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rilling of ame of levation he infor o. 1, fro o. 2, fro o. 3, fro nclude d o. 1, fro	commenced drilling co above sea mation give m m m ata on rate om	atractor E level at S in is to be ke 30 of water in	3-3 • Line r 1 ept confiden to to to to flow and e	19 34 19 34 10	Drilling feet. DS OR ZONH No. 4, from No. 5, from No. 6, from F WATER Schich water roce	Was com Address DOPT ES om om om ANDS ose in ho	ipleted Tuls Lok 71	4-3 4-3 4-3 4-3 4-3 4-3 4-3 4-3 4-3 4-3 4-3 4-3 4-3 4-3 4-3 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4-5 4	9 1 9	19
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MUDDING AND CEMENTING RECORD

SIZE OF HOLE	SIZE OF CASING	WHERE SET	NO. SACKS OF CEMENT	METHOD USED	MUD GRAVITY	AMOUNT OF MUD USED
1	0-3/4	119'	125	Halliburton		
	7-5/8	1846'	800	*		
	5-1/2	3666*	150	*		

PLUGS AND ADAPTERS

Heaving plug-Material____ ____Length_____Depth Set____

Adapters----Material______Size_____

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RECORD OF SHOOTING OR CHEMICAL TREATMENT

SIZE	SHELL USED		PLOSIVE OR MICAL USED	QUANTITY	DATE	DEPTH SHOT OR TREATED	DEPTH CLEANED OUT
		Ches	1700948	10000	4-4-39	38401	
		*	*	20000	4-6-89	36501	
		40	*	20000	4-13-39	3830'	

Results of shooting or chemical treatment_____

RECORD OF DRILL-STEM AND SPRCIAL TESTS

If drill-stem or other special tests or deviation surveys were made, submit report on separate sheet and attach hereto.

	TOOLS USED		
Rotary tools were used fromfeet to	feet, and from	feet to	feet
Cable tools were used fromfeet tofeet	feet, and from	feet to	feet
	PRODUCTION		
Put to producing	19_39_		
The production of the first thours was		n% was oil;	^~/o
emulsion;% water; and	% sediment. Gravity, Be	\$.0	<u> </u>
If gas well, cu, ft. per 24 hours	Gallons gasoline per 1,	000 cu. ft. of gas	
Rock pressure, lbs. per sq. in	Oas 011 Satio	- 937	
	EMPLOYEES		
	Driller T. C. CO	16888	Driller
l. C. Cornett	Driller	,	Driller

FORMATION RECORD ON OTHER SIDE

I hereby swear or affirm that the information given herewith is a complete and correct record of the well and all work done on it so far as can be determined from available records.

Subscribed and sworn to before me this	Midland, Texas, May 9th, 1939.
day of 19 39	Place Date
day of the Unit man	Position District Superintendent
// Notary Public	Ronresonting The Texas Several

FORMATION RECORD

	TO	THICKNESS IN FEET	FORMATION
0	40	40	Sand & Caliche
40	85	45	Sand & Clay
85	130	45	244 Beds
120 210	340	210	Red Bods & Send Rock
1080	1082 1175	872 93	
1175	1226	53	Anhydrite & Shale Anhydrite & Sed Bods
1228	1255	27	Ashritte
1255	1870	18	Broken Ankydrite
1870	2040	770	Anhydrits à Salt
2040	2140	100	Broken anhydrite
2140 2250	1250 1420	110 176	Balt, Potash, Anhydrite Shelle
2480	2460	40	Anhydrite & Salt Anhydrite & Line
2460	2561	101	Anhydrite
A561	2600	39	Anhydrite, Lime, & Sand
2600	1893	293	Annyerite
5983	2977	84	Ashydrite & Line
29 77 2995	299 8 3060	18	Line
3060	3449	65 389	Line & Anhydrite Line
3449	3443	14	dendy Line
3483	3543	A Q	Line
8843	3677	34	Line & Sund
3377	3874	297	1.1.200
TOTAL	VITTI: 387	' 4'	
Toral (NFTH: 387	* * *	Deviation Tests As Follows:
TOTAL L	nft h: 387	* * *	1
Toral (NFTH: 387	* * *	1
TUTAL (* *	XFYH: 387	* 4 *	1
TOTAL F	NFTH: 387	* * *	1
TOTAL	NF TH: 387	* * *	1
TOTAL	NFY H: 387	* 4 *	1
TUTAL (*	NF TH: 387	* 6*	$\begin{array}{rcl} 500^{\circ} & - 1/2^{\circ} \\ 1090^{\circ} & - 0^{\circ} \\ 1885^{\circ} & - 2^{\circ} \\ 1800^{\circ} & - 1^{\circ} \\ 2000^{\circ} & - 1^{\circ} \\ 2414^{\circ} & - 1-1/2^{\circ} \\ 2370^{\circ} & - 2^{\circ} \end{array}$
TUTAL	XFYR: 387	* 4 *	$\begin{array}{rcl} 500^{\circ} & - 1/2^{\circ} \\ 1090^{\circ} & - 0^{\circ} \\ 1885^{\circ} & - 2^{\circ} \\ 1800^{\circ} & - 1^{\circ} \\ 2000^{\circ} & - 1^{\circ} \\ 2414^{\circ} & - 1-1/2^{\circ} \\ 2570^{\circ} & - 2^{\circ} \end{array}$
TOTAL	NFY H: 387	* * *	$\begin{array}{rcl} 500^{\circ} & - 1/2^{\circ} \\ 1090^{\circ} & - 0^{\circ} \\ 1885^{\circ} & - 2^{\circ} \\ 1800^{\circ} & - 1^{\circ} \\ 2000^{\circ} & - 1^{\circ} \\ 2414^{\circ} & - 1-1/2^{\circ} \\ 2370^{\circ} & - 2^{\circ} \end{array}$
	NF 18: 389	* 6 *	$\begin{array}{rcl} 500^{\circ} & - 1/2^{\circ} \\ 1090^{\circ} & - 0^{\circ} \\ 1885^{\circ} & - 2^{\circ} \\ 1800^{\circ} & - 1^{\circ} \\ 2000^{\circ} & - 1^{\circ} \\ 2414^{\circ} & - 1-1/2^{\circ} \\ 2370^{\circ} & - 2^{\circ} \end{array}$
	NF 18: 387	Y 4 ?	$\begin{array}{rcl} 500^{\circ} & - 1/2^{\circ} \\ 1090^{\circ} & - 0^{\circ} \\ 1885^{\circ} & - 2^{\circ} \\ 1800^{\circ} & - 1^{\circ} \\ 2000^{\circ} & - 1^{\circ} \\ 2414^{\circ} & - 1-1/2^{\circ} \\ 2370^{\circ} & - 2^{\circ} \end{array}$
	NF 1 H: 387	* 6 *	$\begin{array}{rcl} 500^{\circ} & - 1/2^{\circ} \\ 1090^{\circ} & - 0^{\circ} \\ 1885^{\circ} & - 2^{\circ} \\ 1800^{\circ} & - 1^{\circ} \\ 2000^{\circ} & - 1^{\circ} \\ 2414^{\circ} & - 1-1/2^{\circ} \\ 2370^{\circ} & - 2^{\circ} \end{array}$
	XFXH: 387	* 4 *	$\begin{array}{rcl} 500^{\circ} & - 1/2^{\circ} \\ 1090^{\circ} & - 0^{\circ} \\ 1885^{\circ} & - 2^{\circ} \\ 1800^{\circ} & - 1^{\circ} \\ 2000^{\circ} & - 1^{\circ} \\ 2414^{\circ} & - 1-1/2^{\circ} \\ 2370^{\circ} & - 2^{\circ} \end{array}$
	NF 18: 387	Y 4 7	$\begin{array}{rcl} 500^{\circ} & - 1/2^{\circ} \\ 1090^{\circ} & - 0^{\circ} \\ 1885^{\circ} & - 2^{\circ} \\ 1800^{\circ} & - 1^{\circ} \\ 2000^{\circ} & - 1^{\circ} \\ 2414^{\circ} & - 1-1/2^{\circ} \\ 2370^{\circ} & - 2^{\circ} \end{array}$
	N.F. 387	* 6 *	$\begin{array}{rcl} 500^{\circ} & - 1/2^{\circ} \\ 1090^{\circ} & - 0^{\circ} \\ 1885^{\circ} & - 2^{\circ} \\ 1800^{\circ} & - 1^{\circ} \\ 2000^{\circ} & - 1^{\circ} \\ 2414^{\circ} & - 1-1/2^{\circ} \\ 2370^{\circ} & - 2^{\circ} \end{array}$
	NF 18: 387	Y 4 *	$\begin{array}{rcl} 500^{\circ} & - 1/2^{\circ} \\ 1090^{\circ} & - 0^{\circ} \\ 1885^{\circ} & - 2^{\circ} \\ 1800^{\circ} & - 1^{\circ} \\ 2000^{\circ} & - 1^{\circ} \\ 2414^{\circ} & - 1-1/2^{\circ} \\ 2370^{\circ} & - 2^{\circ} \end{array}$
	NJ XI 387	Y 4 7	$\begin{array}{rcl} 500^{\circ} & - 1/2^{\circ} \\ 1090^{\circ} & - 0^{\circ} \\ 1885^{\circ} & - 2^{\circ} \\ 1800^{\circ} & - 1^{\circ} \\ 2000^{\circ} & - 1^{\circ} \\ 2414^{\circ} & - 1-1/2^{\circ} \\ 2370^{\circ} & - 2^{\circ} \end{array}$
	XIX: 387	* * *	$\begin{array}{rcl} 500^{\circ} & - 1/2^{\circ} \\ 1090^{\circ} & - 0^{\circ} \\ 1885^{\circ} & - 2^{\circ} \\ 1800^{\circ} & - 1^{\circ} \\ 2000^{\circ} & - 1^{\circ} \\ 2414^{\circ} & - 1-1/2^{\circ} \\ 2370^{\circ} & - 2^{\circ} \end{array}$
	NYYH: 387	Y 4 ?	$\begin{array}{rcl} 500^{\circ} & - 1/2^{\circ} \\ 1090^{\circ} & - 0^{\circ} \\ 1885^{\circ} & - 2^{\circ} \\ 1800^{\circ} & - 1^{\circ} \\ 2000^{\circ} & - 1^{\circ} \\ 2414^{\circ} & - 1-1/2^{\circ} \\ 2370^{\circ} & - 2^{\circ} \end{array}$
	NJ XI : 387	Y 4 7	$\begin{array}{rcl} 500^{\circ} & - 1/2^{\circ} \\ 1090^{\circ} & - 0^{\circ} \\ 1885^{\circ} & - 2^{\circ} \\ 1800^{\circ} & - 1^{\circ} \\ 2000^{\circ} & - 1^{\circ} \\ 2414^{\circ} & - 1-1/2^{\circ} \\ 2370^{\circ} & - 2^{\circ} \end{array}$