

NCV 15.1

Corrected Copy

Type Test ☒ Initial ☐ Annual ☐ Special		Test Date 11-3-77	
Company Texas Pacific Oil Company, Inc.		Connection To Air	
Pool Jalmat Gas		Formation Jalmat Gas	
Completion Date 9-12-77		Total Depth 3700	Plug Back TD 3630
Elevation 3341 GL		Farm or Lease Name State "A" A/C - 2	
Csg. Size 5 1/2"	Wt. 14.0	d 5.012	Set At 3700
Perforations: From 3034 To 3577		Well No. 62	
Tbg. Size 2 3/8	Wt. 4.7	d 1.995	Set At 3689
Perforations: From To		Unit K	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple G.O. Dual		Packer Set At 3426	County Lea
Producing Thru Annulus	Reservoir Temp. °F 85 @ 3306	Mean Annual Temp. °F 60	Baro. Press. - P _a 13.2
State New Mexico			
L 3306	H 3306	G _g est. 0.675	% CO ₂ ---
% N ₂ ---		% H ₂ S ---	Prover 4"
Meter Run ---		Taps ---	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI	4" Prover						Packer	choke	414.0	
1.	1.250"			10.0	--	60		14/64"	412.0	
2.	1.250"			24.5	--	58		19/64"	407.0	60 min.
3.	1.250"			47.5	--	59		32/64"	398.0	60 min.
4.	2.000"			22.5	--	59		36/64"	389.0	60 min.
5.	2.000"			48.0	--	54		48/64"	354.0	60 min.

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	* Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	25.91	--	23.2	1.0000	1.217	1.000	732
2	25.91	--	37.7	1.0020	1.217	1.000	1191
3	25.91	--	60.7	1.0010	1.217	1.000	1916
4	67.08	--	35.7	1.0010	1.217	1.000	2917
5	67.08	--	61.0	1.0060	1.217	1.000	5010

NO.	P _t	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio <u>none</u>	Mcf/bbl.
1.	0.03	520	1.36		A.P.I. Gravity of Liquid Hydrocarbons	Deg.
2.	0.06	518	1.36		Specific Gravity Separator Gas <u>0.675</u>	X X X X X X X X
3.	0.09	519	1.36		Specific Gravity Flowing Fluid <u>X X X X X</u>	
4.	0.05	519	1.36		Critical Pressure <u>669</u>	P.S.I.A.
5.	0.09	514	1.35		Critical Temperature <u>382</u>	R

P _c <u>427.2</u>	P _c ² <u>182.5</u>	(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 4.753$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 3.130$
NO.	P _t ²	P _w	P _w ²
1			181.0
2			177.1
3			170.5
4			165.0
5			144.1

Absolute Open Flow <u>15,681</u> Mcfd @ 15.025		Angle of Slope <u>53.8</u>	Slope, n <u>0.732</u>
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Remarks: * Fpv factors less than listings in tabler.
Point alignment not exact.

Approved By Commission:	Conducted By: <u>Ralph E. Brown</u>	Calculated By: <u>R. West</u>	Checked By:
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OL CONSERVATION COMM.
HOBBS, N. M.