobbs, New Mexico

AGENT and TITLE E. J. Barber Gas Analyst

WITNESSED E. J. Barber

COMPANY KiPass Natural Gas Company

## REMARKS

Orig. & 2 cc: New Mexico Oil Conservation Commission

cc: SW, PCR, WJR, 19D, GGS, FIRM

30 % pressure drop could not be maintained on this test due to the line capacity of the purchaser being inadequate and high line pressures on their system would not permit the volume to be maintained

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

$Q$  = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.

$P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia

$P_w$  = Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia

$P_t$  = Flowing wellhead pressure (tubing if flowing through tubing, casing if  
flowing through casing.) psia

$P_f$  = Meter pressure, psia.

$h_w$  = Differential meter pressure, inches water.

$F_g$  = Gravity correction factor.

$F_t$  = Flowing temperature correction factor.

$F_{pv}$  = Supercompressibility factor.

$n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .