

NEW MEXICO OIL CONSERVATION COMMISSION

HOBBS OFFICE OCC

Form C-122

Revised 12-1-55

HOBBS OFFICE OCC

1956 SEP 30

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Pool Eumont Gas Formation Queen County LeaInitial _____ Annual _____ Special X (Retest) Date of Test Sept. 3, 1956Company Schermerhorn Oil Corp. Lease Christmas Well No. 1Unit D Sec. 11 Twp. 20 S Rge. 37 E Purchaser Permian Basin Pipeline Co.Casing 5 1/2" Wt. 14.0# I.D. 5.012" Set at 3663' Perf. _____ To _____Tubing 2 3/8" Wt. 4.7# I.D. 1.995" Set at 3745' Perf. _____ To _____Gas Pay: From 2660' To 3775' L 3663' xG 0.665 -GL 2436' Bar.Press. 13.2Producing Thru: Casing X Tubing _____ Type Well Single Completion

Single-Bradenhead-G. G. or G.O. Dual

Date of Completion: 12-1-58 Packer _____ Reservoir Temp. _____

OBSERVED DATA

Tested Through (~~Pressure~~) (~~Choke~~) (Meter) _____ Type Taps Pipe

No.	Flow Data					Tubing Data		Casing Data		Duration of Flow Hr.
	(Pressure) (Line) Size	(Choke) (Orifice) Size	Press. psig	Diff. h _w	Temp. °F.	Press. psig	Temp. °F.	Press. psig	Temp. °F.	
SI								<u>910.4</u>		<u>72 Hr. S.I.</u>
1.	<u>4"</u>	<u>1.250"</u>	<u>450.6</u>	<u>9.0</u>	<u>61</u>			<u>747.5</u>		<u>24 Hr.</u>
2.	<u>4"</u>	<u>1.250"</u>	<u>456.5</u>	<u>12.9</u>	<u>61</u>			<u>690.7</u>		<u>24 Hr.</u>
3.	<u>4"</u>	<u>1.250"</u>	<u>455.7</u>	<u>20.2</u>	<u>64</u>			<u>618.1</u>		<u>24 Hr.</u>
4.	<u>4"</u>	<u>1.250"</u>	<u>455.0</u>	<u>27.1</u>	<u>65</u>			<u>551.4</u>		<u>24 Hr.</u>
5.										

FLOW CALCULATIONS

No.	Coefficient (24-Hour)	$\sqrt{h_{wpf}}$	Pressure psia	Flow Temp. Factor F _t	Gravity Factor F _g	Compress. Factor F _{pv}	Rate of Flow Q-MCFPD @ 15.025 psia
1.	<u>10.24</u>	<u>64.61</u>		<u>0.9990</u>	<u>0.9498</u>	<u>1.050</u>	<u>659</u>
2.	<u>10.24</u>	<u>77.84</u>		<u>0.9990</u>	<u>0.9498</u>	<u>1.050</u>	<u>794</u>
3.	<u>10.24</u>	<u>97.82</u>		<u>0.9962</u>	<u>0.9498</u>	<u>1.050</u>	<u>980</u>
4.	<u>10.24</u>	<u>112.60</u>		<u>0.9952</u>	<u>0.9498</u>	<u>1.048</u>	<u>1142</u>
5.							

PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio Dry Gas cf/bbl.
Gravity of Liquid Hydrocarbons _____ deg.
F_c 1.712 (1-e^{-s}) 0.154Specific Gravity Separator Gas _____
Specific Gravity Flowing Fluid _____
P_c 928.6 P_c² 858.0

No.	P _t (psia)	P _t ²	F _c Q	(F _c Q) ²	(F _c Q) ² (1-e ^{-s})	P _w ²	P _c ² -P _w ²	Cal. P _w	P _w / P _c
1.	<u>760.7</u>	<u>578.7</u>	<u>1.128</u>	<u>1.272</u>	<u>0.1959</u>	<u>578.9</u>	<u>274.1</u>	<u>760.9</u>	<u>82.4</u>
2.	<u>709.9</u>	<u>495.5</u>	<u>1.359</u>	<u>1.847</u>	<u>0.2844</u>	<u>495.8</u>	<u>357.2</u>	<u>704.1</u>	<u>78.2</u>
3.	<u>681.3</u>	<u>398.5</u>	<u>1.695</u>	<u>2.878</u>	<u>0.4424</u>	<u>398.9</u>	<u>454.1</u>	<u>681.6</u>	<u>68.4</u>
4.	<u>564.6</u>	<u>318.8</u>	<u>1.955</u>	<u>3.822</u>	<u>0.5886</u>	<u>319.4</u>	<u>583.6</u>	<u>565.2</u>	<u>61.2</u>
5.									

Absolute Potential: 1.735 MCFPD; n 0.89COMPANY Schermerhorn Oil CorporationADDRESS Box 1537, Hobbs, New MexicoAGENT and TITLE J. H. Moore, GeologistWITNESSED H. E. BarrettCOMPANY Permian Basin Pipeline Company, Box 2376, Hobbs, New Mexico

REMARKS

CO₂ and N₂ content of gas is negligible.

INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

Q = Actual rate of flow at end of flow period at W. H. working pressure (P_w).
MCF/da. @ 15.025 psia and 60° F.

P_c = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.
psia

P_w = Static wellhead working pressure as determined at the end of flow period.
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia

P_t = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia

P_f = Meter pressure, psia.

h_w = Differential meter pressure, inches water.

F_g = Gravity correction factor:

F_t = Flowing temperature correction factor.

F_{pv} = Supercompressability factor.

n = Slope of back pressure curve.

Note: If P_w cannot be taken because of manner of completion or condition of well, then P_w must be calculated by adding the pressure drop due to friction within the flow string to P_t .