Form C-122

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Revised 12-1-55

Date of Test Second Date of Test	ool Eumont		Fc	rmation_	99900	B PM	5:51	County	Lea 6	-19-56
Lease J. W. Cooper Mell No.	nitial 🛣	Anni	ual		Spec	ial		_Date of :	Test	-27-56
No. 14	ompany The Tex	каз Сощра	ny	I	Lease J.	W. Goo	per	Well	No. 5	
Asing 52 Wt. 14# I.D. 5.012 Set at 3300 Perf. To abing 2 3/6 Wt. 4.70 I.D. 1.995 Set at 3480 Perf. 3470 To 3473 As Pay: From 3300 To 3500 L 3470 xG .675 -GL 2342 Bar.Press. Troducing Thru: Casing Tubing X Type Well Single Sate of Completion: 2-24-54 Packer Bone Single-Bradenhead-G. G. or G.O. Dual Reservoir Temp. Asset of Troops (TROOPS) (Meter) Tubing Data Casing Data Provided (Circles Press. Diff. Temp. Press. Temp. Press. Temp. Or Flow (Line) (Circles Press. Diff. Temp. Press. Temp. Press. Temp. Duration (Line) (Circles Press. Diff. Temp. Press. Temp. Press. Temp. Size Size Size psig hw Op. psig Op. in. A 1.75 \$5.25.5 Press. Press. Press. Press. Press. Temp. Press. Temp. Press. Temp. Press. Temp. Or Flow (Line) (Circles Press. Press. Press. Press. Press. Temp. P										
Single										
Reservoir From 3300 To 3500 L 3470 xG .675 TGL 2342 Bar.Press. Reservoir True: Casing					5.					
Tubing T										
Coefficient										
Coefficient	roducing Thru:	Casing_		Tul	oing	Sing	_Type we le-Brade	nhead-G.	G. or G	.O. Dual
Prove	ate of Complet	ion:	4-24	Packer	RORE		_Reservo	ir Temp		
Flow Data	102= 1.64%	No= 1.54	*		OBSERV.	ED DATA				
Continue	ested Through	(Prover)	(cnoke)	(Meter)				Type Tap	sP	ipe
Coefficient Coeff		Flow	Data			Tubing	Data			
Size psig				Diff.	Temp.	Press.	Temp.	Press.	Temp.	Duration of Flo
	, , ,			h _w	o _F .	psig	°F.	psig	[⊃] F•	li de la constantia de la
FLOW CALCULATIONS FRACTOR FACTOR FACTOR FACTOR Q-MCFPD Q-MC	I									
Pressure Flow Calculations Factor	. 4									
Pressure Flow Calculations Factor					75					
Pressure Prow CALCULATIONS Rate of Flow Pressure Prow Temp. Factor Fac	. 4				79	598.4		685.7	 	24
Pactor Factor F	<u> </u>			<u>. I </u>	FLOW CAL	CULATION	S			
(24-Hour)	ſ	ient	Pressure				•			
PRESSURE CALCULATIONS Specific Gravity Separator Gas Specific Gravity Flowing Fluid Pt Pt Pt Pt Pt Pt Pt P		$ar)$ \sqrt{h}	wPf	psia						
PRESSURE CALCULATIONS s Liquid Hydrocarbon Ratio cf/bbl. Specific Gravity Separator Gas. 67 avity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid Pc 998.7 Pc 997.4 [O. Pw Pt (psia) Pt FcQ (FcQ)2 (FcQ)2 (FcQ)2 Pw2 Pc-Pw Pc Pc Pc Pw Pc Pc Pc Pw Pc Pc Pc Pc Pw Pc Pc Pc Pc Pc Pc Pc Pw Pc				67.5			.9427	1,0		1,327
PRESSURE CALCULATIONS s Liquid Hydrocarbon Ratio cf/bbl. Specific Gravity Separator Gas. 67 avity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid Pc 998.7 Pc 997.4 [O. Pw Pt (psia) Pt FcQ (FcQ)2 (FcQ)2 (FcQ)2 Pw2 Pc-Pw Pc Pc Pc Pw Pc Pc Pc Pw Pc Pc Pc Pc Pw Pc Pc Pc Pc Pc Pc Pc Pw Pc	21.69	9:	1.55		.985	9	.9427			2.015
