

## NEW MEXICO OIL CONSERVATION COMMISSION

ELVIS A. UIZ  
GAS ENGINEER 54

HOBBS OFFICE OCC

Form C-122

MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Revised 12-1-55

1956 OCT 8 PM 2:21

Pool Eumont Formation Queens County LeaInitial x Annual \_\_\_\_\_ Special \_\_\_\_\_ Date of Test 7-16-56  
7-23-56Company The Texas Company Lease V. M. Henderson Well No. 4Unit 6 Sec. 30 Twp. 21-S Rge. 37-E Purchaser Permian Basin Pipe Line Co.Casing 5 1/2 Wt. 14.04 I.D. 5.012 Set at 3480 Perf. \_\_\_\_\_ To \_\_\_\_\_Tubing 2 3/8 Wt. 4.74 I.D. 1.995 Set at 3662 Perf. 3658 To 3662Gas Pay: From 3476 To 3675 L 3658 xG .695 -GL 234.1 Bar.Press. 13.2Producing Thru: Casing \_\_\_\_\_ Tubing x Type Well SingleDate of Completion: 8-22-55 Packer \_\_\_\_\_ Single-Bradenhead-G. G. or G.O. Dual  
Reservoir Temp. \_\_\_\_\_ $CO_2 = 4.31\%$   $H_2 = 0.50\%$ 

## OBSERVED DATA

Tested Through (Prevor) (Choke) (Meter) Type Taps Pipe

No.	Flow Data			Tubing Data		Casing Data		Duration of Flow Hr.
	(Prevor) (Line) Size	(Choke) (Orifice) Size	Press. psig	Diff. $h_w$	Temp. $^{\circ}F$	Press. psig	Temp. $^{\circ}F$	
SI								
1.	4	1.50	462.7	7.3	75	692.9		71 3/4
2.	4	1.50	462.0	13.2	75	683.5		24 1/4
3.	4	1.50	460.0	19.3	79	577.7		24
4.	4	1.50	460.0	19.3	79	529.0		24
5.	4	1.50	469.9	21.4	78	491.1		24

## FLOW CALCULATIONS

No.	Coefficient (24-Hour)	$\sqrt{h_w p_f}$	Pressure psia	Flow Temp. Factor $F_t$	Gravity Factor $F_g$	Compress. Factor $F_{pv}$	Rate of Flow Q-MCFPD @ 15.025 psia
1.	15.26	54.94	475.9	.9859	.9292	1.045	661
2.	15.26	79.20	475.2	.9859	.9292	1.045	1,157
3.	15.26	95.57	473.2	.9822	.9292	1.045	1,391
4.	15.26	101.7	483.1	.9831	.9292	1.045	1,481
5.							

## PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio \_\_\_\_\_ cf/bbl.  
Gravity of Liquid Hydrocarbons \_\_\_\_\_ deg.  
 $F_c$  9.936  $(1-e^{-S})$  0.160Specific Gravity Separator Gas \_\_\_\_\_  
Specific Gravity Flowing Fluid \_\_\_\_\_  
 $P_c$  706.1  $P_c^2$  498.6

No.	$P_w$ $P_t$ (psia)	$P_t^2$	$F_c Q$	$(F_c Q)^2$	$(F_c Q)^2$ $(1-e^{-S})$	$P_w^2$	$F_c^2 - P_w^2$	Cal. $P_w$	$P_w$ $P_c$
1.	636.7	405.4	8.545	73.19	11.71	417.1	41.5	615.8	.99
2.	590.9	349.0	11.58	134.3	21.17	349.4	128.8	608.4	.81
3.	543.2	295.0	13.81	190.8	30.44	294.6	174.0	589.7	.77
4.	506.3	256.3	14.72	216.7	34.07	256.0	207.0	539.4	.72
5.									

Absolute Potential: 2,700 MCFPD; n .63COMPANY The Texas Company  
ADDRESS Box 1270, Midland, Texas  
AGENT and TITLE L. I. Baker, District Gas Man  
WITNESSED N. E. Barreca  
COMPANY Permian Basin Pipe Line Company

REMARKS

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

$Q$  = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.

$P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia

$P_w$  = Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia

$P_t$  = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia

$P_f$  = Meter pressure, psia.

$h_w$  = Differential meter pressure, inches water.

$F_g$  = Gravity correction factor.

$F_t$  = Flowing temperature correction factor.

$F_{pv}$  = Supercompressibility factor.

