

## NEW MEXICO OIL CONSERVATION COMMISSION

HOBBS OFFICE OCC

Form C-12

## MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Revised 12-1-55

1957 FEB 11 AM 9:48

Pool Tubbs Formation Tubbs County Lee  
 Initial X Annual \_\_\_\_\_ Special \_\_\_\_\_ Date of Test 12-13-56  
 Company Sinclair Oil & Gas Company Lease J.R. Come "A" Well No. 1  
 Unit X Sec. 26 Twp. 21S Rge. 37E Purchaser None  
 Casing 5 1/2 Wt. 174 I.D. 4.892 Set at 6554 Perf. 6066 To 6191  
 Tubing 2 3/8 Wt. 4.7 I.D. 1.995 Set at 6514 Perf. 6480 To 6540  
 Gas Pay: From 6066 To 6191 L 6060 xG .719 -GL 4357 Bar.Press. 13.2  
 Producing Thru: Casing X / Tubing \_\_\_\_\_ Type Well G.O. Dual  
 Date of Completion: 12-1-56 Packer 6400 Single-Bradenhead-G. G. or G.O. Dual  
 Reservoir Temp. 120

## OBSERVED DATA

Tested Through (Prover) (Orifice) (Water)Type Taps 2" G.F.P.

No.	Flow Data					Tubing Data		Casing Data		Duration of Flow Hr.
	(Prover) ( <u>Orifice</u> ) Size	(Orifice) Size	Press. psig	Diff. h <sub>w</sub>	Temp. °F.	Press. psig	Temp. °F.	Press. psig	Temp. °F.	
1.	<u>2"</u>	<u>3/16</u>	<u>624</u>		<u>30</u>			<u>1493</u>	<u>60</u>	<u>72</u>
2.		<u>1/4</u>	<u>654</u>		<u>14</u>			<u>1792</u>	<u>60</u>	<u>3</u>
3.		<u>5/16</u>	<u>780</u>		<u>23</u>			<u>1693</u>	<u>60</u>	<u>3</u>
4.		<u>7/16</u>	<u>780</u>		<u>23</u>			<u>1599</u>	<u>60</u>	<u>3</u>
5.		<u>1/2</u>	<u>730</u>		<u>42</u>			<u>1115</u>	<u>60</u>	<u>3</u>
								<u>741</u>	<u>60</u>	<u>20</u>

No.	FLOW CALCULATIONS							Rate of Flow Q-MCFPD @ 15.025 psia
	Coefficient (24-Hour)	$\sqrt{h_w P_f}$	Pressure psia	Flow Temp. Factor F <sub>t</sub>	Gravity Factor F <sub>g</sub>	Compress. Factor F <sub>pv</sub>		
1.	<u>.7851</u>		<u>637.2</u>	<u>1.0302</u>	<u>.9427</u>	<u>1.032</u>		<u>430</u>
2.	<u>1.4030</u>		<u>647.2</u>	<u>1.0452</u>	<u>.9427</u>	<u>1.112</u>		<u>1025</u>
3.	<u>2.1577</u>		<u>713.2</u>	<u>1.0574</u>	<u>.9427</u>	<u>1.114</u>		<u>1476</u>
4.	<u>4.3297</u>		<u>713.2</u>	<u>1.0574</u>	<u>.9427</u>	<u>1.114</u>		<u>1476</u>
5.	<u>5.5233</u>		<u>733.2</u>	<u>1.0170</u>	<u>.9427</u>	<u>1.114</u>		<u>1289</u>

## PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio 29.569 cf/bbl.  
 Gravity of Liquid Hydrocarbons 65 deg.  
 F<sub>c</sub> 1.012 (1-e<sup>-s</sup>) .279

Specific Gravity Separator Gas .677  
 Specific Gravity Flowing Fluid .719  
 P<sub>c</sub> 1906.2 P<sub>c</sub> 3633.6

No.	P <sub>w</sub> P <sub>t</sub> (psia)	P <sub>t</sub> <sup>2</sup>	F <sub>c</sub> Q	(F <sub>c</sub> Q) <sup>2</sup>	(F <sub>c</sub> Q) <sup>2</sup> (1-e <sup>-s</sup> )	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>	Cal. P <sub>w</sub>	P <sub>w</sub> P <sub>c</sub>
1.	<u>1805.2</u>	<u>3259</u>	<u>.960</u>	<u>.922</u>	<u>.237</u>	<u>3259.2</u>	<u>374.4</u>	<u>1805.2</u>	<u>94.7</u>
2.	<u>1706.2</u>	<u>2911</u>	<u>1.897</u>	<u>3.448</u>	<u>.893</u>	<u>2911.2</u>	<u>721.8</u>	<u>1706.2</u>	<u>89.5</u>
3.	<u>1612.2</u>	<u>2599</u>	<u>3.057</u>	<u>9.223</u>	<u>2.389</u>	<u>2599.2</u>	<u>1032.2</u>	<u>1612.2</u>	<u>84.6</u>
4.	<u>1120.2</u>	<u>1253</u>	<u>6.192</u>	<u>38.341</u>	<u>9.930</u>	<u>1582.9</u>	<u>2350.7</u>	<u>1132.4</u>	<u>59.4</u>
5.	<u>754.2</u>	<u>569</u>	<u>7.772</u>	<u>60.404</u>	<u>13.645</u>	<u>584.6</u>	<u>3048.8</u>	<u>744.7</u>	<u>40.1</u>

