

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 2-7-82	
Company AMOCO PRODUCTION COMPANY				Connection EL PASO NATURAL GAS			
Pool MONUMENT DRAW				Formation MORROW		Unit F	
Completion Date 12 17 81		Total Depth 13588.		Plug Back TD 13500.		Elevation 3674.	
Form or Lease Name WATKINS GAS COM B							
Csg. Size 4.500		Wt. 15.1		Set At 3.826		Perforations: From 13177. To 13400.	
Trg. Size 2.375		Wt. 4.7		Set At 1.995		Perforations: From 0 To 0	
Well No. 1							
Unit Sec. Twp. Rge. K 23 20S 35E							
Type Well - Single - Dradhead - G.C. or G.O. Multiple SINGLE						Packer Set At 9858.	
Producing Thru TUBING		Reservoir Temp. °F 196.0 13288.		Mean Annual Temp. °F 60.0		Baro. Press. - P _a 13.2	
State NEW MEXICO							
L 13288.		H 13288.		G _g 0.666		% CO ₂ 0.62	
				% N ₂ 0.68		% H ₂ S 0.	
				Prover 0.		Meter Run 4.0 FLANGE	
						Taps	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							4317.	66.			72.0
1.	4.00 x 2.750			640.	5.3	46.	2605.	64.	0.	0.	0.7
2.	4.00 x 2.750			704.	7.3	60.	2072.	67.	0.	0.	0.7
3.	4.00 x 2.750			731.	10.9	63.	1621.	70.	0.	0.	0.7
4.	4.00 x 2.750			714.	11.6	64.	1321.	66.	0.	0.	0.7
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	41.23	58.78	653.2	1.0137	1.2252	1.0798	3250.
2	41.23	72.31	717.2	1.0000	1.2252	1.0785	3939.
3	41.23	90.02	744.2	0.9971	1.2252	1.0795	4895.
4	41.23	91.69	727.2	0.9962	1.2252	1.0769	4969.
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1.	0.97	506.	1.34	0.858	4.2	48.0	0.666	XXXXXX	671.	376.
2.	1.07	520.	1.38	0.860					P.S.I.A.	R
3.	1.11	523.	1.39	0.858						
4.	1.08	524.	1.39	0.862						
5.										

P _c 4339.10 P _c ² 18828.					$(1) \frac{P_c^2}{P_c^2 - P_w^2} = 1.1239$ $(2) \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.1239$	
NO.	P _r ²	P _w	P _w ²	P _c ² - P _w ²	$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 5585.$	
1	6855.	2666.	7109.	11719.		
2	4348.	2149.	4616.	14212.		
3	2671.	1728.	2985.	15843.		
4	1780.	1441.	2076.	16752.		
5						

Absolute Open Flow 5585.		Mcf/d @ 15.025		Angle of Slope θ 45.0		Slope, n 1.000	
Remarks:							

Approved By Jerry Sexton Dist. L. Suggs	Conducted By:	Calculated By: Barbara Hemmeline	Checked By:
---	---------------	-------------------------------------	-------------