NEW MEXICO OIL CONSERVATION COMMSSION

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Form C-122
Revised 9-1-65

Type Test: [X] Initial [ ] Annual [ ] Special		Test Date: 1-[illegible]-76	
Company: [illegible]	Connection: None		
Pool: [illegible] Tubb	Formation: Tubb		Unit
Completion Date: 2-6-76	Total Depth: 7000'	Plug Back TD: 6947' / Elevation: 3531 GL	Farm or Lease Name: WARREN Unit
Csg. Size: [illegible]" / Wt. 23 & 26 / d / Set At 7000'	Perforations: From 6341 To 6580		Well No. #35
Tbg. Size: 2 1/2 / Wt. 6.50 / d / Set At 6256	Perforations: From To		Unit K / Sec. 28 / Twp. 20S / Rge. 38E
Type Well – Single – Bradenhead – G.G. or G.O. Multiple: Single	Packer Set At: 6256		County: Lea
Producing Thru: Tubing / Reservoir Temp. °F @ / Mean Annual Temp. °F	Baro. Press. – P_a		State: New Mexico
L / H / Gg / % CO_2 / % N_2	% H_2S / Prover		Meter Run: X / Taps

FLOW DATA / TUBING DATA / CASING DATA

NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h_w	Temp. °F	Tubing Press. p.s.i.g.	Tubing Temp. °F	Casing Press. p.s.i.g.	Casing Temp. °F	Duration of Flow
SI							1371		[illegible]		72 hrs
1.	4"		1.750	302	20.0	65°					3 hrs
2.	4"		1.750	310	32.3	80°					2.45 hrs
3.	4"		1.750	314	50.8	50°					2.[illegible] hrs
4.	4"		1.750	322	79.1	72°					3 hrs
5.											

RATE OF FLOW CALCULATIONS

NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P_m	Flow Temp. Factor Ft.	Gravity Factor Fg	Super Compress. Factor, Fpv	Rate of Flow Q, Mcfd
1	14.93	79.378	315.2	.9952	1.213	1.028	1432
2.	14.93	102.315	323.2	.9795	1.213	1.032	1869
3.	14.93	12[illegible].875	327.2	.9[illegible]	1.213	1.033	2366
4.	14.93	162.872	335.2	.9887	1.213	1.034	3015
5.							

NO.	P_r	Temp. °R	T_r	Z
1.	Calculated by			
2.	Computer			
3.				
4.				
5.				

Gas Liquid Hydrocarbon Ratio ______ Mcf/bbl.
A.P.I. Gravity of Liquid Hydrocarbons 1.4.6 Deg.
Specific Gravity Separator Gas .680 XXXXXXXXX
Specific Gravity Flowing Fluid XXXXX
Critical Pressure ______ P.S.I.A. ______ P.S.I.A.
Critical Temperature ______ R ______ R

P_c 1828.1 P_c^2 3341.9 M

NO	P_t^2	P_w	P_w^2 M	$P_c^2 - P_w^2$ M
1		1692.5	2854.4	487.5
2		1616.2	2612.1	729.5
3		1511.7	2285.5	1056.4
4		1388.0	1926.5	1415.4
5				

(1) $\frac{P_c^2}{P_c^2 - P_w^2} = \frac{3341.9}{3341.9 - 2285.5}$ (2) $\left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n$ = 2.0186