PRESSURE CALCULATIONS s Liquid Hydrocarbon Ratio cf/bbl. Specific Gravity Separator Gas. 67 avity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid Pc 998.7 Pc 997.4 [O. Pw Pt (psia) Pt FcQ (FcQ)2 (FcQ)2 (FcQ)2 Pw2 Pc-Pw Pc Pc Pc Pw Pc Pc Pc Pw Pc Pc Pc Pc Pw Pc Pc Pc Pc Pc Pc Pc Pw Pc	21.69				.982	2	.9427			3.096
S Liquid Hydrocarbon Ratio cf/bbl. avity of Liquid Hydrocarbons deg. (1-e-s) Specific Gravity Separator Gas. Specific Gravity Flowing Fluid Pc 998.7 Pc 997.4 Co. Pw Pt (psia) Pt FcQ (FcQ) ² (FcQ) ² Pw ² Pc-Pw Cal. Pw Pc Specific Gravity Flowing Fluid Pc 998.7 Pc 997.4 Cal. Pw Pc Pw Pc Specific Gravity Flowing Fluid Pc 998.7 Pc 997.4 Cal. Pw Pc Pw Pc Specific Gravity Flowing Fluid Pc 998.7 Pc 997.4 Cal. Pw Pc Pw Pc Specific Gravity Flowing Fluid Pc 998.7 Pc 997.4 Cal. Pw Pc Pw Pc Pw Pc Specific Gravity Flowing Fluid Pc 998.7 Pc 997.4 Cal. Pw Pc P										
avity of Liquid Hydrocarbons deg. Specific Gravity Flowing Fluid P _C 998.7 P _C 997.4 [O. P _W P _t (psia) P _t P _t F _c Q (F _c Q) ² (F _c Q) ² P _w ² P _c ² P _w ² P _c ² P _w P _t P _t (psia) P _t				PR	ESSURE C	CALCULATI				۷.
(1-e-s) P _C 998.7 P _C 997.4 (1-e-s) P _C 998.7 P _C 998.7 P _C 998.7 P _C 997.4 (1-e-s) P _C 998.7 P _C 997.4 (1-e-s)	s Liquid Hydro	ocarbon Rat	io				Spec	ific Gravi	ty Sepa	arator Gas
Pw	•		ons (1-e ^{-s})		aeg.		P _C _	98.7	P _c 99	7.4
Pt (psia)			- · · · · ·	-						
Second to the se		2		/ \2) /-	2012	D ()	p ² p ²	C	21 P
Second to the se	Dr (neis)	Pt	FcQ	(F _c Q)~		(cQ) L-e-s)	$P_{\mathbf{w}}^{\sim}$	Pc-rw	, C	P_{W} P_{C}
Absolute Potential: 5,280 MCFPD; n_80 COMPANY ADDRESS BOX 1270 Maland 1988 GENT and TITLE J. Below Bistrics Gas Man VITNESSED Repress	902.0									.90
Absolute Potential: 5,280 MCFPD; n_80	119.0							385.1		
Absolute Potential: 5,280 MCFPD; n80		 								
COMPANY ADDRESS Box 1270 Milend Fexas AGENT and TITLE VITNESSED N. R. Berrett	5.									
ADDRESS Box 1270 Midland Toxas AGENT and TITLE L. I. Befor District Gas Man VITNESSED H. E. Berrott	bsolute Poten	tjal: 5		<u> </u>	MCFPD	; n <u> </u>				
GENT and TITLE L. I. Being Bistrict Gas Man / 1000km	COMPANY	The			Taya	.				
VITNESSED B. E. Berrott			Bain				L	Mon	kin	
	VI:TNESSED	H. E		220			<u> </u>			

INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

- Q I Actual rate of flow at end of flow period at W. H. working pressure ($P_{\rm W}$). MCF/da. @ 15.025 psia and 60° F.
- P_c = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater. psia
- P_{w} Static wellhead working pressure as determined at the end of flow period. (Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- Pt Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia
- Pf Meter pressure, psia.
- hw Differential meter pressure, inches water.
- Fg Gravity correction factor.
- Ft⊆ Flowing température correction factor.
- F_{DV} Supercompressability factor.
- n I Slope of back pressure curve.

Note: * If P_w cannot be taken because of manner of completion or condition of well, then P_w must be calculated by adding the pressure drop due to friction within the flow string to P_t .