			3	NEW MEXIC(	O OIL CON	SERVATIO	on commiss HO	ION BBS OFFIC	E 000		
								D		Form C-	
										Revised 12-1.	
	Eunoat										
Init	ial		Annual	<b>X</b>	Spe	cial		Date of	Test_9	-3-56	
Comp	any <u>Am<b>erad</b></u>	Pet. C	orp.		_Lease	Laughli	n	Wel	1 No	1	
Unit	_ <b>D</b>	Sec9_	Twp2	2 <b>05</b> _F	lge <b>37</b> .	EPur	chaser P	ermian Bas	in P.L.	Ce	
Casi	ng <b>6-5/8</b> " V	Wt. 20.0	<u>#_</u> I.D.	6.049" S	et at <u>3</u>	<b>800'</b> P	erf334	÷ 1	То3	1861	
Tubi	ng <b>3-1/2"</b>	Nt9.3	<b>I.</b> D	<b>2.992</b> * S	Set at <b>3</b>	<b>825'</b> P	erf382	21	То 3	3251	
	Pay: From										
Prod	ucing Thru:	Casi	ng <b>x</b>		ubing		Type We	all <b>G.O.</b>	Dual	/	
Date	ucing Thru: of Complet	ion <b>a</b>	-10_6/	Pack	or 275	Si	ngle-Brade	enhead-G.	G. or G.	.0. Dual	
	or compret							ort. Temb.		<u> </u>	
<b>.</b>	1 <b>(7</b> )	(-	<b>)</b> ( <b>-</b> , <b>-</b> ,	<b>N</b> <i>i</i>		VED DATA					
Test	ed Through	V() () () () ()		GOX (Meter	·)			Туре Тар	s <b>Pip</b>	<u>}</u>	
~	(Prover)		W Data	ss. Diff	• Temp.	Tubin	g Data	Casing Da	ata	Duratio	
No.	(Line)	(Orific	be) ps			1	1			of Flow	
SI	Size	5126	e ps.	ig h <sub>w</sub>	°F.	psig	°F.	psig 988.3	· F.	Hr.	
1.	<u> </u>	1.25	· 45	.9 7.6	82			840.7	7	71 hrs. 23-3/4 hrs.	
1. 2. 3.	<u></u>	1.25		.2 13.7	64			778.2		23-3/4 *	
4.	<u>k=</u>	1.25		.9 20.2	67		+	728.2		<u>24</u> * 24 *	
5.1								7			
					The second s	CULATIO	NS				
No.	Coeffici	ent		Pressure	1	Temp.	Gravity Factor	Compres Factor		late of Flow Q-MCFPD	
	(24-Hou	17) v	h <sub>w</sub> p <sub>f</sub>	psia	1	<sup>7</sup> t	Fg	Fpv		@ 15.025 psia	
1.	10.24		59.71		0.979		5 0.9427		1	588	
$\frac{1.}{2.}$ $\frac{3.}{4.}$ 5.			80.62		0.9962		0.9427	1.049		813	
<u> </u>			<b>98.17</b> 16.50		0.994		0.9427	1.04		987	
5.											
				P	RESSURE (	CALCUTAT:	IONS				
	lquid Hydro				_ cf/bbl.			fic Gravit			
Gravity of Liquid Hydrocarbons			deg.			Specific Gravity Flowing Fluid P <sub>c</sub> <b>1001.5</b> P <sup>2</sup> <b>1003.0</b>					
co <sub>2</sub>	2.09%	<b>N</b> 2	1.39%			-	<u> </u>				
No.	Pw	Pt <sup>2</sup>	F ()	(F <sub>c</sub> Q)	2 (1	2		$P_c^2 - P_w^2$			
	P <sub>t</sub> (psia)		F <sub>c</sub> Q			$\left[c_{e}^{Q}\right]^{2}$	P <sub>w</sub> 2	$r_c - r_{\tilde{w}}$	Cal P.	Pw Pc	
	853.9 791.4	729.1	0.8226	0.676		0974	729.2	273.8	853.9	85	
	741.4	549.7	1.381	1.907		2746	<u>626.5</u> 550.0	376.5	791.5		
	688.6	474.2	1.638	2.68		3864	474.6	528.4	688.9		
	l		ſ <u>(</u>		<u>_</u>	<u></u>		L	I		
Abso] COMPA	ute Porent	ial: da_Pet	2220		MCFPD;	n <b>1 (1</b>	dmited)				
ADDRE	SS Drame	r D - Me		New Mexic	0			2 11			
	and TITLE	W.G.	Abbett .	Dist. Er		NUS	I able	AF			
W1TNE COMPA		R.L. Permi		P.L. Co.			· · · _ · · · ·				
	<del></del>		<u></u>	<u> </u>		ARKS					

н с. I.

Slope (n) is in excess of 1.0 but, due to this being a retest, the test will be submitted with a slope of 1.0 down through the data point corresponding to the highest rate of flow.

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- Q = Actual rate of flow at end of flow period at W. H. working pressure ( $P_W$ ). MCF/da. @ 15.025 psia and 60° F.
- P<sub>c</sub>= 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- P<sub>w</sub>: Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia

Pf Meter pressure, psia.

hw Differential méter pressure, inches water.

FgI Gravity correction factor.

Ft Flowing temperature correction factor.

F <sub>py</sub> Supercompressability factor.	•		•
	*	*	
n _ Slope of back pressure curve.	r		,

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_+$ .