

NEW MEXICO OIL CONSERVATION COMMISSION
MULTIPOINT AND ONE POINT BACK PRESSURE TEST OF GAS WELL

Form C-122
Revised 9-1-65

Type Test ☒ Initial ☐ Annual ☐ Special				Test Date 8-12-75	
Company Gulf Oil Co. - U. S.				Connection	
Pool				Formation	
Completion Date		Total Depth		Plug Back TD	
				Elevation	
Farm or Lease Name Covington - A - Federal					
Csg. Size	Wt.	d	Set At	Perforations: From 14,305 To 14,613	
Tbg. Size 2 7/8	Wt. 6.5	d	Set At	Perforations: From To	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple				Packer Set At	
Producing Thru Tbg.				Reservoir Temp. °F 208 @ 14,275	
Mean Annual Temp. °F				Baro. Press. - P _a	
L	H	Gg .591	% CO ₂	% N ₂	% H ₂ S
Prover				Meter Run X	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
1.	4	X	3/4	913.2	25	117	913.2	94			60 min.
2.	4	X	1 1/4	913.2	11	106	913.2	88			60 min.
3.	4	X	1 1/4	913.2	17	103	913.2	86			60 min.
4.	4	X	1 1/4	913.2	22	101	913.2	86			60 min.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mscf/d
1.	2.661	151	913.2	.9493	1.301	1.055	478
2.	7.469	100	913.2	.9585	1.301	1.055	897
3.	7.469	125	913.2	.9610	1.301	1.055	1125
4.	7.469	142	913.2	.9628	1.301	1.055	1280
5.							

NO.	P _t	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	1.35	577	1.64	.898	A.P.I. Gravity of Liquid Hydrocarbons	
2.	1.35	566	1.61	.898	Specific Gravity Separator Gas .591	XXXXXX
3.	1.35	563	1.60	.898	Specific Gravity Flowing Fluid 672	XXXXXX
4.	1.35	561	1.60	.898	Critical Pressure 350	P.S.I.A.
5.					Critical Temperature	R

NO.	P _t ²	P _w	P _w ²	P _t ² - P _w ²	(1) $\frac{P_t^2}{P_t^2 - P_w^2} =$	(2) $\left[\frac{P_t^2}{P_t^2 - P_w^2} \right]^n =$
1.		6394.2	40886	5820	$\frac{P_t^2}{P_t^2 - P_w^2} = 1.959$	$\left[\frac{P_t^2}{P_t^2 - P_w^2} \right]^n = 1.517$
2.		5602.2	31385	15321		
3.		4782.2	22869	23837		
4.		3886.2	15103	31603		
5.						

AOF = Q $\left[\frac{P_t^2}{P_t^2 - P_w^2} \right]^n = 1.706$

Absolute Open Flow **1733** Mcfd @ 15.025 Angle of Slope **58°** Slope, n **.620**

Remarks: **Open flow calculated from BHP data using Amerada RPG-3, Ser. # 34923 gauge**

Approved By Commission: <i>John W. Ramsey</i>	Conducted By:	Calculated By: <i>David Cameron</i>	Checked By:
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