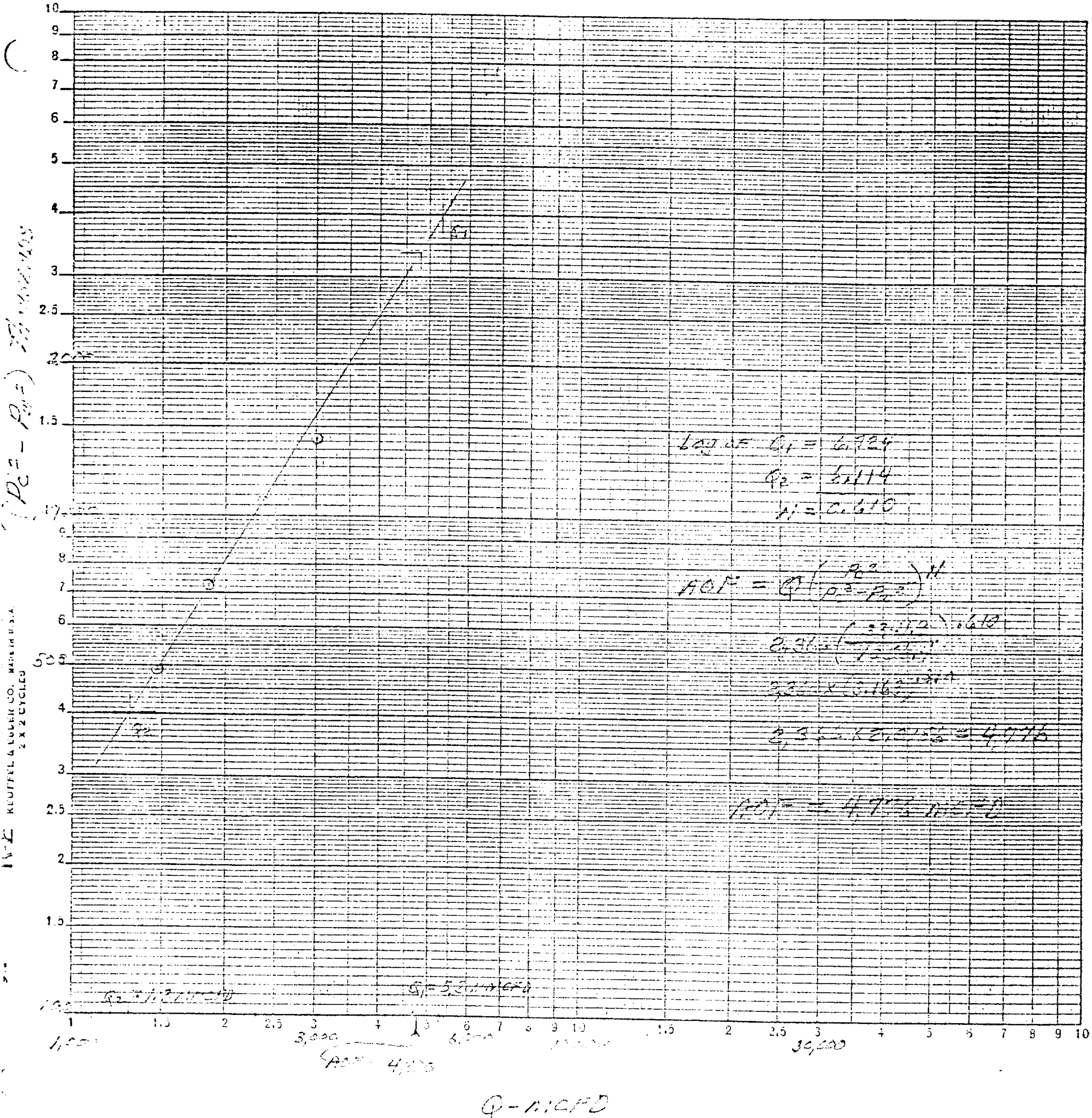
$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2}\right]^n$ = 4776

Absolute Open Flow 4,776 Mcfd @ 15.025 Angle of Slope Θ ______ Slope, n 0.610

Remarks: ______

Approved By Commission:	Conducted By:	Calculated By:	Checked By:
[signature]	W.E. [illegible]	[illegible]	

[illegible] (3) File


KEUFFEL & ESSER CO. MADE IN U.S.A.
2 X 2 CYCLES
Q1
Q2
Log of Q1 = 6.724
Q2 = 6.114
n = 0.610
3,000
6,000
30,000
Q - MCFD