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appropriate district office
See Rule 401 & Rule 1122

State of New Mexico
En , Minerals and Natural Resources Department.

Form C-122
Revised 4-1-91

OIL CONSERVATION DIVISION

P.O. Box 2088
Santa Fe, New Mexico 87504-2088

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Operator EXXON USA					Lease or Unit Name F. F. HARDISON B				
Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 8-14-95		Well No. 3		
Completion Date 7-13-95		Total Depth 6607		Plug Back TD 6780		Elevation		Unit Lr. - Sec. - TWP - Rge. G-34-27-37	
Csg. Size 5 1/2	Wt. 15.5	d	Set At 6607	Perforations: From: 5988 To: 6154			Country LEA		
Tbg. Size 2-3/8	Wt. 4.7	d 1.995	Set At 5934	Perforations: From: To:			Pool Tubb Oil & Gas		
Type Well - Single - Bradenhead - G.G. or I.O. Multiple single				Packer Set At 5934			Formation TUBB		
Producing Thru TBG		Reservoir Temp. °F 60		Mean Annual Temp. °F 60		Baro. Press - P _a 13.2		Connection SALES	
L 5934	II 5934	Gg. .697	% CO ₂ .10	% N ₂ 2.26	% H ₂ S	Prover	Meter Run 4.026	Taps FLG	

FLOW DATA					TUBING DATA		CASING DATA		Duration of Flow	
NO.	Prover Line Size	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.		Temp. °F
SI						368		PKR		24 hr.
1.	4 X .625		59	10.20	66	366		"		45 min
2.	4 X .625		59	23.00	66	362		"		45 min
3.	4 X .625		60	64.00	67	356		"		45 min
4.	4 X .625		60	96.00	67	345		"		45 min
5.										

RATE OF FLOW CALCULATIONS							
NO.	COEFFICIENT (24 HOUR)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg.	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1.	1.845	27.14	72.2	.9943	1.198	1.009	60
2.	1.845	40.75	72.2	.9943	1.198	1.009	90
3.	1.845	68.45	73.2	.9933	1.198	1.009	152
4.	1.845	83.83	73.2	.9933	1.198	1.009	186
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	DRY GAS	Mcf/bbl
1.	.10	526	1.37	.982	A.P. L Gravity of Liquid Hydrocarbons	DRY	Deg.
2.	.10	526	1.37	.982	Specific Gravity Separator Gas	.697	XXXXXXXXXX
3.	.10	527	1.37	.982	Specific Gravity Flowing Fluid	XXXXXX	
4.	.10	527	1.37	.982	Critical Pressure	*666	P.S.I.A. P.S.I.A.
5.					Critical Temperature	*382	R R

P_c **381.2** P_c² **145.3**

NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²
1.		379.3	143.9	1.4
2.		375.4	141.0	4.4
3.		369.9	136.8	8.5
4.		359.3	129.1	16.2
5.				

1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{101.027}{101.027 - 16.2} = 10.051$

2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 10.051$

AOF = Q $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = .603$

Absolute Open Flow 603 Mcfd @ 15.025	Angle of Slope Θ 63.5	Slope, n .500
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Remarks: ***=CORRECTED TO 2.26% N₂**

Approved By Division	Conducted By: PRO WELL TESTERS	Calculated By: BM	Checked By: BM
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