Absolute Potential: 5.112 MCFPD; n 1.000  
 COMPANY Sinclair Oil & Gas Company  
 ADDRESS 520 Bank Broadway, Hobbs, New Mexico  
 AGENT and TITLE R. L. Harwood - Gas Analyst  
 WITNESSED \_\_\_\_\_  
 COMPANY \_\_\_\_\_

## REMARKS

Orig. &amp; 2cc:OCC

cc:FCR, WJR, CCS, PHD, KPW, PBPL, F11c(3)

FILED  
 (402) 62001-1

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

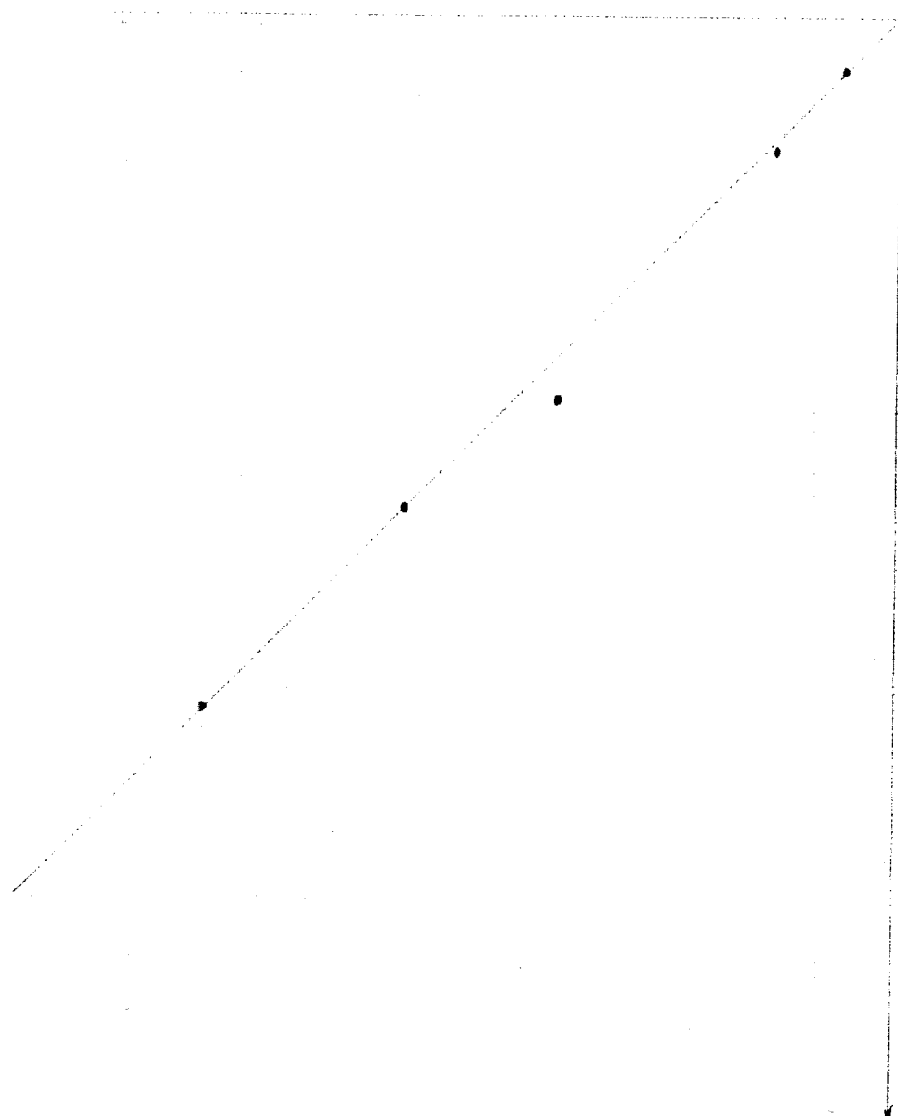
The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

- $Q$  = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.
- $P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia
- $P_w$  = Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia
- $P_t$  = Flowing wellhead pressure (tubing if flowing through tubing, casing if  
flowing through casing.) psia
- $P_f$  = Meter pressure, psia.
- $h_w$  = Differential meter pressure, inches water.
- $F_g$  = Gravity correction factor.
- $F_t$  = Flowing temperature correction factor.
- $F_{pv}$  = Supercompressibility factor.
- $n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .

$P_1^2 \cdot P_2^2$



HP-5, 112 MCFPD

$Q = 1,000$