

W MEXICO OIL CONSERVATION COMPANY
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
 Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 2-3-89	
Company EXXON CORPORATION				Connection AIR		
Pool PADDOCK				Formation GLORITIA PADDOCK		Unit
Completion Date 1-13-89		Total Depth 5180		Plug Back To 5180		Elevation PADDOCK (SAN ANGELO)
Csg. Size 7.0	Wt. 23.0	Gr. 6.366	Set At 5065	Performances: From 5026 To 5061		Well No. 2
Tub. Size 2.375	Wt. 4.7	Gr. 1.995	Set At 4955	Performances: From To		Unit Sec. Twp. Rge. P 34 21S 37E
Type Well - Single - Bradenhead - G.G. or G.O. Multiple SINGLE-GAS				Packer Set At 4955		County LEA
Producing Thru TUBING		Reservoir Temp. °F 109 @ 5043		Mean Annual Temp. °F 60		Baro. Press. - P _a 13.2
L 5043		H 5043		Gg 0.705	% CO ₂ 1.24	% N ₂ 3.63
				% H ₂ S 0.04	Prover	Meter Run 4.026
						FLANGE

FLOW DATA						TUBING DATA		CASING DATA		Direction of Flow	
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
51							1514	58			72
1.	4.026 X	1.250		570	7	60	1440	58			1
2.	4.026 X	1.250		580	15	60	1379	58			1
3.	4.026 X	1.250		600	24.5	60	1322	58			1
4.	4.026 X	1.250		600	57	62	1189	58			1
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compens. Factor, Fpv	Rate of Flow Q, Mhd
1	7.47	63.89	583.2	1.000	1.1910	1.0660	606
2	7.47	94.33	593.2	1.000	1.1910	1.0672	896
3	7.47	122.57	613.2	1.000	1.1910	1.0697	1166
4	7.47	186.96	613.2	.9981	1.1910	1.0686	1774
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	A.P.I. Gravity of Liquid Hydrocarbons	Specific Gravity Separator Gas	Specific Gravity Flowing Fluid	Critical Pressure	Critical Temperature
1	.87	520	1.37	.880	29.2	47.5	.705	.799	667	379
2	.89	520	1.37	.878						
3	.92	520	1.37	.874						
4	.92	522	1.38	.876						
5.										

NO.	P _r	P _w	P _r ²	P _w ²	P _r ² - P _w ²
1	2112	1457	2123	218	
2	1938	1398	1953	388	
3	1783	1343	1803	538	
4	1445	1221	1490	851	
5					

(1) $\frac{P_r^2}{P_r^2 - P_w^2} = 2.7509$

ADP = Q $\left[\frac{P_r^2}{P_r^2 - P_w^2} \right]^n = 4344$

(2) $\left[\frac{P_r^2}{P_r^2 - P_w^2} \right]^n = 2.4487$

Absolute Open Flow	4344	Mhd @ 15.025	Angle of Slope @	48.5	Slope, n	885
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Remarks: CHOKES RATE1 5/64 RATE2 7/64 RATE3 9/64 RATE4 13/64

MAR 7 1989

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
	STEVE RIPLEY	MATT LEE	