

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 3-15-79	
Company Texas Oil & Gas Corporation						Connection	
Pool Undes. N. Osudo						Formation Morrow	
Completion Date 1/15/79		Total Depth 11600		Plug Back TD 11420		Elevation 3655 KB	
Farm or Lease Name Osudo State						Well No. 1	
Csg. Size 4 1/2"	Wt. d	d Set At	Set At 11600	Perforations: From 11,324 To 11,340		Unit Sec. Twp. Rge. D 29 20S 36E	
Tbg. Size 2 3/8"	Wt. 4.7#	d Set At	Set At 11,175	Perforations: From Open Ended		County Lea	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single						Packer Set At 11,175	
Producing Thru Tubing		Reservoir Temp. °F 194 @ 11,332		Mean Annual Temp. °F 13.2		State New Mexico	
L 11,332	H	Gg .616	% CO ₂ .27	% N ₂ .42	% H ₂ S Trace	Prover X	Meter Run Flange

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							3779	57			
1.	6"	x	1.875"	99	19	75	3737	60			.75 Hr.
2.	6"	x	1.875"	124	52	73	3664	62			1 Hr.
3.	6"	x	1.875"	132	65	71	3650	64			.5 Hr.
4.	6"	x	3.500"	225	15	38	3292	68			1 Hr.
5.	6"	x	3.500"	416	32	30	2389	69			1 Hr.

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	16.80	46.171	112.2	.9859	1.274	1.009	983
2	16.80	84.465	137.2	.9877	1.274	1.011	1805
3	16.80	97.149	145.2	.9896	1.274	1.012	2082
4	62.47	59.774	238.2	1.022	1.274	1.025	4983
5	62.47	117.194	429.2	1.030	1.274	1.051	10097

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio 117.8 Mcf/bbl.
1.	.16	535	1.47	.982	A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2.	.20	533	1.46	.978	Specific Gravity Separator Gas _____ X X X X X X X X
3.	.21	531	1.46	.977	Specific Gravity Flowing Fluid _____ X X X X X
4.	.35	498	1.37	.952	Critical Pressure 671 P.S.I.A. _____ P.S.I.A.
5.	.64	490	1.35	.906	Critical Temperature 364 R _____ R

P _f 4887.2 P _s 23,885					(1) $\frac{P_f^2}{P_f^2 - P_s^2} = 2.949$	(2) $\left[\frac{P_f^2}{P_f^2 - P_s^2} \right]^n = 2.560$
NO.	P _t ²	P _s ²	P _s ²	P _f ² - P _s ²	AOF = Q $\left[\frac{P_f^2}{P_f^2 - P_s^2} \right]^n = 25,844$	
1		4861.2	23,631	254		
2		4810.2	23,138	747		
3		4772.2	22,774	1111		
4		4517.2	20,405	3480		
5		3973.2	15,786	8099		

Absolute Open Flow 27,500 Mcfd @ 15.025	Angle of Slope Θ 49	Slope, n .869
Remarks:		
Approved By Commission:	Conducted By:	Calculated By:
Checked By:		

RECEIVED

MAR 19 1979

**OIL CONSERVATION COMM.
BOBBS, N. M.**