

NE' EXICO OIL CONSERVATION COMMISS' N
MULTIPOINT AND ONE POINT BACK PRESSURE TEST OR GAS WELL

Form C-122
Revised 9-1-63

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 5-19-82	
Company Superior Oil Company			Connection Llano			
Pool Undesignated			Formation Morrow		Unit J	
Completion Date 3-10-82		Total Depth 15,322	Plug Back TD 15,200	Elevation G.L. 3591 K.B. 3614	Farm or Lease Name State 7 SST	
Well Size 5" Liner 7 5/8"	Wt. 18# 33.7	d 4.276 6.765	Set At 11776-15322 12,080	Perforations: From 14,636 To 14,902	Well No. 1	
Th. Size 2 3/8" 2 7/8"	Wt. 4.7# 6.5	d 1.995 2.441	Set At 14,564	Perforations: From OPEN To ENDED	Unit Sec. Twp. Rje. J 7 22S 32E	
Type Well - Single - Brdenhead - G.C. or G.O. Multiple SINGLE				Packer Set At 14,564	County Lea	
Producing Thru Tubing		Reservoir Temp. °F 210° 14,769	Mean Annual Temp. °F 60°	Baro. Press. - P _g 13.2	State New Mexico	
L 14,769	H 14,769	G _g .6212	% CO ₂ .983	% N ₂ .397	% H ₂ S Prover Meter Run 3,068 Taps Flg.	

FLOW DATA							TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. hw	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	Temp. °F	
SI							4460		PKR	CHOKE	24 HRS.
1.	3.068	x	.750	500	14"	60°	3675	74°		2/64	1 Hr.
2.	3.068	x	.750	510	37	60	3260	76		3/64	1 Hr.
3.	3.068	x	.750	510	47	58	2760	76		4/64	1 Hr.
4.	3.068	x	.750	510	62	58	2317	79		6/64	1 Hr.
5.											

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor Ft.	Gravity Factor F _g	Super Compress. Factor, F _{pv}	Rate of Flow Q, Mcfd
1	2.672	84.76	513.2	1.000	1.269	1.048	301
2	2.672	139.13	523.2	1.000	1.269	1.049	495
3	2.672	156.81	523.2	1.002	1.269	1.049	559
4	2.672	180.10	523.2	1.002	1.269	1.049	642
5							

NO.	P _f	Temp. °R	T _f	Z	Gas Liquid Hydrocarbon Ratio _____ Mcf/bbl.
1	.760	520	1.43	.911	A.P.I. Gravity of Liquid Hydrocarbons _____ Deg.
2	.775	520	1.43	.908	Specific Gravity Separator Gas .6212 XXXXXXXXXX
3	.775	518	1.43	.908	Specific Gravity Flowing Fluid XXXXX
4	.775	518	1.43	.908	Critical Pressure 675 P.S.I.A. P.S.I.A.
5					Critical Temperature 363 R R

P _c 4467.1 P _c ² 19,954				(1) $\frac{P_c^2}{P_c^2 - P_w^2} = 1.3746$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 1.26026$
NO	P _i ²	P _w	P _w ²	P _c ² - P _w ²	$AOF = Q \left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = 809$
1		3683	13564	6390	
2		3270	10693	9261	
3		2769	7667	12287	
4		2332	5438	14516	
5					

Absolute Open Flow 809	Mcfd @ 15.025	Angle of Slope @ 53° 59'	Slope, n 72700
Remarks:			
Approved By Commission:	Conducted By: T.B	Calculated By: M.K	Checked By: M.K.