

Submit in duplicate to
appropriate district office
See Rule 401 & Rule 1122

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator ORYX ENERGY						Lease or Unit Name MAVEETY STATE GAS COM					
Type Test ☒ Initial ☐ Annual ☐ Special						Test Date 2-2-94		Well No. 9			
Completion Date 12-13-93			Total Depth 3700		Plug Back TD 3643		Elevation		Unit 35 Sec 19S TWP 36E Rge.		
Csg. Size	Wt.	d	Set At	Perforations:				County			
5 1/2	15.5	4.950	3700'	From: 2814 To: 3584				LEA			
Tbg. Size	Wt.	d	Set At	Perforations:				Pool			
2 3/8	4.7	1.995	2771'	From: To:							
Type Well - Single - Bradenhead - G.G. or P.O. Multiple single						Packer Set At 2771		Formation EUMONT			
Producing Thru tbg		Reservoir Temp. °F 88		Mean Annual Temp. °F 60		Baro. Press - P _a 13.2		Connection PIPELINE			
L 3199	H 3199	Gg .720	% CO ₂ 4.28	% N ₂ 1.55	% H ₂ S	Prover none	Meter Run 3.068	Taps fig.			

FLOW DATA					TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
1.	3.068	X 1.75	11.8	.5	46	110	42	PKR.		60 min
2.	3.068	X 1.75	13.2	1.8	51	106	47			60 min
3.	3.068	X 1.75	13.5	5.8	57	103	47			60 min
4.	3.068	X 1.75	13.4	13.2	60	100	47			60 min
5.						94	47			60 min

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	h _w P _m	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{sp}	Rate of Flow Q, Mcfd
1.	15.61	3.54	25	1.014	1.179	1.004	66
2.	15.61	6.89	26.4	1.009	1.179	1.003	128
3.	15.61	12.44	26.7	1.003	1.179	1.003	230
4.	15.61	18.74	26.6	1.000	1.179	1.003	346
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	DRY GAS	Mcf/bbl.
1.	.037	506	1.30	.993	A.P. I. Gravity of Liquid Hydrocarbons	DRY	Deg.
2.	.039	511	1.32	.994	Specific Gravity Separator Gas	.720	XXXXXXXXXX
3.	.039	517	1.33	.994	Specific Gravity Flowing Fluid	DRY	XXXXXXXXXX
4.	.039	520	1.34	.994	Critical Pressure	684	P.S.I.A. P.S.I.A.
5.					Critical Temperature	388	R R

p_c **123.2** p_c² **15.2**

NO.	p _t ²	p _w	p _w ²	p _c ² - p _w ²
1.		119.4	14.3	.9
2.		117.0	13.7	1.5
3.		115.9	13.4	1.7
4.		113.6	12.9	2.3
5.				

1) $\frac{p_c^2}{p_c^2 - p_w^2} = 6.702$

AOF = Q $\left[\frac{p_c^2}{p_c^2 - p_w^2} \right]^n = 2,319$

(2) $\left[\frac{p_c^2}{p_c^2 - p_w^2} \right]^n = 6.702$

Absolute Open Flow 2,319 Mcfd @ 15.025	Angle of Slope Θ 45°	Slope, n 1.000
---	-----------------------------	-----------------------

Remarks: **NO FLUID MADE DURING TEST**

Approved By Division	Conducted By: PRO WELL TESTERS	Calculated By: K.S.	Checked By: B.M.
----------------------	---------------------------------------	----------------------------	-------------------------