

## NEW MEXICO OIL CONSERVATION COMMISSION

Form C-122

## MULTI-POINT BACK PRESSURE TEST FOR GAS WELLS

Revised 12-1-55

Pool Jalmat Formation Yates County Lea  
Initial \_\_\_\_\_ Annual \_\_\_\_\_ Special X Date of Test 3/3-3/11/60  
Company Dalport Oil Corporation Lease Lunt B Well No. 1  
Unit P Sec. 20 Twp. 22S Rge. 36E Purchaser El Paso Natural Gas Company  
Casing 5 Wt. 11.4 I.D. \_\_\_\_\_ Set at 3400 Perf. \_\_\_\_\_ To \_\_\_\_\_  
Tubing 2 Wt. 4.7 I.D. \_\_\_\_\_ Set at 3160 Perf. \_\_\_\_\_ To \_\_\_\_\_  
Gas Pay: From 3164 To 3363 L 3160 xG .674 -GL 2130 Bar.Press. 13.2  
Producing Thru: Casing \_\_\_\_\_ Tubing X Type Well Single  
Single-Bradenhead-G. G. or G.O. Dual  
Date of Completion: 3-4-59 Packer None Reservoir Temp. \_\_\_\_\_

## OBSERVED DATA

Tested Through (Prover) (Choke) (Meter) \_\_\_\_\_ Type Taps Flange

No.	Flow Data					Tubing Data		Casing Data		Duration of Flow Hr.
	(Prover) (Line) Size	(Choke) (Orifice) Size	Press. psig	Diff. h <sub>w</sub>	Temp. °F.	Press. psig	Temp. °F.	Press. psig	Temp. °F.	
SI						660				72
1.	4	1.000	218	9.00	70	327				24
2.	4	1.000	186	16.00	71	307				24
3.	4	1.000	218	14.44	74	325				24
4.	4	1.000	220	16.00	68	330				24
5.										

## FLOW CALCULATIONS

No.	Coefficient (Flange) (24-Hour)	$\sqrt{h_{wPF}}$	Pressure psia	Flow Temp. Factor F <sub>t</sub>	Gravity Factor F <sub>g</sub>	Compress. Factor F <sub>pv</sub>	Rate of Flow Q-MCFPD @ 15.025 psia
1.	6.135	45.62	231.2	.9905	.9435	1.022	267.2
2.	6.135	56.45	199.2	.9896	.9435	1.019	329.4
3.	6.135	57.77	231.2	.9868	.9435	1.022	337.1
4.	6.135	61.08	233.2	.9924	.9435	1.023	358.9
5.							

## PRESSURE CALCULATIONS

Gas Liquid Hydrocarbon Ratio \_\_\_\_\_ cf/bbl.  
Gravity of Liquid Hydrocarbons \_\_\_\_\_ deg.  
F<sub>c</sub> 9.936 (1-e<sup>-s</sup>) 0.136  
Specific Gravity Separator Gas .674  
Specific Gravity Flowing Fluid \_\_\_\_\_  
P<sub>c</sub> 673.2 P<sub>c</sub> 453.2

No.	P <sub>max</sub> P <sub>t</sub> (psia)	P <sub>t</sub> <sup>2</sup>	F <sub>c</sub> Q	(F <sub>c</sub> Q) <sup>2</sup>	(F <sub>c</sub> Q) <sup>2</sup> (1-e <sup>-s</sup> )	P <sub>w</sub> <sup>2</sup>	P <sub>c</sub> <sup>2</sup> -P <sub>w</sub> <sup>2</sup>	Cal. P <sub>w</sub>	P <sub>w</sub> / P <sub>c</sub>
1.	340.2	115.7	2.655	7.05	0.96	116.7	336.5	341.6	.5074
2.	320.2	102.5	3.273	10.71	1.46	104.0	349.2	322.5	.4790
3.	338.2	114.4	3.349	11.21	1.52	115.9	337.3	340.4	.5056
4.	343.2	117.8	3.566	12.72	1.73	119.5	333.7	345.7	.5135
5.									

Absolute Potential: 465 MCFPD; n 777  
COMPANY DALPORT OIL CORPORATION  
ADDRESS 930 Fidelity Union Life Bldg., Dallas, Texas  
AGENT and TITLE President  
WITNESSED J. B. Murray  
COMPANY El Paso Natural Gas Company, Jal., New Mexico

## REMARKS

\*This well produced an undertermined amount of water during this test. Poor point alignment on back pressure curve. Therefore the average Jalmat slope of .777 was drawn through the data point corresponding to the highest rate of flow.

## INSTRUCTIONS

This form is to be used for reporting multi-point back pressure tests on gas wells in the State, except those on which special orders are applicable. Three copies of this form and the back pressure curve shall be filed with the Commission at Box 871, Santa Fe.

The log log paper used for plotting the back pressure curve shall be of at least three inch cycles.

## NOMENCLATURE

$Q$  = Actual rate of flow at end of flow period at W. H. working pressure ( $P_w$ ).  
MCF/da. @ 15.025 psia and 60° F.

$P_c$  = 72 hour wellhead shut-in casing (or tubing) pressure whichever is greater.  
psia

$P_w$  = Static wellhead working pressure as determined at the end of flow period.  
(Casing if flowing thru tubing, tubing if flowing thru casing.) psia

$P_t$  = Flowing wellhead pressure (tubing if flowing through tubing, casing if flowing through casing.) psia

$P_f$  = Meter pressure, psia.

$h_w$  = Differential meter pressure, inches water.

$F_g$  = Gravity correction factor.

$F_t$  = Flowing temperature correction factor.

$F_{pv}$  = Supercompressability factor.

$n$  = Slope of back pressure curve.

Note: If  $P_w$  cannot be taken because of manner of completion or condition of well, then  $P_w$  must be calculated by adding the pressure drop due to friction within the flow string to  $P_t$ .