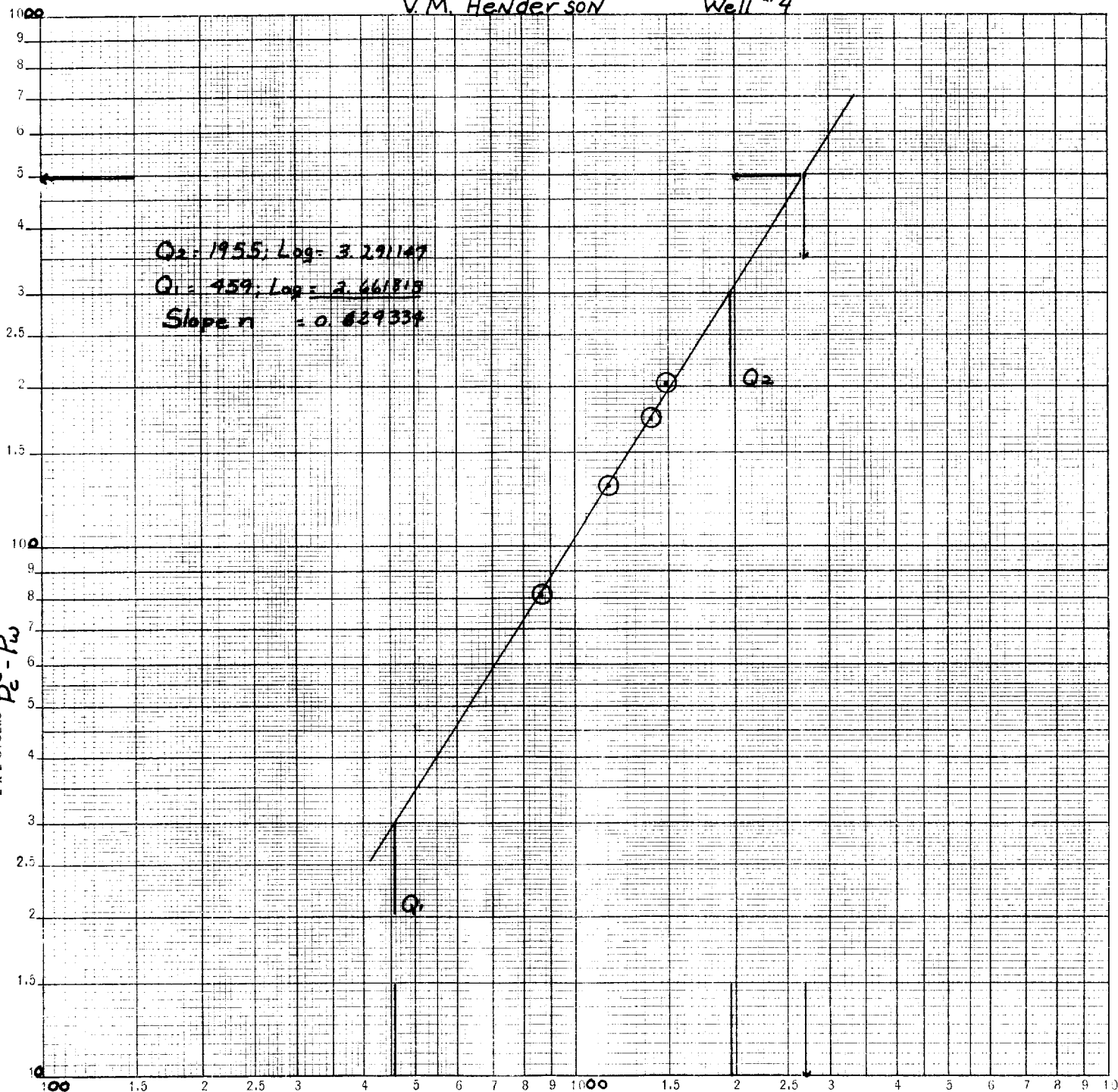
$n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .

The Texas Co  
V.M. Henderson

Well #4

LOGARITHMIC 359-110  
KEUFFEL & ESSER CO. MADE IN U.S.A.  
2 X 2 CYCLES  
 $P_e - P_w$

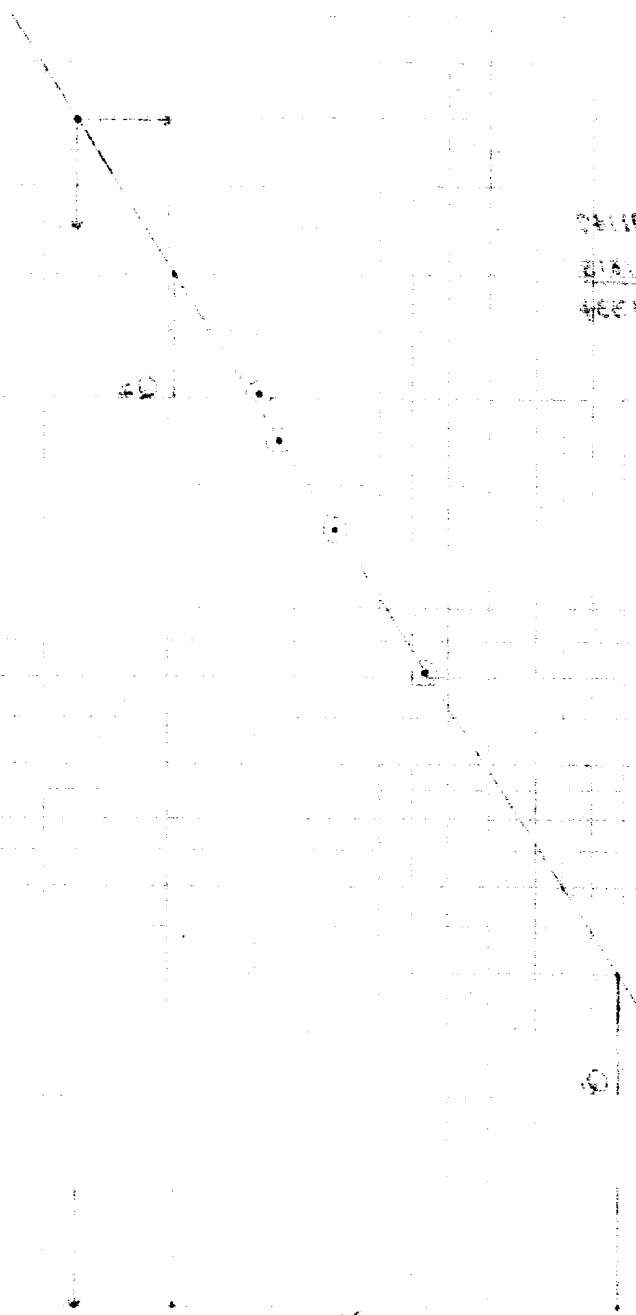


$Q = \text{MCF/Day}$

$Q = 2,700$

Y<sup>2</sup> new

W22002W25 N.1



34101 2 - geo (221) - 20

31812 1 - geo (227) - 10

460938 2 - geo (228)

221 (227) - 10

227 (228)