

## NEW MEXICO OIL CONSERVATION COMMISSION

Form C-122

Revised 12-1-55

## MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Pool Dumont Formation Yates County Lea  
Initial Annual X Special          Date of Test 6/13/56  
Company Shelly Oil Co. Lease Van Etten Well No. 9  
Unit L Sec. 9 Twp. 20S Rge. 37E Purchaser Southern Union Gas Co.  
Casing 7" Wt. 20# I.D. 6.456 Set at 3531 Perf. 3220 To 3240  
Tubing 2 1/2" Wt. 6.5# I.D. 2.441 Set at 3766 Perf. 3761 To 3766  
Gas Pay: From 3220 To 3747 L 3761 xG 0.654 -GL 2460 Bar.Press. 13.2  
Producing Thru: Casing          Tubing X Type Well Single  
Single-Bradenhead-G. G. or G.O. Dual  
Date of Completion:          Packer          Reservoir Temp.         

## OBSERVED DATA

Tested Through (Dumont) (Choke) (Meter) Type Taps Flange

No.	Flow Data					Tubing Data		Casing Data		Duration of Flow Hr.
	(Prover) (Line) Size	(Choke) (Orifice) Size	Press. psig	Diff. h <sub>w</sub>	Temp. °F.	Press. psig	Temp. °F.	Press. psig	Temp. °F.	
SI								916		72
1.	4"	1"	510	15	82			871		24
2.	"	1"	530	76	75			811		"
3.	"	1"	540	26	74			767		"
4.	"	3/8"	644	*	72			-		"
5.										

\* No. 4 test was taken with a critical flow prover.

## FLOW CALCULATIONS

No.	Coefficient (24-Hour)	$\sqrt{h_{wpf}}$	Pressure psia	Flow Temp. Factor F <sub>t</sub>	Gravity Factor F <sub>g</sub>	Compress. Factor F <sub>pv</sub>	Rate of Flow Q-MCFPD @ 15.025 psia
1.	6.135	88.6	523.2	0.9795	0.9578	1.047	534
2.	"	203.2	543.2	0.9899	"	1.053	1239
3.	"	119.9	553.2	0.9863	"	1.054	7328
4.	3.039	-	657.2	0.9887	"	1.064	2012
5.							

## PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio          cf/bbl.  
Gravity of Liquid Hydrocarbons          deg.  
F<sub>c</sub> 5.866 (1-e<sup>-s</sup>) 0.156  
Specific Gravity Separator Gas           
Specific Gravity Flowing Fluid           
P<sub>c</sub> 929.2 P<sub>c</sub> 863.4

No.	P <sub>w</sub> P <sub>t</sub> (psia)	P <sub>t</sub> <sup>2</sup>	F <sub>c</sub> Q	(F <sub>c</sub> Q) <sup>2</sup>	(F <sub>c</sub> Q) <sup>2</sup> (1-e <sup>-s</sup> )	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>	Cal. P <sub>w</sub>	P <sub>w</sub> /P <sub>c</sub>
1.	801.2	781.8	3.13	9.80	1.53	783.3	80.1	885.0	0.95
2.	824.2	679.3	7.27	52.85	8.21	687.5	175.9	829.2	0.89
3.	780.2	606.7	4.30	18.49	2.88	611.6	25.6	782.0	0.84
4.									
5.									

Absolute Potential: 24,700 MCFPD; n 1.0000  
COMPANY Shelly Oil Co.  
ADDRESS Box 38, Hobbs, N. M.  
AGENT and TITLE (SIGNED) H. E. AGS Dist. Supt.  
WITNESSED None  
COMPANY         

## REMARKS

Peer point alignment so a slope of 1.0 was drawn through the point representing the highest flow rate.

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

$Q$  = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.

$P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia

$P_w$  = Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia

$P_t$  = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia

$P_f$  = Meter pressure, psia.

$h_w$  = Differential meter pressure, inches water.

$F_g$  = Gravity correction factor.

$F_t$  = Flowing temperature correction factor.

$F_{pv}$  = Supercompressibility factor.

$n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .