

NEW MEXICO OIL CONSERVATION COMMISSION

HOBBS OFFICE OCC

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

6-28-56
LEWIS A. UTZ Form C-122
ENGINEER
Revised 12-1-55

1955 OCT 8 PM 2:22

1 Summit Formation Queens County Lea

tial x Annual _____ Special _____ Date of Test 6-28-56
7-5-56

pany The Texas Company Lease State of N.M. "G" NCT-2 Well No. 9

it B Sec. 19 Twp 20-S Rge. 37-E Purchaser Permian Basin Pipe Line Co.

Casing 5 1/2 Wt. 14.4 I.D. 5.012 Set at 3405 Perf. _____ To _____

Tubing 2 3/8 Wt. 4.70 I.D. 1.995 Set at 3511 Perf. _____ To _____

Gas Pay: From 3405 To 3550 L 3511 xG 0.660 -GL 2317 Bar.Press. _____

Producing Thru: Casing _____ Tubing x Type Well Single

Date of Completion: 1-12-54 Packer 3356 Single-Bradenhead-G. G. or G.O. Dual
Reservoir Temp. _____

CO₂ = 2.08% H₂ = 1.35%

OBSERVED DATA

Tested Through (Prover) (Choke) (Meter) Type Taps Pipe

No.	Flow Data					Tubing Data		Casing Data		Duration of Flow Hr.
	(Known) (Line) Size	(Choke) (Orifice) Size	Press. psig	Diff. h _w	Temp. °F.	Press. psig	Temp. °F.	Press. psig	Temp. °F.	
SI						898.0				71 1/2
1.	4	1.75	457.9	2.7	61	788.0				23 3/4
2.	4	1.75	460.2	6.5	65	641.1				24 1/4
3.	4	1.75	462.0	10.0	70	538.7				24
4.	4	1.75	468.0	11.8	72	477.5				23 3/4
5.										

FLOW CALCULATIONS

No.	Coefficient (24-Hour)	$\sqrt{h_w p_f}$	Pressure psia	Flow Temp. Factor F _t	Gravity Factor F _g	Compress. Factor F _{pv}	Rate of Flow Q-MCFPD @ 15.025 psia
1.	21.69	35.67	471.1	.9990	.9535	1.048	772
2.	21.69	55.47	473.4	.9952	.9535	1.045	1,193
3.	21.69	68.93	475.2	.9905	.9535	1.043	1,473
4.	21.69	75.35	481.2	.9867	.9535	1.043	1,607
5.							

PRESSURE CALCULATIONS

Liquid Hydrocarbon Ratio _____ cf/bbl.
viscosity of Liquid Hydrocarbons _____ deg.
9.936 (1-e^{-s}) 0.147

Specific Gravity Separator Gas _____
Specific Gravity Flowing Fluid _____
P_c 911.2 P_c² 830.3

P _w P _t (psia)	P _t ²	F _c Q	(F _c Q) ²	(F _c Q) ² (1-e ^{-s})	P _w ²	P _c ² -P _w ²	Cal. P _w	P _w P _c
801.2	641.9	7.67	58.83	8.648	650.5	179.8	806.5	.88
654.3	428.1	11.85	140.4	20.64	428.7	381.6	669.9	.72
551.9	304.6	14.64	214.3	31.50	336.1	494.2	579.7	.61
490.7	240.8	15.97	255.0	37.49	278.2	552.1	527.4	.54

solute Potential: 2,270 MCFPD; n .84

MPANY The Texas Company
DRESS Box 1270, Midland, Texas
ENT and TITLE L. I. Baker, District Gas Man
TNESSED H. E. Barrett
MPANY Permian Basin Pipe Line Company

REMARKS

INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

NOMENCLATURE

Q = Actual rate of flow at end of flow period at W. H. working pressure (P_w).
MCF/da. @ 15.025 psia and 60° F.

P_c = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.
psia

P_w = Static wellhead working pressure as determined at the end of flow period.
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia

P_t = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia

P_f = Meter pressure, psia.

h_w = Differential meter pressure, inches water.

F_g = Gravity correction factor.

F_t = Flowing temperature correction factor.

F_{pv} = Supercompressibility factor.

n = Slope of back pressure curve.

Note: If P_w cannot be taken because of manner of completion or condition of well, then P_w must be calculated by adding the pressure drop due to friction within the flow string to P_t .

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