

MULTIPOINT AND ONE POINT BACK PRESSURE TEST FOR GAS WELL

Type Test ☒ Initial ☐ Annual ☐ Special					Test Date 5-22-85				
Company Texaco Producing Inc.				Connection TW					
Pool UNDEZ				Formation Atoka				Unit C	
Completion Date 4-1-85		Total Depth 15,000		Plug Back TD 14,200		Elevation 3791.9		Farm or Lease Name Bilbrey Fed. Com.	
Log. Size 4 1/2	Wt. 13 1/2	d 3.958	Set At 1500	Perforations: From 13,638 To 13,726			Well No. 1		
Log. Size 2 3/8	Wt. 4.7	d 1.995	Set At 13,395	Perforations: From Open To End			Unit C	Sec. 4	
Type Well - Single - Bradenhead - G.G. or G.O. Multiple Single				Packer Set At 13,395		County Lea			
Producing Thru Tbg		Reservoir Temp. °F 208 @ 13,395		Mean Annual Temp. °F 60		Bero. Press. - P _a 13.2		State NM	
L 13,395	H 13,395	Gg .689	% CO ₂ .485	% N ₂ 3.367	% H ₂ S	Prover	Meter Run 2.067	Taps Flg	

FLOW DATA						TUBING DATA		CASING DATA		Duration of Flow
NO.	Prover Line Size	X	Orifice Size	Press. p.s.i.g.	Diff. h _w	Temp. °F	Press. p.s.i.g.	Temp. °F	Press. p.s.i.g.	
SI										
1.	2.067	x	.875	470	9	69	5805	62		
2.	2.067	x	.875	480	19	79	5380	62		
3.	2.067	x	.875	480	33	84	4640	62		
4.	2.067	x	.875	480	46	79	3780	62		
5.										

RATE OF FLOW CALCULATIONS							
NO.	Coefficient (24 Hour)	$\sqrt{h_w P_m}$	Pressure P _m	Flow Temp. Factor F _t	Gravity Factor F _g	Super Compress. Factor, F _{pr}	Rate of Flow Q, Mcfd
1	3.729	65.95	483.2	.9915	1.205	1.050	308
2	3.729	96.80	493.2	.9822	1.205	1.043	448
3	3.729	127.58	493.2	.9777	1.205	1.045	586
4	3.729	150.62	493.2	.9822	1.205	1.043	697
5.							

NO.	P _r	Temp. °R	T _r	Z	Gas Liquid Hydrocarbon Ratio	Mcf/bbl.
1.	.73	529	1.40	.907	56.639	
2.	.74	539	1.42	.910	51 @ 60	
3.	.74	544	1.44	.915		
4.	.74	539	1.42	.910		
5.						

P _c 6233.2 P _c 238852.8		A.P.I. Gravity of Liquid Hydrocarbons		Specific Gravity Separator Gas		Specific Gravity Flowing Fluid		Critical Pressure		Critical Temperature	
		51 @ 60		.689		XXXXXX		664		379	
								P.S.I.A. 668		P.S.I.A. 398	

NO.	P _i ²	P _w	P _w ²	P _c ² - P _w ²	(1) $\frac{P_c^2}{P_c^2 - P_w^2} =$	(2) $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n =$
1		5818.73	33857.3	4995.5	1.590	1.2633
2		5395.22	29108.2	9744.6		
3		4656.12	21679.3	17173.5		
4		3797.41	14420.2	24432.6		
5						

AOF = C $\left[\frac{P_c^2}{P_c^2 - P_w^2} \right]^n = .881$

Absolute Open Flow 881 Mcfd @ 15.025		Angle of Slope @ 63.25		Slope, n .504	
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Remarks: Equivalent length (deff) and friction factor calculated
Well made 1.5 bbl condensate during test

Approved By Division	Conducted By: L. J. Rupp	Calculated By: K. Erdine	Checked By: W. B. Fisher
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RECEIVED
JUN -6 1985
O.C.D.
HOBBS OFFICE