

NEW MEXICO OIL CONSERVATION COMMISSION

ELVIN L. WEST  
GAS ENGINEER

Form C-122

Revised 12-1-55

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Pool Desert Formation Queen County Lea

Initial X Annual \_\_\_\_\_ Special X Date of Test 9-12-56

Company Sinclair Oil & Gas Company Lease W. C. Reach Well No. 1

Unit D Sec. 21 Twp. 20 S Rge. 37 E Purchaser Permian Basin Pipe Line Company

Casing 7" Wt. 24# I.D. 6.336 Set at 3712' Perf. 3380' To 3422'

Tubing 2-3/8" Wt. 4.7# I.D. 1.995 Set at 3769' Perf. 3614' To 3615'

Gas Pay: From 3380' To 3422' L 3380' xG .675 -GL 2282' Bar.Press. 13.2

Producing Thru: Casing X Tubing \_\_\_\_\_ Type Well Gas Oil Dual

Date of Completion: 11-12-54 Packer \_\_\_\_\_ Single-Bradenhead-G. G. or G.O. Dual  
Reservoir Temp. 114

OBSERVED DATA

Tested Through ~~XXXXXXXXXXXX~~ (Meter) Type Taps \_\_\_\_\_ Pipe \_\_\_\_\_

Flow Data						Tubing Data		Casing Data		Duration of Flow Hr.
No.	(Prover) (Line) Size	(Choke) (Orifice) Size	Press. psig	Diff. h <sub>w</sub>	Temp. °F.	Press. psig	Temp. °F.	Press. psig	Temp. °F.	
SI								991.5	70	72-1/4
1.	4	1.750	460.3	6.2	60			818.7	70	23-1/4
2.			465.7	14.3	63			719.0	70	24
3.			470.3	23.0	64			644.7	70	24
4.			459.6	45.1	65			590.9	70	24
5.										

FLOW CALCULATIONS

No.	Coefficient (24-Hour)	$\sqrt{h_{wpf}}$	Pressure psia	Flow Temp. Factor F <sub>t</sub>	Gravity Factor F <sub>g</sub>	Compress. Factor F <sub>pv</sub>	Rate of Flow Q-MCFPD @ 15.025 psia
1.	21.69	54.18	473.5	1.0000	.9427	1.049	1162
2.	21.69	82.75	478.9	.9971	.9427	1.049	1370
3.	21.69	105.4	483.3	.9962	.9427	1.050	2254
4.	21.69	146.0	472.8	.9952	.9427	1.046	3108
5.							

PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio \_\_\_\_\_ cf/bbl.  
Gravity of Liquid Hydrocarbons \_\_\_\_\_ deg.  
P<sub>c</sub> .752 (1-e<sup>-s</sup>) .345

Specific Gravity Separator Gas .675  
Specific Gravity Flowing Fluid \_\_\_\_\_  
P<sub>c</sub> 1004.7 P<sub>c</sub> 1009.4

No.	P <sub>w</sub> P <sub>t</sub> (psia)	P <sub>t</sub> <sup>2</sup>	F <sub>c</sub> Q	(F <sub>c</sub> Q) <sup>2</sup>	(F <sub>c</sub> Q) <sup>2</sup> (1-e <sup>-s</sup> )	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>	Cal. P <sub>w</sub>	P <sub>w</sub> P <sub>c</sub>
1.	831.9	692.1	.8738	.7635	.1107	692.2	317.2	832.0	.83
2.	732.2	536.1	1.332	1.772	.2369	536.4	473.0	732.4	.73
3.	657.9	432.8	1.693	2.873	.4266	433.2	576.2	658.2	.66
4.	604.1	364.9	2.337	5.462	.7920	365.7	643.7	604.7	.60
5.									

Absolute Potential: 4873 MCFPD; n 1.000 Limited

COMPANY Sinclair Oil & Gas Company

ADDRESS 520 East Broadway Street Hobbs, New Mexico

AGENT and TITLE Richard L. Harned Gas Analyst

WITNESSED R. L. West

COMPANY Permian Basin Pipe Line Company

REMARKS

An average curve drawn through the data points would have been in excess of 1.00. Due to this being a retest, an average slope of 1.00 was drawn through the high data point.

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- $Q$  = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.
- $P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia
- $P_w$  = Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- $P_t$  = Flowing wellhead pressure (tubing if flowing through tubing, casing if  
flowing through casing.) psia
- $P_f$  = Meter pressure, psia.
- $h_w$  = Differential meter pressure, inches water.
- $F_g$  = Gravity correction factor.
- $F_t$  = Flowing temperature correction factor.
- $F_{pv}$  = Supercompressability factor.
- $n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .