

N MEXICO OIL CONSERVATION COMM DN
MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 4/15/76							
Company Continental Oil Company			Connection El Paso Natural Gas Company								
Pool Eumont			Formation Eumont Queen		Unit D						
Completion Date		Total Depth	Plug Back To	Deviation							
				State J-2							
Csg. Size 5 1/2	Wt. 17	d	Set At 3680	Perforations: From 3018 To 3649	Well No. 12						
Tbg. Size 2 3/8	Wt. 4.7	d	Set At 2963	Perforations: From Open End To	Unit Sec. Twp. Pgs. D 2 22 36						
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 2963	County Lee						
Producing Thru Tbg.		Reservoir Temp. °F a	Mean Annual Temp. °F	Baro. Press. - P _a	State New Mexico						
L	H	Gg	% CO ₂	% N ₂	% H ₂ S						
		661									
FLOW DATA			TUBING DATA		CASING DATA						
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	Duration of Flow
SI							528			72 hr.	S.I.E.
1.	4	x	2.00	68	6.3	60	500				30 Min.
2.	4	x	2.00	70	16.8	56	430				30 Min.
3.	4	x	2.00	78	36.0	58	380				60 Min.
4.	4	x	2.00	85	62.4	52	380				45 Min.
5.											
RATE OF FLOW CALCULATIONS											
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor F _{pv}	Rate of Flow Q, Mscf				
1	19.81	22.62	81.2	1.000	1.230	Nil	551				
2	19.81	37.39	83.2	1.004	1.230	Nil	915				
3	19.81	57.24	91.0	1.002	1.230	Nil	1328				
4	19.81	78.28	98.2	1.008	1.230	Nil	1923				
5											
NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio _____ Mscf bbl.						
					A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.						
1.	.12	520	1.38	Nil	Specific Gravity Separator Gas .661 X X X X X X X X X						
2.	.12	516	1.37	Nil	Specific Gravity Flowing Fluid X X X X X						
3.	.14	518	1.37	Nil	Critical Pressure 670 P.S.I.A. _____ P.S.I.A.						
4.	.15	512	1.35	Nil	Critical Temperature 378 R _____ R						
5.											
P _c 541.2 P _c ² 292,000					(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 3.064$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.855$						
NO.	P _t ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 3.064$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 2.855$ ACF = $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 5.490$						
1		516.5	266.8	26.1							
2		502.8	252.8	40.1							
3		467.9	218.9	74.0							
4		444.2	197.3	95.6							
5											
Absolute Open Flow 5,400					Mscf @ 15.025		Angle of Slope 46.75		Slope, n 236		
Remarks:											
Approved By Commission:			Conducted By: Richard T. Pagan			Calculated By: Reginald E. Reston			Checked By:		

NO. 1000(2)
FILE